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Bayside Apartments, Barrie

Vitmont Holdings (Barrie) Inc.

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1 Introduction

Tatham Engineering Limited (Tatham) was retained by Vitmont Holdings (Barrie) Inc. to address the traffic impacts associated with the proposed Bayside Apartments mixed-use development to be located on the southwest corner of the intersection of Mulcaster Street and Collier Street within the City of Barrie. The location of the development site is illustrated in Figure 1.

The purpose of this study is to address the requirements of the City of Barrie with respect to the potential transportation impacts of the development on the area road network. In particular, the following will be discussed:

- the operations of the road system through the study area prior to the proposed development;
- an estimation of the growth in the traffic volumes not otherwise attributed to the development (i.e. from overall growth in the area and/or other developments);
- an estimation of the number of new trips the proposed development is likely to generate;
- the operations of the study area road system upon completion of the development; and
- the resulting impacts and need for mitigating measures (if required) to ensure acceptable overall road operations.

Chapter 2 of this report addresses the existing conditions, detailing the road system and corresponding traffic operations. Chapter 3 addresses future conditions, prior to the completion of the proposed development, and will address the expected growth in the traffic levels and the resulting operating conditions. Chapters 4 and 5 address the proposed development, the ensuing vehicle trips that it will generate, and the associated impacts on the road system. Chapter 6 addresses potential impacts during construction and lastly, Chapter 7 summarizes the report and the key findings.



2 Existing Conditions

This chapter will describe the road network, traffic volumes and operations for the existing conditions.

2.1 ROAD NETWORK

The road network to be addressed by this study consists of Collier Street, Mulcaster Street, Dunlop Street, Owen Street and the following intersections:

- Mulcaster Street with Collier Street:
- Dunlop Street with Mulcaster Street; and
- Collier Street with Owen Street.

The existing right-in/right-out commercial access on Collier Street, which will serve as the site access. has also been considered.

Photographs of the road system are provided in Figure 2.

2.1.1 Road Sections

Collier Street

As per *The City of Barrie Official Plan*¹, Collier Street is major collector road, providing east-west service parallel to Dunlop Street. To the west of Owen Street, Collier Street has a 2-lane cross section, providing one lane of travel per direction; whereas to the east of Owen Street (through to Mulcaster Street), the road has a 4-lane cross-section providing two lanes of travel per direction. There is a combination of parallel and angled on-street parking provided on both sides of the street (angled parking is provided on the south side only). Collier Street has a landscaped raised centre median throughout the immediate study area, with gaps to allow for left turn lanes at intersections and major driveways. As a major collector road, Collier Street has an assumed planning capacity of 500 vehicles per hour per lane (vphpl). This is consistent with lane capacity assumptions applied in the City's EMME traffic model, as noted in *The City of Barrie Transportation Master Plan - Final Report*².



¹ The City of Barrie Official Plan. Planning & Building Services Department. January 2018.

² The City of Barrie Transportation Master Plan - Final Report. WSP. June 2019

Mulcaster Street

Mulcaster Street is classified as a major collector road, providing north-south service through the study area. To the north of Collier Street, Mulcaster Street has a 4-lane cross section, providing two lanes of travel per direction; however, only the southbound lanes are delineated as such, with no pavement markings in the northbound direction (although the width can accommodate two-lanes). For the purpose of this study, the road has been modelled as providing two southbound lanes and one northbound lane. To the south of Collier Street, Mulcaster Street provides one lane of travel per direction, with on-street perpendicular parking on both sides of the street. Mulcaster Street has an assumed planning capacity of 500 vphpl.

Dunlop Street

Dunlop Street is an east-west arterial road with a 2-lane cross section (one lane of travel per direction) through the study area. Dunlop Street was recently improved to include a flexible streetscape design, consisting of mountable curb and moveable bollards which allow the onstreet parking area to be converted into pedestrian space during the summer months. While designated as an arterial road, a slightly reduced assumed planning capacity of 650 vphpl has been assumed for Dunlop Street, recognizing the urban downtown environment it serves.

Owen Street

Owen Street is a north-south local road with a 2-lane cross-section, providing one lane of travel per direction. On-street parking is currently provided on both sides of the street, with parallel parking on the west side and angled parking on the east side. As a local road, Owen Street has an assumed planning capacity of 400 vphpl.

Speed Limits

The speed limit on each road is 50 km/h, reflective of the built nature of the area and the City's speed limit policy (50 km/h unless otherwise posted). In this regard, a design speed of 60 km/h has been applied (speed limit + 10 km/h on lower speed roads).

2.1.2 Key Intersections

The configuration and control for each of the study area intersections are detailed in Table 1..:



Table 1: Intersection Configuration

| INTERSECTION | CONTROL | APPROACH | CONFIGURATION |
|--------------------------------------|--------------------------|----------|--|
| Mulcaster Street & Collier Street | signals | east | exclusive left, exclusive through & shared through/right |
| | | west | exclusive left, exclusive through & shared through/right |
| | | north | shared left/through & shared through/right |
| | | south | shared left/through & exclusive right |
| Dunlop Street & Mulcaster Street | signals | east | exclusive left & shared through/right |
| | | west | shared left/through/right |
| | | north | shared left/through & exclusive right |
| | | south | shared left/through/right |
| Collier Street & Owen Street | signals | east | exclusive left & shared through/right |
| | | west | exclusive left & shared through/right |
| | | north | shared left/through/right |
| | | south | shared left/through/right |
| Collier Street & Site Access | stop (at site access) | east | • 2 through |
| (RI/RO) | (2: 5::5 25555) | west | exclusive through & shared through/right |
| | | south | right turn |

2.2 TRAFFIC VOLUMES

To determine existing traffic volumes on the study area road network, traffic counts were obtained for the following intersections (corresponding traffic count details are provided in Appendix A):

- Mulcaster Street & Collier Street Wednesday June 1, 2016 (City of Barrie);
- Dunlop Street & Mulcaster Street Tuesday March 19, 2019 (City of Barrie);



- Collier Street & Owen Street Wednesday October 11, 2017; and
- Owen Street & Dunlop Street Wednesday October 11, 2017.

In addition to those noted above, traffic counts conducted in April 2014 for the intersections of Mulcaster Street with Collier Street and Dunlop Street as part of the *Dunlop Street Corridor Improvements Class EA*³ were also reviewed.

While some of the traffic data is older than what is typically desired, new traffic counts were not undertaken due to the ongoing COVID-19 pandemic and related restrictions, which have significantly impacted traffic volumes and patterns (i.e. new traffic counts may not reflect typical peak conditions). In addition, there is on-going construction within the Dunlop Street corridor which may also impact traffic volumes and operations through the study area.

Given that the traffic counts were conducted over various years, several adjustments were made to ensure that the existing volumes carried forward in the assessment are reasonably reflective of the existing conditions that would otherwise be anticipated in absence of the current pandemic situation. The adjustments were based on the historic volumes and growth patterns for the area. While most of the adjustments were fairly minor, the following adjustments to the intersection of Dunlop Street with Mulcaster Street were considered more significant in nature:

- The 2019 volumes on Dunlop Street, west of Mulcaster Street, were 15% less than those observed in 2017 at Owen Street reflecting an annual decrease of approximately 8% per annum. As such, the 2017 volumes observed on Dunlop Street at Owen Street were carried through the intersection with Mulcaster Street based on the 2019 distribution patterns observed at said intersection.
- The 2019 northbound PM peak hour volumes on Mulcaster Street, north of Dunlop Street, reflect a 100% increase when compared to the 2014 northbound volumes (approximately 15% per annum) and a 90% increase when compared to the 2016 northbound volumes (approximately 24% per annum). In reviewing the overall volumes, the 2019 northbound through volumes (PM peak hour) on Mulcaster Street at Dunlop Street are significantly greater than the 2014 volumes, and greater than what would otherwise be expected given the historic volumes observed for this movement along with the growth experienced at the other movements at the intersection over the same time period. The higher volumes may be associated with a traffic event on the wider road network that at the time of the counts, resulting in a route diversion. Regardless, the northbound through volumes are considered uncharacteristically high and thus have been adjusted to avoid an overly conservative assessment. The northbound through volumes (PM peak hour) on Mulcaster Street at

³ Dunlop Street Corridor Improvements Class EA Phases 1 & 2 Report. City of Barrie. December 2015



Dunlop Street have been established based on the 2016 observed northbound volumes on Mulcaster Street, south of Collier Street, adjusted by an annual growth rate of 4.8% to reflect 2019 conditions. The 4.8% annual growth rate applied reflects the observed annual growth in the northbound PM peak hour volumes on Mulcaster Street, south of Collier Street, between 2014 and 2016.

In addition to the noted adjustments, the traffic volumes were further adjusted to reflect 2020 conditions. In this respect, the following growth rates were applied:

- 4% per annum Dunlop Street;
- 2% per annum Collier Street and Mulcaster Street; and
- 1% per annum Owen Street.

Additional discussion regarding background growth rates is provide in Section 3.2.

With respect to the existing right-in/right-out access to Collier Street, inbound and outbound peak hour volumes have been assumed as traffic counts were not conducted at this intersection.

The 2020 existing volumes are illustrated in Figure 3.

2.3 TRAFFIC OPERATIONS

The assessment of existing conditions provides the baseline from which the future traffic volumes and operations (both with and without the subject development) can be assessed. The capacity, and hence operations, of a road system is effectively dictated by its intersections. As such, the analysis focused on the operations of the noted key intersections. The analysis is based on the 2020 traffic volumes, the existing configuration and intersection control (including optimization of traffic signal timings) and procedures outlined in the 2000 Highway Capacity Manual (using Synchro v.10 software). For the signalized intersections, the review considers the average delay (measured in seconds), level of service (LOS) and volume to capacity (v/c) for each approach and the overall intersection. For the unsignalized site access, the analysis considers the same metrics for the critical movements, namely the stop-controlled exit movement. Level of service A corresponds to the best operating condition with minimal delays whereas level of service F corresponds to poor operations resulting from high intersection delays. A v/c ratio of less than 1.0 indicates the intersection movement/approach is operating at less than capacity while v/c of 1.0 indicates capacity has been reached. A summary of the analyses is provided in Table 2, whereas detailed operations worksheets for the existing traffic conditions are included in Appendix B.

Based on the existing volumes and intersection configuration and control, the study area intersections provide excellent overall levels of service (LOS B or better) with minimal delays



during both peak hours. As such, no improvements are required to support the existing conditions.

Table 2: Intersection Operations - 2020 Existing Conditions

| INTERSECTION & MC | OVEMENT | CONTROL | WEEKDAY AM PEAK HOUR | | | WEEKDAY PM PEAK HOUR | | |
|--------------------------------------|---------|---------|-------------------------|-----|------|-------------------------|-----|------|
| | | | Delay | LOS | v/c | Delay | LOS | v/c |
| Mulcaster Street & Collier Street | EB | signal | 7 | А | 0.13 | 7 | А | 0.14 |
| Comer Street | WB | | 14 | В | 0.19 | 13 | В | 0.20 |
| | NB | | 22 | С | 0.70 | 21 | С | 0.65 |
| | SB | | 15 | В | 0.26 | 17 | В | 0.42 |
| | overall | signal | 15 | В | 0.39 | 14 | В | 0.36 |
| Dunlop Street & Mulcaster Street | EB | signal | 16 | В | 0.38 | 20 | В | 0.62 |
| raicaster street | WB | | 8 | Α | 0.48 | 9 | А | 0.54 |
| | NB | | 20 | С | 0.60 | 18 | В | 0.51 |
| | SB | | 22 | С | 0.60 | 26 | С | 0.73 |
| | overall | signal | 16 | В | 0.46 | 17 | В | 0.63 |
| Collier Street & Owen Street | EB | signal | 3 | А | 0.26 | 4 | А | 0.28 |
| | WB | | 3 | Α | 0.23 | 4 | А | 0.24 |
| | NB | | 24 | С | 0.28 | 22 | С | 0.30 |
| | SB | | 24 | С | 0.30 | 22 | С | 0.26 |
| | overall | signal | 6 | А | 0.26 | 7 | А | 0.28 |
| Collier Street & Site Access | NB | stop | 9 | А | 0.01 | 9 | А | 0.01 |



3 Future Background Conditions

This chapter will describe the road network and background traffic volumes expected for the years 2023 and 2028. The 2023 horizon year has been adopted to reflect full build-out and occupancy of the proposed development, whereas the 2028 horizon will address the longer-term impacts (5 years beyond build-out). While a 10-year horizon is also often considered in traffic impact studies, such is not considered necessary for this development given the limited volume of traffic that it will generate (as detailed further in Section 4.5).

3.1 ROAD NETWORK

Consideration has been given to the following road improvement (recent and planned) as detailed below.

3.1.1 Dunlop Street Corridor Improvements Class EA

As part of the recent improvements to the Dunlop Street corridor, the intersection of Dunlop Street and Mulcaster Street was reconfigured to eliminate the exclusive left turn lanes on the north, south and west approaches. The exclusive left turn lane on the east approach has been maintained. It is noted that these improvements have been considered in the operations assessment for all horizons and conditions, including existing conditions.

3.1.2 The City of Barrie Transportation Master Plan

The City of Barrie Transportation Master Plan identified the following improvements for the area:

- implement continuous two-way left turn lane along Collier Street from Mulcaster Street to Blake Street; and
- buffered bicycle lanes along Collier Street from Bayfield Street to Blake Street.

The recommended timing for the continuous two-way left turn lane on Collier Street, east of Mulcaster Street is 2026 to 2031, whereas the buffered bicycle lanes are identified by 2041. It is noted that the continuous two-way left turn lane will not have any impact on the study area intersections, recognizing that the east and west approaches on Collier Street already provide exclusive left turn lanes.

3.2 TRAFFIC VOLUMES

Future background traffic volumes expected for the 2023 and 2028 horizon years for the study area have been determined based on the existing traffic volumes, historical and projected



growth, and additional increases in volumes due to other development within the immediate area (apart from the subject development).

3.2.1 Background Growth

Population & Employment Growth

The 2016 census results for the City of Barrie indicate that the population increased from 136,063 persons in 2011 to 141,434 in 2016, translating to an annual growth rate of 0.8%. According to *A Place to Grow: Growth Plan for the Greater Golden Horseshoe*⁴, which is intended to guide future development within the Greater Golden Horseshoe, the City of Barrie has been allocated an ultimate population (year 2051) of 298,000 persons. In consideration of the 2016 census population level of 141,434, this translates to an annual increase of approximately 2.2%.

With respect to employment, the *Growth Plan* identifies an employment level of 198,000 jobs by 2051. When compared to the 2011 employment level of 77,000 jobs, the 2051 employment level translates to an annual increase of 2.4%.

City of Barrie Transportation Model

Traffic growth projections provided in *The City of Barrie Transportation Master Plan*, as derived from the City's EMME transportation model, were reviewed for 2016 (existing conditions) and 2031. The model considers the travel demands of the entire City based primarily on population and employment levels within individual zones. In developing future travel demands, a number of factors are considered including planned growth, development levels, population forecasts, transportation improvements and transit initiatives and service levels.

In comparing the model's 2016 base year volumes to the 2031 volumes, growth rates ranging from -0.2% to 2.1% were realized on the study area road sections.

Other Studies

The following background growth rates were applied in recently completed traffic studies for developments in the downtown area:

• Downtown Barrie Retirement Residence TIS⁵: 3.5% for the period 2019 to 2021 and 2% for the period 2021 to 2026;

⁵ Downtown Barrie Residences Traffic Impact Study. Tatham Engineering Ltd. December 2019.



⁴A Place to Grow: Growth Plan for the Greater Golden Horseshoe. Ministry of Municipal Affairs & Housing. August 2020.

- The Residences at Five Points TIS6: 4% on Dunlop Street, 2% on Bayfield Street, Clapperton Street, Ross Street and Collier Street, and 1% on Maple Avenue;
- Barrie Waterfront Developments TIS7: 4% on Dunlop Street, 2% on Bayfield Street and Simcoe Street, and 1% on Mary Street and Maple Street.

Background Growth Rate

In consideration of anticipated population and employment growth and projected traffic growth identified in the City's traffic model, an annual growth rate in the order of 2.0% to 2.5% is justified. However, to maintain consistency with other traffic studies completed in the area, the following background growth rates have been applied:

- 4% on Dunlop Street;
- 2% on Collier Street and Mulcaster Street; and
- 1% on Owen Street.

3.2.2 **Development Growth**

With respect to planned developments in the immediate area that will contribute additional traffic volumes to the study area road networks, the following have been considered:

- 314-unit retirement residence to be located on the southeast corner of Collier Street and Owen Street (as detailed in the Downtown Barrie Retirement Residence TIS);
- Owen Street and Worsley Street mixed-use development consisting of 447 m² of commercial retail space and 307 residential apartment units (Owen Street TIS8);
- 185 Dunlop Street East mixed-use development consisting of 1,764 m² of commercial space (including a health and fitness club) and 178 residential apartment units (Traffic Impact Study - Revised Addendum, 185 Dunlop Street⁹); and
- 157 Dunlop Street East mixed-use development consisting of 500 m² of commercial space, a 130 room hotel and 136 residential condominium units (details provided in the Traffic Impact Study - Revised Addendum, 185 Dunlop Street).

The trip generation and distribution for each background development reflects those provided in the respective traffic studies. The volumes have been distributed through the study area road

⁹ Traffic Impact Study - Revised Addendum, 185 Dunlop Street. JD Northcote Engineering Inc. October 2019.



⁶ The Residences at Five Points Traffic Impact Study. Tatham Engineering Ltd. April 2020.

⁷ Barrie Waterfront Developments Traffic Impact Study. Tatham Engineering Ltd. April 2020.

⁸ Owen Street Traffic Impact Study. JD Northcote Engineering Inc. November 2017.

network based on observed traffic patterns and anticipated travel routes. Excerpts from the respective traffic studies are provided in Appendix C, as well as figures illustrating the trip distribution through the study area.

For the purpose of this study, it has been assumed that all background development will be builtout by the 2023 horizon year. A summary of the total background development volumes distributed through the study area is illustrated in Figure 4.

3.2.3 Background Traffic Volumes

The resulting 2023 and 2028 background traffic volumes are illustrated in Figure 5 and Figure 6. The background volumes are based on the 2020 traffic volumes, adjusted to reflect the respective annual background growth rates and the additional traffic volumes associated with the noted background developments.

3.3 TRAFFIC OPERATIONS

The study area intersections were again analyzed for each horizon year given the projected background volumes. The results are summarized in Table 3 and Table 4 (detailed worksheets are provided in Appendix D). The previously noted intersection modifications and road improvements have been considered and signal timings have been optimized to ensure efficient operations.

As indicated, the subject intersections will continue to provide good overall operating conditions (LOS C or better) with minimal delays through 2028 given the assumed background traffic volumes and the existing intersection configurations and control.



Table 3: Intersection Operations - 2023 Background Conditions

| INTERSECTION & MC | OVEMENT | CONTROL | WEEKDAY AM PEAK HOUR | | | WEEKDAY PM PEAK HOUR | | |
|--------------------------------------|---------|---------|-------------------------|-----|------|-------------------------|-----|------|
| | | | Delay | LOS | v/c | Delay | LOS | v/c |
| Mulcaster Street & Collier Street | EB | signal | 8 | А | 0.14 | 7 | А | 0.16 |
| Comer Street | WB | | 15 | В | 0.21 | 14 | В | 0.22 |
| | NB | | 22 | С | 0.71 | 21 | С | 0.68 |
| | SB | | 15 | В | 0.27 | 17 | В | 0.44 |
| | overall | signal | 15 | В | 0.41 | 15 | В | 0.39 |
| Dunlop Street & Mulcaster Street | EB | signal | 18 | В | 0.46 | 22 | С | 0.70 |
| Traincuster Street | WB | | 9 | А | 0.54 | 11 | В | 0.64 |
| | NB | | 20 | С | 0.62 | 19 | В | 0.55 |
| | SB | | 23 | С | 0.62 | 30 | С | 0.79 |
| | overall | signal | 16 | В | 0.52 | 19 | В | 0.71 |
| Collier Street & Owen Street | EB | signal | 4 | А | 0.30 | 5 | А | 0.31 |
| | WB | | 4 | А | 0.26 | 4 | Α | 0.25 |
| | NB | | 22 | С | 0.32 | 22 | С | 0.37 |
| | SB | | 22 | С | 0.21 | 22 | С | 0.29 |
| | overall | signal | 7 | А | 0.30 | 8 | А | 0.32 |
| Collier Street & Site Access | NB | stop | 9 | А | 0.01 | 10 | А | 0.01 |



Table 4: Intersection Operations - 2028 Background Conditions

| INTERSECTION & MC | OVEMENT | CONTROL | | WEEKDAY AM PEAK HOUR | | | WEEKDAY PM PEAK HOUR | | |
|--------------------------------------|---------|---------|-------|-------------------------|------|-------|-------------------------|------|--|
| | | | Delay | LOS | v/c | Delay | LOS | v/c | |
| Mulcaster Street & Collier Street | EB | signal | 9 | А | 0.16 | 8 | А | 0.18 | |
| Comer Street | WB | | 16 | В | 0.24 | 15 | В | 0.26 | |
| | NB | | 23 | С | 0.74 | 22 | С | 0.71 | |
| | SB | | 15 | В | 0.28 | 17 | В | 0.47 | |
| | overall | signal | 16 | В | 0.45 | 15 | В | 0.43 | |
| Dunlop Street & Mulcaster Street | EB | signal | 20 | С | 0.56 | 30 | С | 0.84 | |
| raicaster street | WB | | 10 | В | 0.63 | 15 | В | 0.77 | |
| | NB | | 21 | С | 0.66 | 20 | В | 0.59 | |
| | SB | | 25 | С | 0.68 | 34 | С | 0.84 | |
| | overall | signal | 17 | В | 0.61 | 23 | С | 0.82 | |
| Collier Street & Owen Street | EB | signal | 5 | А | 0.33 | 5 | А | 0.34 | |
| | WB | | 4 | Α | 0.29 | 4 | А | 0.28 | |
| | NB | | 22 | С | 0.33 | 22 | С | 0.39 | |
| | SB | | 21 | С | 0.22 | 22 | С | 0.30 | |
| | overall | signal | 7 | А | 0.33 | 8 | А | 0.35 | |
| Collier Street & Site Access | NB | stop | 9 | А | 0.01 | 9 | А | 0.01 | |



Proposed Development

This chapter will provide additional details with respect to the proposed development, including its location, the projected site generated traffic volumes and the assignment of such to the adjacent road network.

4.1 SITE LOCATION

The subject site is located at 79 Collier Street in the City of Barrie (as per Figure 1). The property is bounded by existing development to the west and south, Collier Street to the north and Mulcaster Street to the east.

4.2 PROPOSED LAND-USE & PHASING

The proposed mixed-use development will consist of a 16-storey building with 126 residential apartment units and 404 m² (4,349 ft²) of ground floor commercial space. The development will also include a parking garage with 114 spaces.

A site plan in provided in Figure 7. Full build-out has been assumed by 2023.

4.3 SITE ACCESS

As illustrated in Figure 7, access to the site will be provided via the existing right-in/right-out access on Collier Street, which currently serves the adjacent development to the west (73 Collier Street). The existing access will continue to serve 73 Collier Street and will also provide access to the parking garage serving the subject site.

The loading/garbage enclosure area are located on the south side of the building and will be accessed via the existing public laneway.

4.4 **PARKING & ON-SITE CIRCULATION**

4.4.1 **Parking**

As previously noted, the proposed development will include a parking garage, providing 114 spaces for the exclusive use of the residents of the development. This reflects a rate of 0.90 space per unit. Additional discussion on the proposed parking supply, and justification for such, is provided under separate cover.

With respect to the commercial space, the City's Comprehensive Zoning By-law 2009-141 indicates that commercial uses located within the Central Area Commercial (C1) and Urban Growth Centre area are not required to provide parking. As such, parking for the commercial/retail space has not been provided.



4.4.2 **On-Site Circulation**

The internal driveway aisles serving the parking garage will provide two-way operations and maintain a minimum width of 6.4 metres (as per City standards for parking areas with stall angles of 90°). The aisles as proposed are sufficient with respect to the circulation of site generated traffic and the manoeuvring requirements of the design vehicles accessing the parking garage (i.e. passenger cars, SUV's, vans, etc.).

As previously noted, the loading area/garbage enclosure is located on the south side of the building and will be accessed via the existing public laneway. Consideration has been given to the manoeuvring requirements of a garbage truck, a medium single unit truck (i.e. for deliveries, etc.) and a light single unit truck. The truck turning templates are provided in Appendix E.

4.5 SITE TRAFFIC

4.5.1 **Trip Generation**

The number of vehicle trips to be generated by the proposed development for the weekday AM and PM peak hours has been determined based on type of use, development size, and trip generation rates as per the ITE Trip Generation Manual¹⁰, 10th Edition. Based on the proposed development, the trip rates for the multifamily housing - high-rise (ITE code 222) land-use have been applied to the residential units.

With respect to the commercial space, it is noted that a significant portion of the commercial trips will be walk-in traffic given the downtown location. Furthermore, recognizing that there will be no commercial parking on site, vehicular trips generated by the commercial use will be dispersed throughout the study area road network rather than concentrated at a single access point (i.e. commercial patrons arriving by vehicle may utilize on-street parking or municipal parking lots in the area). As such, the commercial traffic has not been considered explicitly in the trip generation; rather, it has been assumed that the commercial traffic is otherwise considered in the background growth rates. It is noted that the commercial space, with a gross floor area of 404 m² (4,349 ft²), would generate in the order of 5 to 15 peak hour trips - assuming a retail tenant (based on ITE trip rates for the shopping centre land-use). When considering an office use or personal service establishment (i.e. hair salon), the peak hour trips reduce to 10 or less.

The associated trip rates and trip estimates are provided in Table 5.

¹⁰ ITE Trip Generation Manual, 10th Edition. Institute of Transportation Engineers. September 2017.



As indicated, the proposed mixed-use development is expected to generate 39 trips during the AM peak hour and 46 trips during the PM peak hour. In context of these reduced trip estimates, a scoped traffic impact study is considered appropriate.

Table 5: Trip Generation - Bayside Apartments

| LAND-USE | RATE/ VARIABLE/ ESTIMATE SIZE | | WEEKDAY AM PEAK HOUR | | | WEEKDAY PM PEAK HOUR | | |
|--|----------------------------------|-----------|-------------------------|------|-------|-------------------------|------|-------|
| | ESTIMATE | SIZE | In | Out | Total | In | Out | Total |
| multifamily housing -high-rise (ITE 222) | rate | units | 0.07 | 0.24 | 0.31 | 0.22 | 0.14 | 0.36 |
| | estimate | 126 units | 9 | 30 | 39 | 28 | 18 | 46 |

Recognizing that the study area is well served by public transit and considering its centralized downtown location, it is expected that a portion of the trips to and from the site will be made via public transit or non-auto modes of transportation (i.e. walking, cycling etc.). Based on a review of the 2016 Transportation Tomorrow Survey (TTS) data, 10% of all trips with an origin or destination within the City of Barrie were done so via walking, cycling or public transit. To account for these trips, a 10% reduction could reasonably be applied; however, to ensure a conservative approach, no adjustments have been applied.

4.5.2 **Trip Distribution & Assignment**

The distribution of the new trips generated by the site has been developed based on the 2016 TTS trip data. The TTS is a survey of a random sampling of 5% of the households in the Greater Toronto Area and surrounding area of Central Ontario, including the City of Barrie. Based on a review of the TTS data with respect to trips to/from Barrie, the following trip distribution was identified:

- to/from the east beyond Barrie 5%;
- to/from the west beyond Barrie 5%;
- to/from the north beyond Barrie 10%;
- to/from the south beyond Barrie 10% and
- to/from locations within Barrie 70%.

As indicated, 70% of the trips remain wholly within Barrie whereas 30% originate from, or are destined to, areas outside of the City. The trips that remain within Barrie were distributed based on additional TTS trip data for the traffic zone within which the development is located. When



considering the distribution of trips that remain within the City, the ultimate trip distribution for the site is as follows:

- to/from the east 5%;
- to/from the west 20%;
- to/from the north 40%; and
- to/from the south 35%.

The assignment of the trips generated by the development to the area road network is based on the trip distribution noted above with consideration given to site access location and configuration, the area road system, and the expected travel routes.

The resulting site generated traffic volumes assigned to the road network are illustrated in Figure 8.



Future Total Conditions 5

his chapter will address the resulting impacts of the proposed mixed-use development on the adjacent road system. Three areas are to be addressed:

- operations of the key intersections, including the site access;
- available sight lines at the site access; and
- potential improvements to the study area road network, if necessary.

5.1 **TRAFFIC VOLUMES**

To assess the impacts of the increased traffic volumes resulting from the proposed development, the site generated traffic was combined with the 2023 and 2028 background traffic volumes. The resulting total traffic volumes are presented in Figure 9 and Figure 10.

5.2 TRAFFIC OPERATIONS

The operations of the key intersections were again investigated considering the total traffic volumes for each horizon year. The intersection configurations and control as employed in the background analyses have been maintained. The results of the operational review are provided in Table 6 through Table 7 (detailed worksheets are provided in Appendix F).

As indicated, the study area intersections and site access will continue to provide good overall operations (LOS C or better) with minimal delays through the 2028 horizon given the projected total volumes. It is noted that the total operating conditions are comparable to those experienced under background conditions (i.e. the proposed development will have minimal impact on the intersection operations).

The site access will also operate well below capacity during the noted peak hour conditions and provide excellent operations (LOS A), recognizing that it will operate in a right-in/right-out fashion.

In consideration of the above, no improvements are considered necessary to accommodate the future total conditions.



Table 6: Intersection Operations - 2023 Total Conditions

| INTERSECTION & MC | OVEMENT | CONTROL | | WEEKDAY AM PEAK HOUR | | | WEEKDAY PM PEAK HOUR | | |
|--------------------------------------|---------|---------|-------|-------------------------|------|-------|-------------------------|------|--|
| | | | Delay | LOS | v/c | Delay | LOS | v/c | |
| Mulcaster Street & Collier Street | EB | signal | 8 | А | 0.15 | 7 | А | 0.16 | |
| Comer Street | WB | | 15 | В | 0.21 | 14 | В | 0.22 | |
| | NB | | 22 | С | 0.71 | 21 | С | 0.68 | |
| | SB | | 15 | В | 0.27 | 17 | В | 0.44 | |
| | overall | signal | 15 | В | 0.41 | 14 | В | 0.39 | |
| Dunlop Street & Mulcaster Street | EB | signal | 18 | В | 0.46 | 22 | С | 0.70 | |
| | WB | | 9 | Α | 0.54 | 11 | В | 0.64 | |
| | NB | | 20 | С | 0.62 | 19 | В | 0.54 | |
| | SB | | 24 | С | 0.66 | 31 | С | 0.80 | |
| | overall | signal | 16 | В | 0.53 | 19 | В | 0.71 | |
| Collier Street & Owen Street | EB | signal | 4 | А | 0.30 | 5 | А | 0.33 | |
| | WB | | 4 | Α | 0.26 | 4 | Α | 0.25 | |
| | NB | | 22 | С | 0.32 | 22 | С | 0.38 | |
| | SB | | 22 | С | 0.23 | 22 | С | 0.33 | |
| | overall | signal | 7 | А | 0.30 | 8 | А | 0.34 | |
| Collier Street & Site Access | NB | stop | 9 | А | 0.05 | 9 | А | 0.04 | |



Table 7: Intersection Operations - 2028 Total Conditions

| Tuble 7: Intersection | | | | | | | | |
|--------------------------------------|---------|---------|-------|-------------------|------|-------|---------|------|
| INTERSECTION & MC | OVEMENT | CONTROL | | VEEKDA PEAK HO | | | PEAK HO | |
| | | | Delay | LOS | v/c | Delay | LOS | v/c |
| Mulcaster Street & Collier Street | EB | signal | 9 | Α | 0.17 | 8 | А | 0.18 |
| | WB | | 16 | В | 0.24 | 15 | В | 0.26 |
| | NB | | 23 | С | 0.74 | 22 | С | 0.71 |
| | SB | | 15 | В | 0.28 | 17 | В | 0.47 |
| | overall | signal | 16 | В | 0.46 | 15 | В | 0.43 |
| Dunlop Street & Mulcaster Street | EB | signal | 20 | С | 0.56 | 31 | С | 0.84 |
| | WB | | 10 | В | 0.63 | 15 | В | 0.77 |
| | NB | | 21 | С | 0.66 | 19 | В | 0.56 |
| | SB | | 26 | С | 0.71 | 36 | D | 0.85 |
| | overall | signal | 18 | В | 0.62 | 23 | С | 0.82 |
| Collier Street & Owen Street | EB | signal | 5 | Α | 0.33 | 5 | А | 0.36 |
| | WB | | 4 | Α | 0.29 | 4 | Α | 0.28 |
| | NB | | 22 | С | 0.34 | 22 | С | 0.40 |
| | SB | | 21 | С | 0.23 | 22 | С | 0.35 |
| | overall | signal | 7 | А | 0.33 | 8 | А | 0.36 |
| Collier Street & Site Access | NB | stop | 9 | А | 0.05 | 9 | А | 0.04 |

5.3 **SIGHT LINE ANALYSIS**

Based on TAC geometric design standards, the minimum stopping sight distance for a design speed of 60 km/h (posted 50 km/h + 10 km/h) is 85 metres. The minimum stopping sight distance provides sufficient distance for an approaching motorist to observe a stationary hazard in the road and bring their vehicle to a complete stop prior to the hazard. In consideration of the



right-in/right-out configuration of the access, only the sight lines to/from the west have been considered (i.e. there will be no potential conflict between vehicles exiting the site and vehicles approaching from the east).

While Collier Street maintains a straight and flat alignment, the sight lines to/from the west at the site access are restricted by both the edge of the building at 73 Collier Street and the presence of on-street parking on the south side of Collier Street (sight lines are illustrated in Figure 11). As motorists exit the site and stop prior to the sidewalk, the sight lines are limited to 10 metres due to the proximity of the northeast corner of the building at 73 Collier Street. As motorists pull forward, the sight lines improve slightly (15 to 20 metres) but are still restricted by the presence of on-street parking. While the sight lines are not ideal, it is noted that this condition is common at most private commercial driveways and public laneways located within a downtown area (including the City of Barrie). The condition will necessitate that motorists exit the site with caution. Given the straight and flat alignment of Collier Street, the available sight lines gradually improve as vehicles slowly pull forward. Achieving the desired sight lines in downtown urban conditions is often difficult due to on-street parking, street furniture, reduced building setbacks, etc.; however, vehicle operating speeds are generally lower in downtown areas and motorists' caution/awareness is heightened. Furthermore, Collier Street consists of two eastbound lanes across the access, providing a second lane for approaching vehicles to utilize should they encounter a vehicle exiting from the site unexpectedly. It is also noted that the sight lines exceed the minimum stopping distance requirements when the on-street parking is not being utilized.

While the available sight lines at the site access are not ideal, they are considered typical when compared to other downtown locations. Signage for exiting motorists to watch for pedestrians is recommended.



Construction Staging Plan 6

This chapter will describe the preparation of a preliminary construction staging plan, illustrating how construction of the development will temporarily impact the area road network. The staging plan considers trades parking, deliveries, impacts to on-street parking and pedestrian facilities, etc. It is noted that the construction staging plan is considered preliminary and for discussion purposes only, recognizing that the contractor selected to construct the development may require revisions based on the actual construction operations.

6.1 CONSTRUCTION STAGING PLAN

The following alterations to the study area transportation network (which includes travel lanes, sidewalks and on-street parking) are recommended to accommodate the construction staging for the proposed development:

- 1. Close the sidewalk on the south side of Collier Street from just beyond the west limit of the site to Mulcaster Street. Pedestrians will be directed to a protected 1.5 metre covered walkway adjacent to the eastbound curb lane. Given the existing curb extensions at the southwest corner of Collier Street with Mulcaster Street, a portion of the existing sidewalk can remain open (although it should also be covered for the duration of construction).
- Close the sidewalk on the west side of Mulcaster Street from Collier Street to the south limit of the site. Pedestrians will be directed to a protected 1.5 metre covered walkway adjacent to the southbound curb lane.
- 3. Temporarily remove the 3 parallel parking spaces on the south side of Collier Street (1 to the west of the existing access and 2 to the east of the access) and 2 perpendicular parking spaces on the west side of Mulcaster Street (the first 2 parking spaces south of the existing parking lot access). Removal of the parking spaces will facilitate the accommodation of staging construction areas and the temporary covered walkways within the existing road platform - thus mitigating impacts to the capacity of the road network.
- 4. Institute and enforce a "No Stopping" zone along Collier Street and Mulcaster Street.
- Erect construction hoarding along the frontage of the site along Collier Street and Mulcaster Street and construct a covered sidewalk to protect pedestrians.

The preliminary construction staging plan is illustrated in Appendix G.



6.2 TRADES PARKING

Given that the proposed development will be constructed to the limits of the property boundary, there will not be space available to accommodate the parking requirements for the various trade workers working on the site. As such, trade workers will be expected to utilize available municipal parking lots in the area. There are municipal lots located on Worsley Street and Owen Street, as well as on-street parking on Mulcaster Street - north of Worsley Street. The Collier Street Parkade is also in close proximity. The developer may also consider arranging for parking provision at the 100-112 Collier Street location, if available at the time of construction.

CONSTRUCTION ACCESS 6.3

Access to the site will occur via Mulcaster Street. The access will serve as the primary access point during site preparation and throughout construction of the site. A secondary staging area may be established on Collier Street if needed of small-scale deliveries and trades vehicles. Additional information regarding the staging requirements to establish the access is discussed above and illustrated in Appendix G.

6.4 IMPACT TO ADJACENT PROPERTIES

The construction staging requirements are not expected to inhibit or prevent access to the adjacent properties and businesses. While it is acknowledged that the site will require construction hoarding along the perimeter, all efforts will be made to ensure access is maintained throughout the construction process. It is noted that no lane closures are proposed as part of the construction. The existing laneway to the south of the site is to remain unobstructed during construction, allowing delivery and service vehicles to continue to access the various businesses fronting Dunlop Street and Mulcaster Street.

6.5 PEDESTRIAN MOVEMENTS

Pedestrian movements on Collier Street and Mulcaster Street will be largely unaffected by the construction of the proposed development. While portions of the sidewalks on both roads are recommended for closure, sidewalk continuity will be maintained via a covered 1.5 metre pedestrian walkway. It is recommended that the covered pedestrian walkway be constructed in a manner that negates the need for users to step up or down (i.e. the covered walkway should be constructed at the same height of the curb in areas where the walkway is located on the road). This will also allow wheelchairs to navigate the area without issue.

6.6 **ON-STREET PARKING**

As previously noted, the proposed construction staging plan will require the temporary closure of 5 on-street parking spaces (3 on Collier Street and 2 on Mulcaster Street). It is expected that



vehicles displaced by the removal of the noted parking spaces will park in other municipal lots in the area.



Summary

Proposed Development

This study has addressed the transportation impacts associated with the proposed mixed-use development located at 79 Collier Street within the City of Barrie. The proposed Bayside Apartments development is a 16-storey building with 126 residential apartment units and 404 m² of commercial space. Upon completion, the site is expected to generate a total of 39 trips during the AM peak hour and 46 trips during the PM peak hour.

Traffic Operations

In addressing the study area operations, the key intersections were analysed under existing conditions (2020) and for the 2023 and 2028 horizon periods. The results of the operational analysis indicate that the key intersections will provide good overall operating conditions through 2028 under both future background and future total conditions. The site access operations were also reviewed, with the Collier Street access providing excellent levels of service through the 2028 horizon period given the projected traffic volumes.

Sight Lines

The sight lines to/from the west along Collier Street do not satisfy the minimum stopping sight distances for a 60 km/h design speed as they are restricted by the adjacent building at 73 Collier Street and existing on-street parking. It is noted that achieving the desired sight lines in downtown urban conditions is often difficult due to on-street parking, street furniture, reduced building setbacks, etc.; however, vehicle operating speeds are generally lower in downtown areas and motorists' caution/awareness is heightened. While the available sight lines at the site access are not ideal, they are considered typical when compared to other downtown locations.

Construction Staging Plan

The preparation of the preliminary construction staging plan was undertaken to illustrate how construction of the development will temporarily impact the area road network. The staging plan considered trades parking, deliveries, impacts to on-street parking and pedestrian facilities, etc. and mitigating measures to ensure minimal impacts to the adjacent roadways.



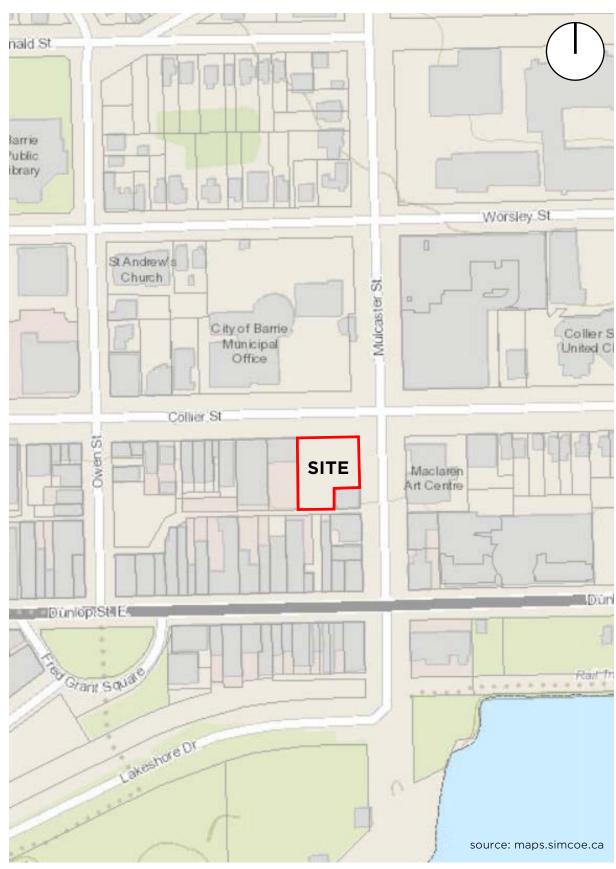








Figure 2A: Area Road Network





Looking south along Mulcaster Street from Collier Street



Looking west along Collier Street from Mulcaster Street





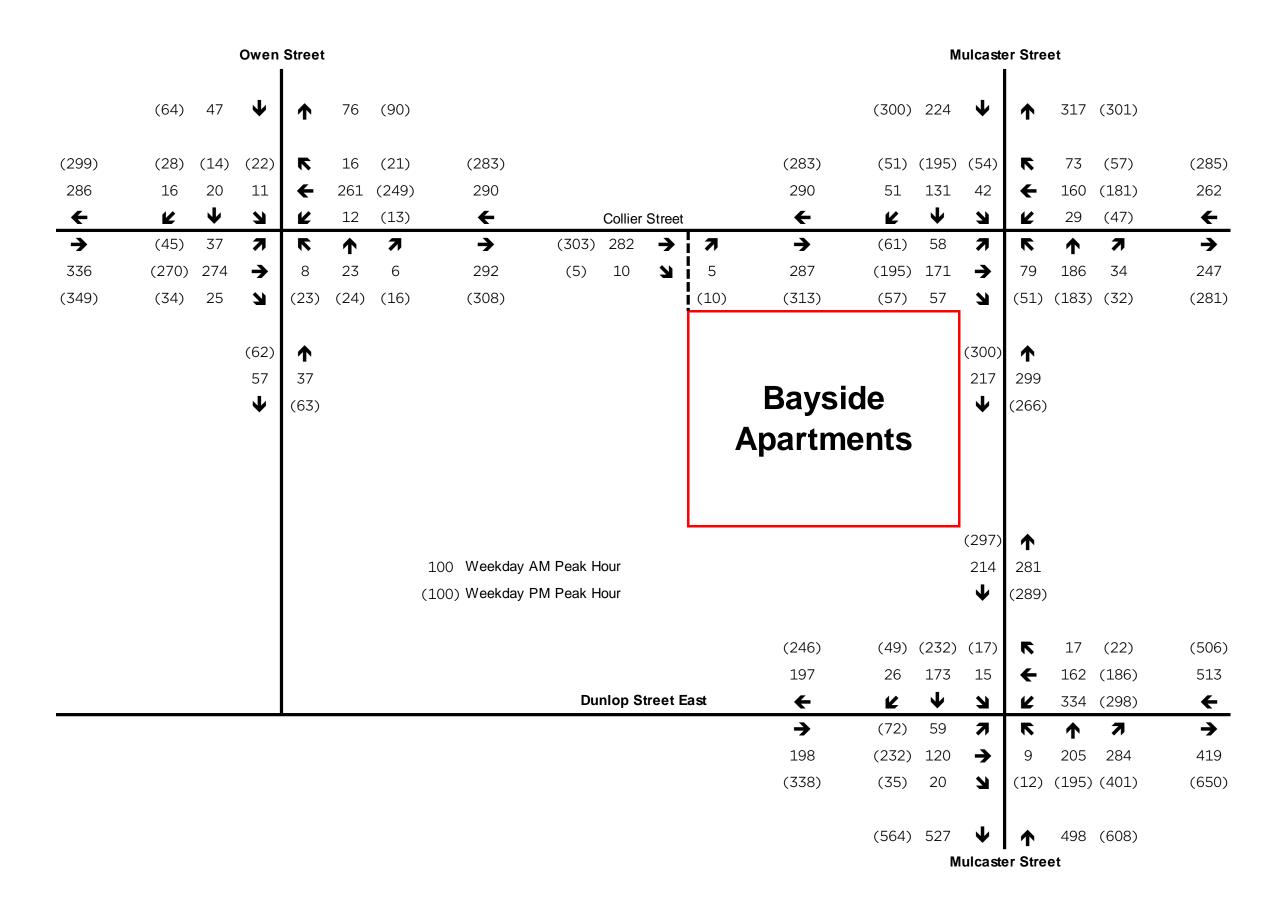
Looking east along Collier Street from site access

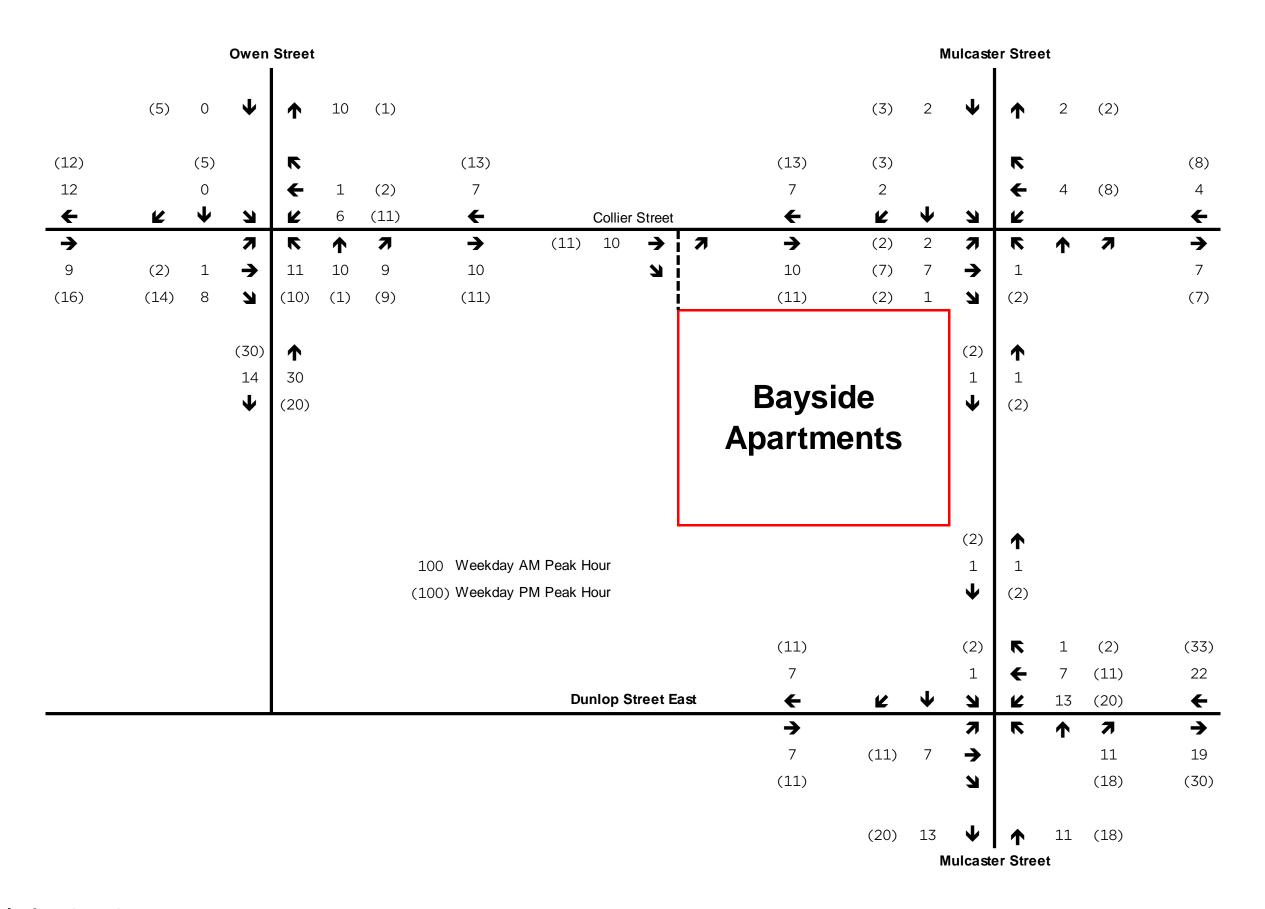


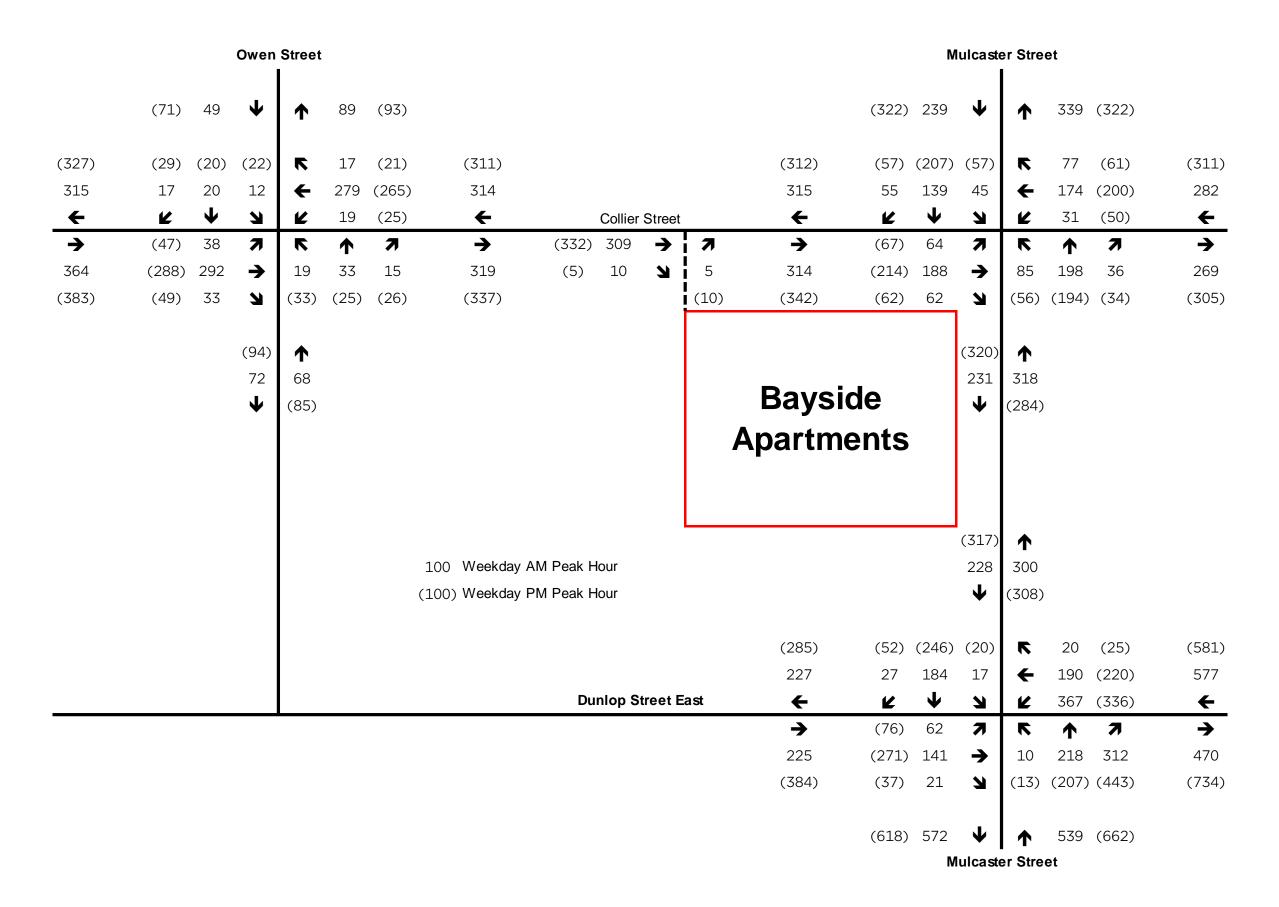
Looking west along Collier Street from site access

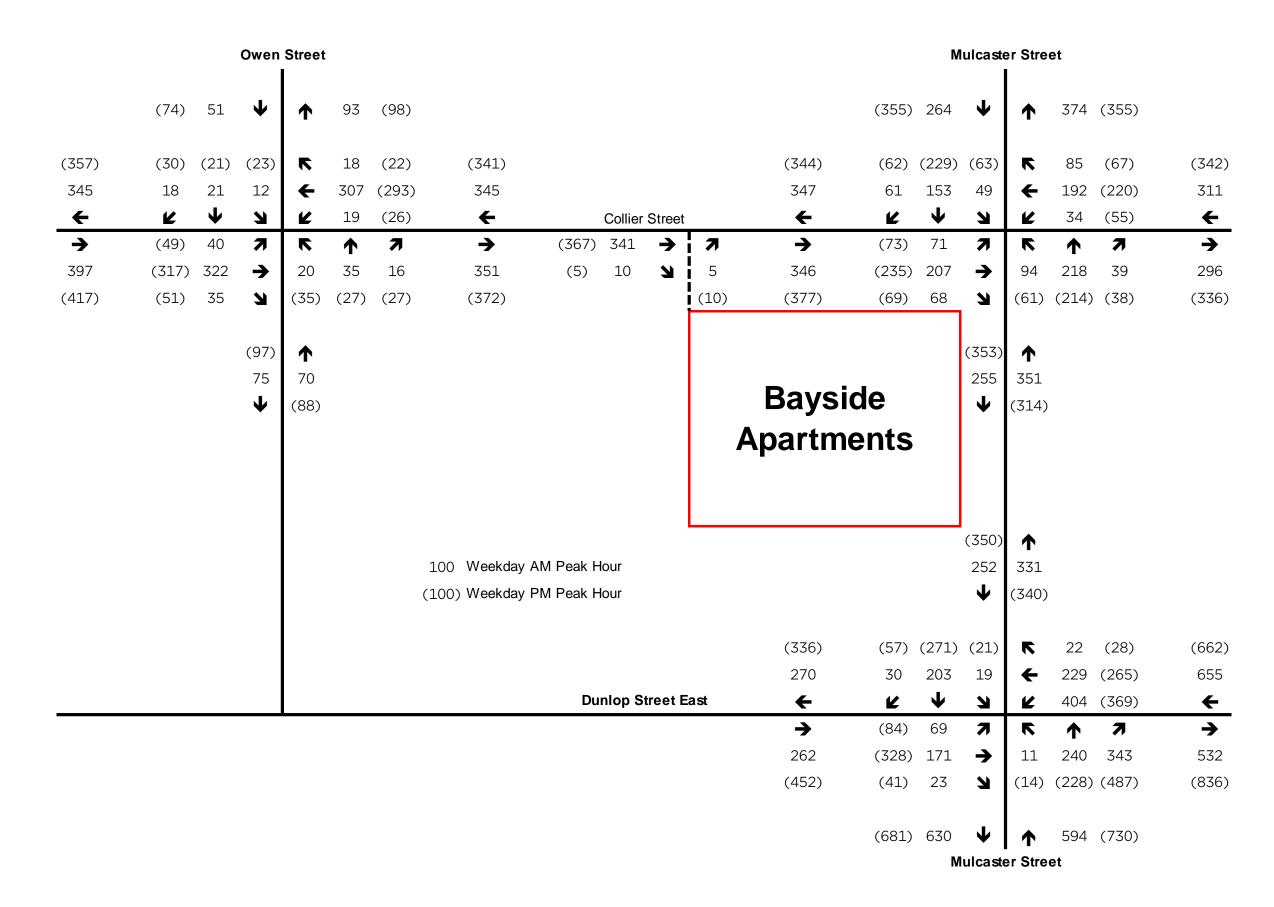
Figure 2C: Area Road Network

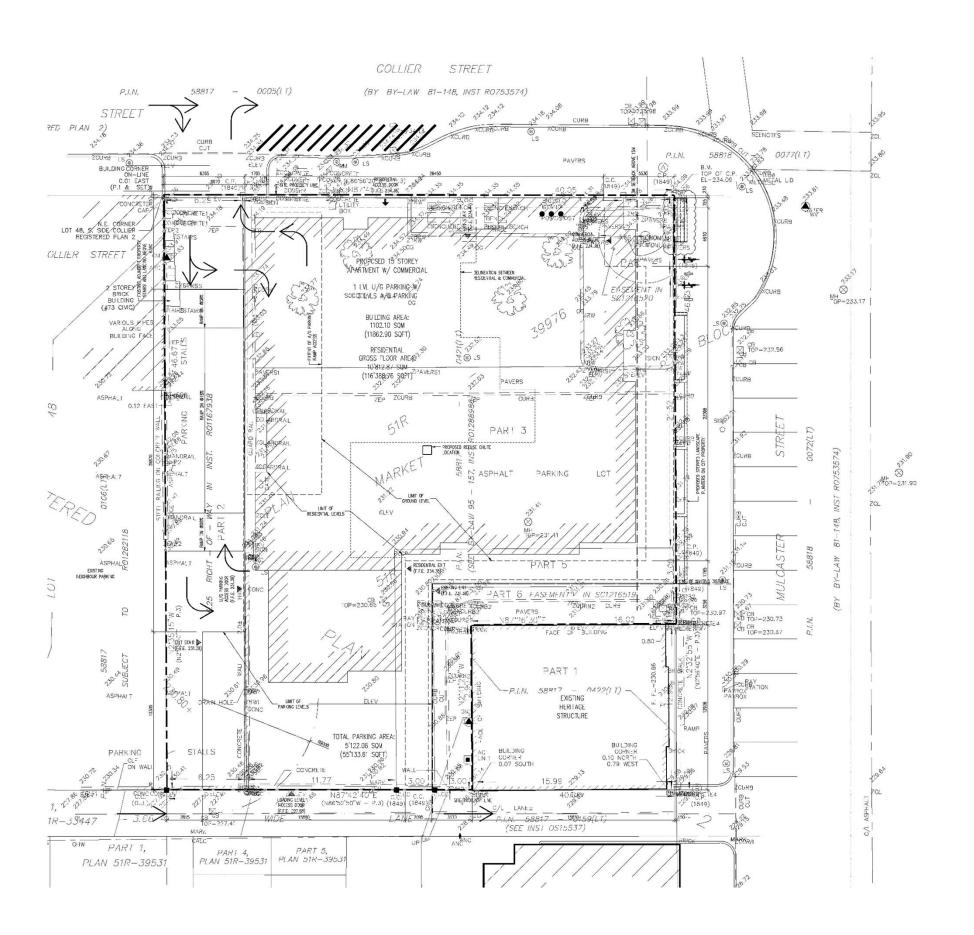




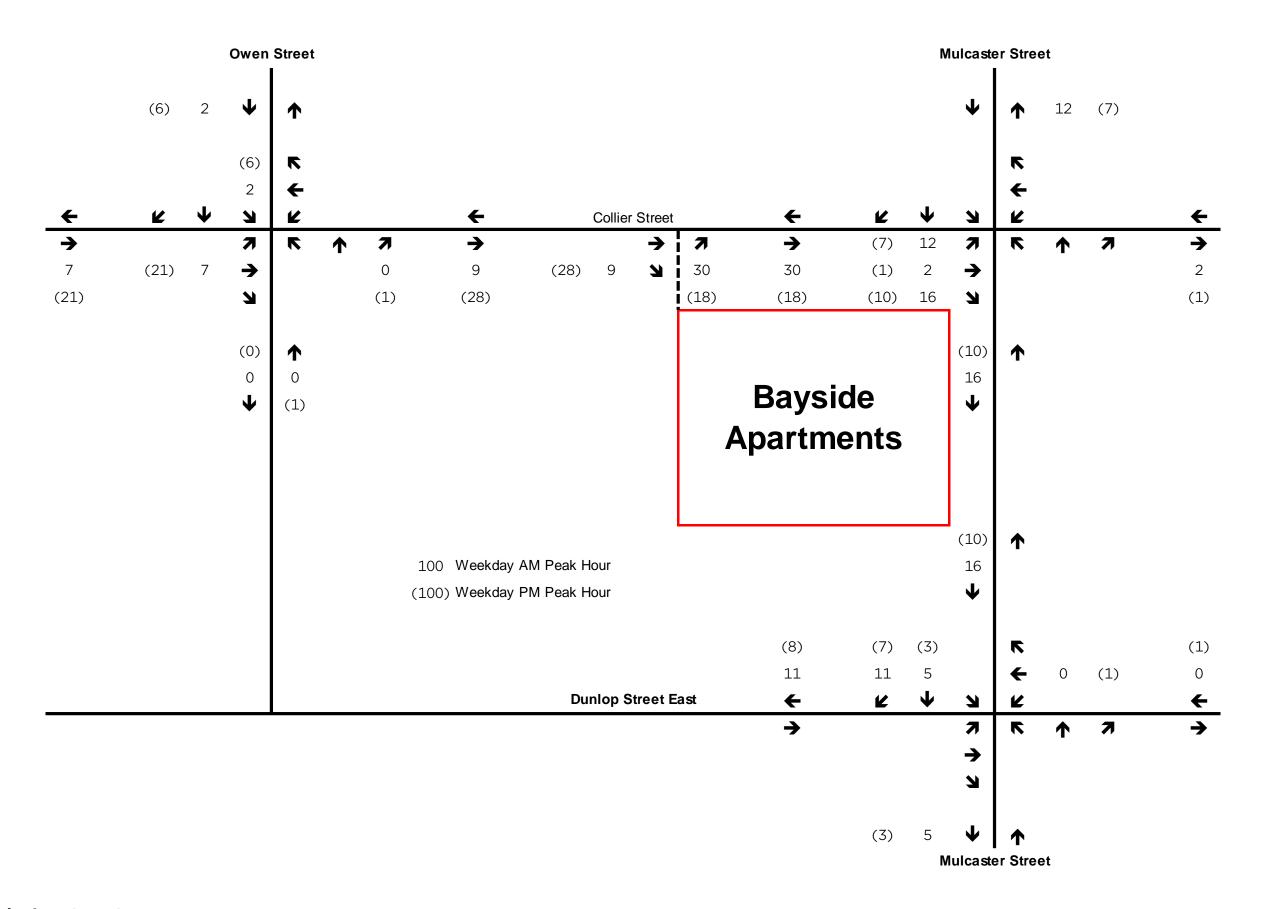


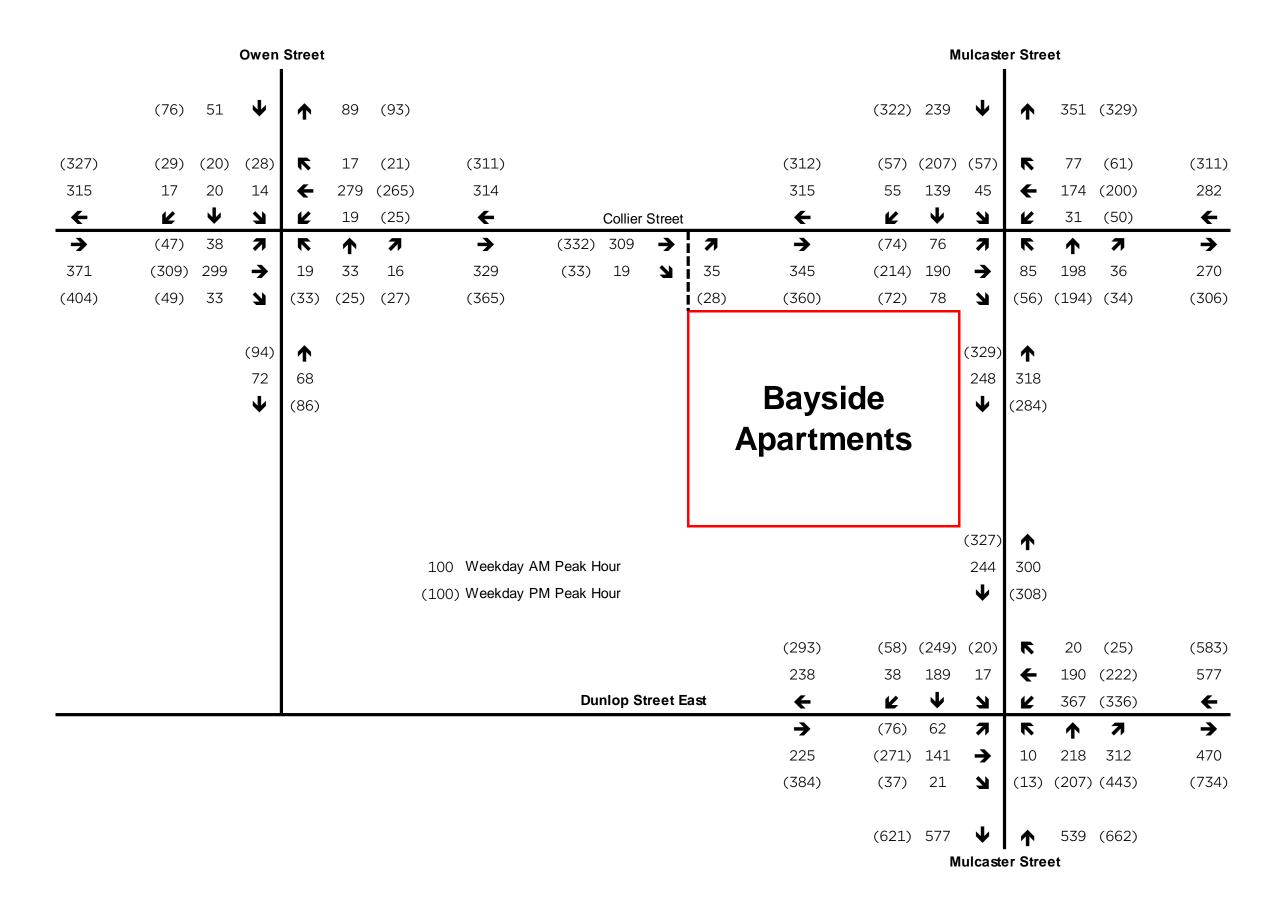


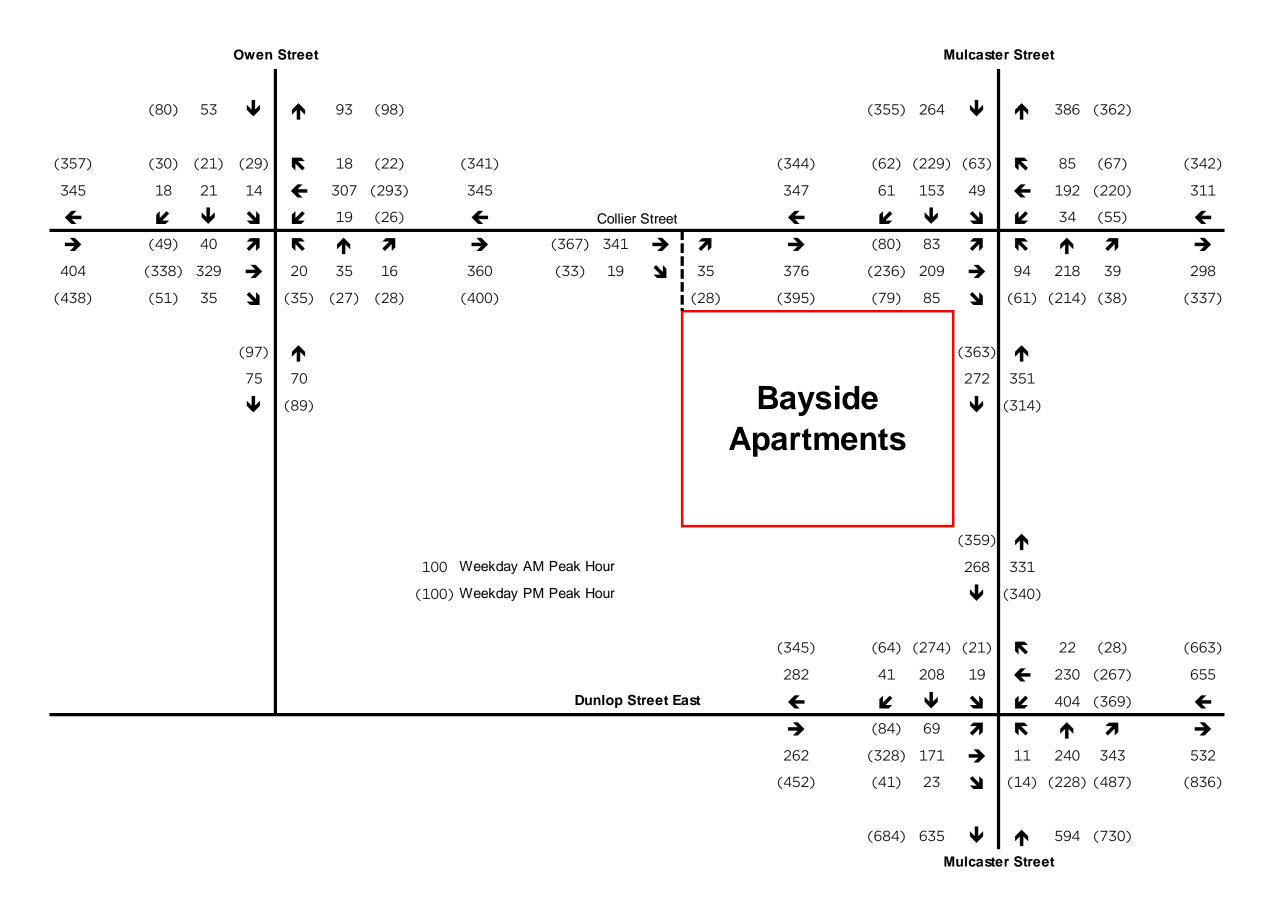














Appendix A: Traffic Count Data



| | | | | _ | | | | | | |
|-----------------------------|----------------|--------|------------|---------|----------|----------|-------------|---------|---------------|-----------|
| Morning Pea | ık Diag | ıram | 1 - | ecified | | od | | ne Ho | | |
| | | | | om: 7 | | | | om: | | |
| | | | То | 9 | :00:00 | | То |): | 9:00:0 | 0 |
| Municipality: Barrie | | | W | eather | condi | tions | | | | |
| Site #: 160020 | 0002 | | | | | | | | | |
| ntersection: Mulcas | ter St & Colli | er St | | | | _ | | | | |
| TFR File #: 1 | | | I - | rson c | | | | | | |
| Count date: 1-Jun-1 | 6 | | I | rson p | • | | | | | |
| ** Signalized Interse | ction ** | | Ma | ajor Ro | ad: N | /lulcast | er St | runs N/ | S | |
| North Leg Total: 564 | Cyclists 0 | 3 0 | 3 | ^ | Cyclists | s 0 | | East Le | eg Total | : 388 |
| North Entering: 257 | Trucks 2 | 4 1 | 7 | | Truck | | | East Er | • | 210 |
| North Peds: 20 | Cars 42 | 166 39 | 247 | | Cars | s 297 | | East Pe | eds: | 16 |
| Peds Cross: ► | Totals 44 | 173 40 |) | | Totals | 307 | | Peds C | ross: | X |
| | $\sqrt{\Box}$ | ПП | L Mulcast | er St | | | | | | |
| Cyclists Trucks Cars Totals | | | 7 | | | 13 | Cars | | S Cyclis | |
| 1 11 200 212 | | | | | | | 52 124 | 2 8 | 0 1 | 54 133 |
| <u></u> | | | N | | | 1 | 22 | 1 | 0 | 23 |
| Co | llier St | | A | | | 42 | 198 | 11 | 1 | ∟ د |
| | | ٧ | v | . E | | | | | | |
| Cyclists Trucks Cars Totals | <u></u> | | 7 | | | Col | ier St | | | |
| 0 4 33 37 | | | S | | | | | | | |
| 2 5 101 108 0 1 30 31 | | | | | | | Coro | Truoles | Cyalia | sto Total |
| 2 10 164 | 7 | | \ | 1 | | | Cars 170 | 6 | S Cyclis 2 | 178 |
| | | Mulca | aster St | | " | | .,, | | | 170 |
| Peds Cross: | Cars 218 | | Cars 3 | 4 212 | 30 | 276 | | Peds C | ross: | M |
| West Peds: 16 | Trucks 6 | | Trucks 1 | 4 | 0 | 5 | | South F | Peds: | 24 |
| West Entering: 176 | Cyclists 3 | _ 💛 | Cyclists 0 | 0 | 0 | 0 | | South E | Entering | : 281 |
| West Leg Total: 388 | Totals 227 | | Totals 3 | 5 216 | | | | | _eg Tota | |



| | | | <u> </u> | arric | | | | | | |
|--|---|---------------|--------------|---------------------|----------------|---|--------------------------------|---|-----------------------------|------------------------------------|
| Mid-day P | eak Diag | ram | | Spec From To: | : 11 | Period ::00:00 | - | | ur Pe 12:30:0 13:30:0 | 00 |
| Intersection: Mu TFR File #: 1 | rrie 00200002 Icaster St & Colli un-16 | ier St | | Perso | on co | conditions: ounted: repared: necked: | | | | |
| ** Signalized Inte | rsection ** | | | Мајо | r Ro | ad: Mulcast | er St ı | runs N/ | 'S | |
| North Leg Total: 507 North Entering: 214 North Peds: 55 Peds Cross: ▶ | Cyclists 0 Trucks 1 Cars 46 Totals 47 | 0 2 126 | 3 |) 6 208 | | Cyclists 1 Trucks 6 Cars 286 Totals 293 | - | East Le East Er East Pe Peds C | eds: | 472 244 60 ∑ |
| • | Totals 268 Collier St | \uparrow | □ ∨ ∨ | Mulcaster St | t | \$\langle\$\bar{\psi}\$ | Cars 66 142 29 237 | Trucks 1 5 0 | S Cyclis 0 1 0 | ts Totals 67 148 29 |
| 0 3 51 5 0 5 153 1 | Totals 54 58 53 53 | M | ulcaster S | s S | $\hat{\Gamma}$ | Col | Cars 219 | Trucks | s Cyclis | ts Totals |

Comments

Cars 71

Trucks 2

Cyclists 0

Totals 73

169

2

1

172

30

1

0

31

270

5

1

M

45

Peds Cross:

South Peds:

South Entering: 276

South Leg Total: 486

X

Cars 207

Trucks 3

Cyclists 0

Totals 210

Peds Cross:

West Peds:

West Entering: 265

West Leg Total: 533



| | ACCU-II | attic inc. | |
|--|--|---|--|
| Afternoon Pea | k Diagram | Specified Period From: 15:00:00 To: 18:00:00 | One Hour Peak From: 16:30:00 To: 17:30:00 |
| Municipality: Barrie Site #: 160020000 Intersection: Mulcaster S TFR File #: 1 Count date: 1-Jun-16 | 2 St & Collier St | Weather condition Person counted: Person prepared: Person checked: | าร: |
| ** Signalized Intersection | on ** | Major Road: Mulc | aster St runs N/S |
| North Entering: 330 Tru North Peds: 25 C | ists 0 6 0 6 6 5 5 ars 46 224 49 3 3 als 47 233 50 | Cyclists 4 Trucks 4 Cars 2 Totals 2 | |
| Cyclists Trucks Cars Totals 3 4 254 261 Collier S | | N E | Cars Trucks Cyclists Total 53 0 0 53 161 3 3 167 45 1 1 47 259 4 4 |
| Cyclists Trucks Cars Totals 0 1 55 56 56 1 2 177 180 53 0 0 53 53 53 1 3 285 | Mulcaster St | | Cars Trucks Cyclists Total 256 3 1 260 |
| West Peds: 43 Tru | cks 4 Truc | ars 47 162 30 23 25 25 25 25 25 25 26 25 26 26 26 26 26 26 26 26 26 26 26 26 26 | Peds Cross: ► South Peds: 24 South Entering: 246 |

Comments

Totals 47

169

30

South Leg Total: 579

West Leg Total: 550

Totals 333



Total Count Diagram

Municipality:

Site #: 1600200002

Intersection: Mulcaster St & Collier St

TFR File #:

Count date: 1-Jun-16 Weather conditions:

Person counted:

Person prepared:

Person checked:

** Signalized Intersection **

North Leg Total: 3934 North Entering: 1929 North Peds: 285 Peds Cross:

Cyclists 0 17 1 Trucks 8 25 9 Cars 338 1215 316 Totals 346 326

Cyclists 15 Trucks 56 Cars 1934 Totals 2005

Major Road: Mulcaster St runs N/S

East Leg Total: 3286 East Entering: 1655 East Peds: 258 X Peds Cross:

Cyclists Trucks Cars Totals 10 55 1717 1782



Collier St





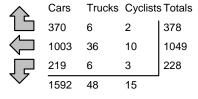
Mulcaster St



18

42

1869



Collier St

Cyclists Trucks Cars Totals 18 321 341 37 1042 1093 14 14 359 374 1 69 1722





Cars Trucks Cyclists Totals 1565 51 15 1631

X Peds Cross: West Peds: 291 West Entering: 1808 West Leg Total: 3590

Cars 1793 Trucks 45 Cyclists 21 Totals 1859

Cars 376 1243 207 1826 Trucks 11 32 5 48 Cyclists 0 0 11 11 Totals 387 1286 212

Peds Cross: ⋈ South Peds: 226 South Entering: 1885 South Leg Total: 3744



Accu-Traffic Inc. Traffic Count Summary

| Intersection: | Mulcast | er St & C | Collier St | | Count D | Date: 1-Jun-16 | Muni | cipality: Ba | arrie | | | | | |
|----------------------|------------|------------|------------|----------------|------------|------------------------|----------------------|--------------|-----------------|---------------------|----------------|---------------|--|--|
| | | | ach Tot | | | | | | h Appro | ach To | tals | | | |
| Hour | | | rucks, & C | | Total | North/South Total | Hour | | es Cars, T | | | Total | | |
| Ending | Left | Thru | Right | Grand Total | Peds | Approaches | Ending | Left | Thru | Right | Grand Total | Peds | | |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 7:00:00 | 0 | 0 | 0 | 0 | 0 | | |
| 8:00:00 | 24 | 113 | 12 | 149 | 8 | 326 | 8:00:00 | 21 | 138 | 18 | 177 | 7 | | |
| 9:00:00 | 40 | 173 | 44 | 257 | 20 | 538 | 9:00:00 | 35 | 216 | 30 | 281 | 24 | | |
| 11:00:00 | 0 | 0 | 0 | o l | 0 | 0 | 11:00:00 | 0 | 0 | 0 | 0 | 0 | | |
| 12:00:00 | 43 | 153 | 64 | 260 | <i>4</i> 6 | 467 | 12:00:00 | <i>4</i> 8 | 135 | 24 | 207 | 33 | | |
| 13:00:00 | 38 | 123 | 40 | 201 | 56 | 447 | 13:00:00 | 61 | 162 | 23 | 246 | 58 | | |
| 14:00:00 | 49 | 133 | 55 | 237 | 66 | 503 | 14:00:00 | 68 | 162 | 36 | 266 | 35 | | |
| 15:00:00 | 0 | 0 | 0 | 0 | 0 | 1 | 15:00:00 | 0 | 1 | 0 | 1 1 | 0 | | |
| 16:00:00 | 53 | 163 | 52 | 268 | 48 | 516 500 | 16:00:00 | <i>5</i> 6 | 163 | 29 | 248 | 27 | | |
| 17:00:00 | <i>4</i> 9 | 221 | 47 | 317 | 23 | 563 453 | 17:00:00 | 53 45 | 165 | 28 | 246 | 25 | | |
| 18:00:00 | 30 | 178 | 32 | 240 | 18 | <i>4</i> 53 | 18:00:00 | 45 | 144 | 24 | 213 | 17 | | |
| | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | |
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| | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | |
| Totals: | 326 | 1257 | 346 | 1929 | 285 | 3814 | S Totals: | 387 | 1286 | 212 | 1885 | 226 | | |
| - | Eas | t Appro | ach Tota | als | | East/West | | | t Appro | | | | | |
| Hour | Includ | es Cars, I | rucks, & C | Grand | Total | Total | Hour | Includ | es Cars, T I | rucks, & C | Grand | Total Peds | | |
| Ending | Left | Thru | Right | Total | Peds | Approaches | Ending | Left | Thru | Right | Total | reus | | |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 7:00:00 | 0 | 0 | 0 | 0 | 0 | | |
| 8:00:00 | 11 | 86 | 34 | 131 | 9 | 215 | 8:00:00 | 20 | 53 | 11 | 84 | 8 | | |
| 9:00:00 | 23 | 133 | 54 | 210 | 16 | 386 | 9:00:00 | 37 | 108 | 31 | 176 | 16 | | |
| 11:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 11:00:00 | 0 | 0 | 0 | 0 | 0 | | |
| 12:00:00 | 34 | 134 | 57 | 225 | 44 | 468 | 12:00:00 | 49 | 135 | 59 | 243 | 29 | | |
| 13:00:00 | 26 | 141 | 50 | 217 | 53 | 462 | 13:00:00 | <i>4</i> 5 | 138 | 62 | 245 | 64 | | |
| 14:00:00 | 38 | 135 | 60 | 233 | 58 | 474 | 14:00:00 | 48 | 142 | 51 | 241 | 50 | | |
| 15:00:00 16:00:00 | 0 31 | 0 129 | 0 | 0 204 | 0 34 | 1 483 | 15:00:00 16:00:00 | 0 | 100 | 1 51 | 1 279 | 0 57 | | |
| 17:00:00 | 36 | 157 | 44 43 | 236 | 28 | 4 63 520 | 17:00:00 | 48 51 | 180 175 | 57 58 | 279 | 37 34 | | |
| 18:00:00 | 29 | 134 | 35 | 198 | 16 | 453 | 18:00:00 | | 162 | 50 50 | 255 | 33 | | |
| 10.00.00 | 23 | 134 | 33 | 130 | 70 | 700 | 10.00.00 | 73 | 102 | 50 | 200 | 55 | | |
| | | | | | | | | | | | | | | |
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| | | | | | | | | | | | | | | |
| Totals: | 228 | 1049 | 377 | 1654 | 258 | | W Totals: | | 1093 | 374 | 1808 | 291 | | |
| | | | Calc | | /alues f | 3462 or Traffic Cr | ossing M | ajor Str | • | | 1808 | 291 | | |
| Totals: Hours E | nding: | 8:00 | | | | | | | • | 374 18:00 269 | 1808 | 291 | | |



| Count | Passenger Cars - North Approach | | | | | | | | | | | | 1 | | | | | | T | |
|----------------------|---------------------------------|---------|--------------|----------|------------|---------|-----|------|------------|----------|--------|--------|-----|------|-------------|-----------|------|------|------------|--------|
| | | Passeng | ger Cars - | North A | pproach | | | True | cks - Nort | h Approa | ach | | | Сус | clists - No | orth Appr | oach | | Pedes | trians |
| Interval | Le | eft | Th | ru | Riç | ght | Le | eft | Th | ru | Riç | ght | Le | eft | Th | ru | Ri | ght | North | Cross |
| Time | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15:00 | 2 | 2 | 26 | 26 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 4 |
| 7:30:00 | 9 | 7 | 45 | 19 | 3 | 2 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 2 |
| 7:45:00 | 13 | 4 | 72 | 27 | 6 | 3 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 11 | 0 | 0 | 7 | 1 |
| 8:00:00 | 23 | 10 | 109 | 37 | 12 | 6 | 1 | 0 | 2 | 11 | 0 | 0 | 0 | 0 | 2 | 11 | 0 | 0 | 8 | 1 |
| 8:15:00 | 31 | 8 | 147 | 38 | 17 | 5 | 1 | 0 | 2 | 0 | 1 | 1 | 0 | 0 | 3 | 1 | 0 | 0 | 13 | 5 |
| 8:30:00 | 45 | 14 | 189 | 42 | 28 | 11 | 1 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 16 | 3 |
| 8:45:00 | 50 | 5 | 226 | 37 | 33 | 5 | 2 | 1 | 3 | 1 | 1 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 22 | 6 |
| 9:00:00 | 62 | 12 | 275 | 49 | 54 | 21 | 2 | 0 | 6 | 3 | 2 | 1 | 0 | 0 | 5 | 1 | 0 | 0 | 28 | 6 |
| 9:15:00 | 62 | 0 | 275 | 0 | 54 | 0 | 2 | 0 | 6 | 0 | 2 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 28 | 0 |
| 11:00:00 | 62 | 0 | 275 | 0 | 54 | 0 | 2 | 0 | 6 | 0 | 2 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 28 | 0 |
| 11:15:00 | 72 | 10 | 315 | 40 | 68 | 14 | 2 | 0 | 7 | 1 | 2 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 37 | 9 |
| 11:30:00 | 80 | 8 | 354 | 39 | 84 | 16 | 2 | 0 | 7 | 0 | 2 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 53 | 16 |
| 11:45:00 | 91 | 11 | 388 | 34 | 107 | 23 | 2 | 0 | 8 | 1 | 2 | 0 | 1 | 1 | 8 | 0 | 0 | 0 | 61 | 8 |
| 12:00:00 | 104 | 13 | 422 | 34 | 118 | 11 | 2 | 0 | 9 | 1 | 2 | 0 | 1 | 0 | 8 | 0 | 0 | 0 | 74 | 13 |
| 12:15:00 | 114 | 10 | 442 | 20 | 126 | 8 | 2 | 0 | 10 | 1 | 3 | 1 | 1 | 0 | 8 | 0 | 0 | 0 | 85 | 11 |
| 12:30:00 | 124 | 10 | 484 | 42 | 136 | 10 | 2 | 0 | 11 | 1 | 3 | 0 | 1 | 0 | 8 | 0 | 0 | 0 | 100 | 15 |
| 12:45:00 | 135 | 11 | 507 | 23 | 145 | 9 | 2 | 0 | 11 | 0 | 3 | 0 | 1 | 0 | 8 | 0 | 0 | 0 | 115 | 15 |
| 13:00:00 | 142 | 7 | 542 | 35 | 157 | 12 | 2 | 0 | 12 | 1 | 3 | 0 | 1 | 0 | 8 | 0 | 0 | 0 | 130 | 15 |
| 13:15:00 | 152 | 10 | 572 | 30 | 170 | 13 | 4 | 2 | 12 | 0 | 3 | 0 | 1 | 0 | 8 | 0 | 0 | 0 | 146 | 16 |
| 13:30:00 | 160 | 8 | 610 | 38 | 182 | 12 | 5 | 1 | 13 | 1 | 4 | 1 | 1 | 0 | 8 | 0 | 0 | 0 | 155 | 9 |
| 13:45:00 | 172 | 12 | 638 | 28 | 197 | 15 | 5 | 0 | 13 | 0 | 5 | 1 | 1 | 0 | 8 | 0 | 0 | 0 | 176 | 21 |
| 14:00:00 | 188 | 16 | 674 | 36 | 210 | 13 | 5 | 0 | 13 | 0 | 5 | 0 | 1 | 0 | 8 | 0 | 0 | 0 | 196 | 20 |
| 14:15:00 | 188 | 0 | 674 | 0 | 210 | 0 | 5 | 0 | 13 | 0 | 5 | 0 | 1 | 0 | 8 | 0 | 0 | 0 | 196 | 0 |
| 15:00:00 | 188 | 0 | 674 | 0 | 210 | 0 | 5 | 0 | 13 | 0 | 5 | 0 | 1 | 0 | 8 | 0 | 0 | 0 | 196 | 0 |
| 15:15:00 | 199 | 11 | 716 | 42 | 221 | 11 | 6 | 1 | 14 | 1 | 5 | 0 | 1 | 0 | 9 | 1 | 0 | 0 | 208 | 12 |
| 15:30:00 | 215 | 16 | 749 | 33 | 233 | 12 | 6 | 0 | 16 | 2 | 5 | 0 | 1 | 0 | 9 | 0 | 0 | 0 | 226 | 18 |
| 15:45:00 | 225 | 10 | 785 | 36 | 245 | 12 | 7 | 1 | 17 | 1 | 6 | 1 | 1 | 0 | 9 | 0 | 0 | 0 | 232 | 6 |
| 16:00:00 | 239 | 14 | 830 | 45 | 261 | 16 | 7 | 0 | 18 | 1 | 6 | 0 | 1 | 0 | 10 | 1 | 0 | 0 | 244 | 12 |
| 16:15:00 | 249 | 10 | 880 | 50 | 274 | 13 | 8 | 1 | 21 | 3 1 | 7 | 1 | 1 | 0 | 11 | 1 | 0 | 0 | 253 | 9 |
| 16:30:00 | 255 | 6 | 928 | 48 | 281 | 7 | 8 | 0 | 22 22 | | 7 | 0 | 1 1 | 0 | 11 | 0 | 0 | 0 | 254 | 1 7 |
| 16:45:00 17:00:00 | 268 | 13 | 983 | 55 | 295 | 14 | 9 | 0 | 22 | 0 1 | 7 8 | 0 1 | 1 1 | 0 | 11 13 | 2 | 0 | 0 | 261 | 7 6 |
| | 286 297 | 18 | 1043 1115 | 60 72 | 306 313 | 11 7 | 9 | | 23 | 1 | 8 | | 1 | 0 | 16 | | 0 | | 267 276 | |
| 17:15:00 17:30:00 | 304 | 11 7 | 1115 | 37 | 313 | 14 | 9 | 0 | 25 | 1 | 8 | 0 | 1 | 0 | 17 | 3 1 | 0 | 0 | 276 | 9 |
| 17:30:00 | 304 | 6 | 1152 | 34 | 327 | 9 | 9 | 0 | 25 25 | 0 | 8 | 0 | 1 | 0 | 17 | 0 | 0 | 0 | 279 | 6 |
| | 310 | 6 | 1215 | | 338 | 2 | 9 | 0 | 25 25 | 0 | 8 | | 1 | 0 | 17 | 0 | 0 | 0 | 285 | |
| 18:00:00 | | | | 29 | | | 9 | 0 | 25 25 | | 8 | 0 | 1 | 0 | 17 | | 0 | 0 | | 0 |
| 18:15:00 18:15:15 | 316 316 | 0 | 1215 | 0 | 338 338 | 0 | 9 | 0 | 25 25 | 0 | 8 | 0 | 1 | 0 | 17 | 0 | 0 | 0 | 285 285 | 0 |
| 10:15:15 | 310 | U | 1215 | U | 330 | U | 9 | U | 25 | U | 0 | U | I | U | 17 | U | U | U | 200 | U |
| | | | | | | | | | | | | | | | | | | | | |



| CCAIIC | Date: | Passen | ger Cars | | proach | | | Tru | cks - Eas | t Approa | ch | | | Cy | clists - E | ast Appr | oach | | Pedes | trians |
|----------|-------|--------|----------|------|--------|------|-----|------|-----------|----------|-----|------|-----|------|------------|----------|------|------|--------|--------|
| Interval | Le | | Th | | Ĺ | ght | Le | | Th | | Rig | ght | Le | | Th | | | ght | East (| Cross |
| Time | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15:00 | 3 | 3 | 24 | 24 | 5 | 5 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 |
| 7:30:00 | 4 | 1 | 41 | 17 | 11 | 6 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 |
| 7:45:00 | 7 | 3 | 60 | 19 | 22 | 11 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 3 |
| 8:00:00 | 11 | 4 | 83 | 23 | 34 | 12 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 9 | 3 |
| 8:15:00 | 14 | 3 | 103 | 20 | 49 | 15 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 13 | 4 |
| 8:30:00 | 23 | 9 | 132 | 29 | 59 | 10 | 1 | 1 | 5 | 2 | 2 | 2 | 0 | 0 | 2 | 11 | 0 | 0 | 16 | 3 |
| 8:45:00 | 28 | 5 | 170 | 38 | 70 | 11 | 1 | 0 | 6 | 1 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 22 | 6 |
| 9:00:00 | 33 | 5 | 207 | 37 | 86 | 16 | 1 | 0 | 10 | 4 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 25 | 3 |
| 9:15:00 | 33 | 0 | 207 | 0 | 86 | 0 | 1 | 0 | 10 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 25 | 0 |
| 11:00:00 | 33 | 0 | 207 | 0 | 86 | 0 | 1 | 0 | 10 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 25 | 0 |
| 11:15:00 | 36 | 3 | 243 | 36 | 100 | 14 | 2 | 1 | 10 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 1 | 1 | 35 | 10 |
| 11:30:00 | 47 | 11 | 273 | 30 | 113 | 13 | 2 | 0 | 12 | 2 | 2 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 45 | 10 |
| 11:45:00 | 54 | 7 | 301 | 28 | 124 | 11 | 3 | 1 | 15 | 3 | 2 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 53 | 8 |
| 12:00:00 | 65 | 11 | 334 | 33 | 141 | 17 | 3 | 0 | 17 | 2 | 2 | 0 | 0 | 0 | 2 | 0 | 2 | 1 | 69 | 16 |
| 12:15:00 | 67 | 2 | 363 | 29 | 147 | 6 | 3 | 0 | 18 | 1 | 2 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 79 | 10 |
| 12:30:00 | 77 | 10 | 401 | 38 | 162 | 15 | 3 | 0 | 19 | 1 | 3 | 1 | 0 | 0 | 3 | 1 | 2 | 0 | 92 | 13 |
| 12:45:00 | 83 | 6 | 441 | 40 | 174 | 12 | 3 | 0 | 22 | 3 | 4 | 1 | 0 | 0 | 3 | 0 | 2 | 0 | 111 | 19 |
| 13:00:00 | 91 | 8 | 468 | 27 | 189 | 15 | 3 | 0 | 22 | 0 | 4 | 0 | 0 | 0 | 4 | 1 | 2 | 0 | 122 | 11 |
| 13:15:00 | 97 | 6 | 503 | 35 | 205 | 16 | 3 | 0 | 23 | 1 | 4 | 0 | 0 | 0 | 4 | 0 | 2 | 0 | 139 | 17 |
| 13:30:00 | 106 | 9 | 543 | 40 | 228 | 23 | 3 | 0 | 24 | 1 | 4 | 0 | 0 | 0 | 4 | 0 | 2 | 0 | 152 | 13 |
| 13:45:00 | 117 | 11 | 569 | 26 | 243 | 15 | 3 | 0 | 25 | 1 | 4 | 0 | 1 | 1 | 5 | 1 | 2 | 0 | 161 | 9 |
| 14:00:00 | 128 | 11 | 597 | 28 | 249 | 6 | 3 | 0 | 27 | 2 | 4 | 0 | 1 | 0 | 5 | 0 | 2 | 0 | 180 | 19 |
| 14:15:00 | 128 | 0 | 597 | 0 | 249 | 0 | 3 | 0 | 27 | 0 | 4 | 0 | 1 | 0 | 5 | 0 | 2 | 0 | 180 | 0 |
| 15:00:00 | 128 | 0 | 597 | 0 | 249 | 0 | 3 | 0 | 27 | 0 | 4 | 0 | 1 | 0 | 5 | 0 | 2 | 0 | 180 | 0 |
| 15:15:00 | 132 | 4 | 625 | 28 | 264 | 15 | 3 | 0 | 28 | 1 | 4 | 0 | 1 | 0 | 6 | 1 | 2 | 0 | 194 | 14 |
| 15:30:00 | 139 | 7 | 667 | 42 | 272 | 8 | 3 | 0 | 28 | 0 | 4 | 0 | 1 | 0 | 6 | 0 | 2 | 0 | 199 | 5 |
| 15:45:00 | 144 | 5 | 695 | 28 | 282 | 10 | 5 | 2 | 28 | 0 | 6 | 2 | 2 | 1 | 6 | 0 | 2 | 0 | 204 | 5 |
| 16:00:00 | 156 | 12 | 723 | 28 | 291 | 9 | 5 | 0 | 29 | 1 | 6 | 0 | 2 | 0 | 6 | 0 | 2 | 0 | 214 | 10 |
| 16:15:00 | 160 | 4 | 754 | 31 | 301 | 10 | 5 | 0 | 31 | 2 | 6 | 0 | 2 | 0 | 6 | 0 | 2 | 0 | 224 | 10 |
| 16:30:00 | 165 | 5 | 787 | 33 | 309 | 8 | 5 | 0 | 32 | 1 | 6 | 0 | 2 | 0 | 7 | 1 | 2 | 0 | 228 | 4 |
| 16:45:00 | 178 | 13 | 824 | 37 | 324 | 15 | 5 | 0 | 34 | 2 | 6 | 0 | 3 | 1 | 8 | 1 | 2 | 0 | 235 | 7 |
| 17:00:00 | 191 | 13 | 873 | 49 | 334 | 10 | 5 | 0 | 34 | 0 | 6 | 0 | 3 | 0 | 8 | 0 | 2 | 0 | 242 | 7 |
| 17:15:00 | 202 | 11 | 914 | 41 | 351 | 17 | 6 | 1 | 34 | 0 | 6 | 0 | 3 | 0 | 8 | 0 | 2 | 0 | 248 | 6 |
| 17:30:00 | 210 | 8 | 948 | 34 | 362 | 11 | 6 | 0 | 35 | 1 | 6 | 0 | 3 | 0 | 10 | 2 | 2 | 0 | 251 | 3 |
| 17:45:00 | 214 | 4 | 977 | 29 | 367 | 5 | 6 | 0 | 36 | 1 | 6 | 0 | 3 | 0 | 10 | 0 | 2 | 0 | 253 | 2 |
| 18:00:00 | 219 | 5 | 1003 | 26 | 369 | 2 | 6 | 0 | 36 | 0 | 6 | 0 | 3 | 0 | 10 | 0 | 2 | 0 | 258 | 5 |
| 18:15:00 | 219 | 0 | 1003 | 0 | 370 | 1 | 6 | 0 | 36 | 0 | 6 | 0 | 3 | 0 | 10 | 0 | 2 | 0 | 258 | 0 |
| 18:15:15 | 219 | 0 | 1003 | 0 | 370 | 0 | 6 | 0 | 36 | 0 | 6 | 0 | 3 | 0 | 10 | 0 | 2 | 0 | 258 | 0 |
| | | | | | | | | | | | | | | | | | | | | |



| Count | Date: | Passeno | er Cars - | | nproach | 0002 | | Truc | ks - Sout | h Appro | ach | | 1 | Cve | clists - So | outh Anni | roach | | Pedes | trians |
|----------|-------|---------|-----------|------|---------|------|-----|------|-----------|---------|-----|------|-----|------|-------------|-----------|-------|------|-------|--------|
| Interval | 14 | eft | Th | | i | ght | Le | | Th | - • • | Ric | aht | Le | | Th | | | ght | South | |
| Time | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15:00 | 5 | 5 | 28 | 28 | 1 | 1 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 |
| 7:30:00 | 10 | 5 | 64 | 36 | 8 | 7 | 3 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 2 | 2 |
| 7:45:00 | 14 | 4 | 97 | 33 | 11 | 3 | 3 | 0 | 1 | 0 | 0 | 0 | Ö | 0 | 2 | 0 | 0 | 0 | 5 | 3 |
| 8:00:00 | 18 | 4 | 134 | 37 | 18 | 7 | 3 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 7 | 2 |
| 8:15:00 | 20 | 2 | 191 | 57 | 21 | 3 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | Ō | 0 | 13 | 6 |
| 8:30:00 | 27 | 7 | 247 | 56 | 31 | 10 | 3 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 18 | 5 |
| 8:45:00 | 38 | 11 | 295 | 48 | 35 | 4 | 4 | 1 | 6 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 26 | 8 |
| 9:00:00 | 52 | 14 | 346 | 51 | 48 | 13 | 4 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 31 | 5 |
| 9:15:00 | 52 | 0 | 346 | 0 | 48 | 0 | 4 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 31 | 0 |
| 11:00:00 | 52 | 0 | 346 | 0 | 48 | 0 | 4 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 31 | 0 |
| 11:15:00 | 60 | 8 | 382 | 36 | 54 | 6 | 4 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 39 | 8 |
| 11:30:00 | 78 | 18 | 408 | 26 | 56 | 2 | 5 | 1 | 8 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 45 | 6 |
| 11:45:00 | 87 | 9 | 443 | 35 | 60 | 4 | 5 | 0 | 9 | 1 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 54 | 9 |
| 12:00:00 | 98 | 11 | 477 | 34 | 71 | 11 | 6 | 1 | 10 | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 64 | 10 |
| 12:15:00 | 105 | 7 | 510 | 33 | 76 | 5 | 7 | 1 | 12 | 2 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 76 | 12 |
| 12:30:00 | 117 | 12 | 539 | 29 | 81 | 5 | 8 | 1 | 15 | 3 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 97 | 21 |
| 12:45:00 | 133 | 16 | 587 | 48 | 86 | 5 | 10 | 2 | 16 | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 109 | 12 |
| 13:00:00 | 155 | 22 | 632 | 45 | 94 | 8 | 10 | 0 | 16 | 0 | 1 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 122 | 13 |
| 13:15:00 | 176 | 21 | 674 | 42 | 105 | 11 | 10 | 0 | 16 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 134 | 12 |
| 13:30:00 | 188 | 12 | 708 | 34 | 111 | 6 | 10 | 0 | 17 | 1 | 2 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 142 | 8 |
| 13:45:00 | 203 | 15 | 735 | 27 | 121 | 10 | 10 | 0 | 20 | 3 | 3 | 1 | 0 | 0 | 4 | 1 | 0 | 0 | 148 | 6 |
| 14:00:00 | 223 | 20 | 789 | 54 | 126 | 5 | 10 | 0 | 20 | 0 | 5 | 2 | 0 | 0 | 4 | 0 | 0 | 0 | 157 | 9 |
| 14:15:00 | 223 | 0 | 790 | 1 | 126 | 0 | 10 | 0 | 20 | 0 | 5 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 157 | 0 |
| 15:00:00 | 223 | 0 | 790 | 0 | 126 | 0 | 10 | 0 | 20 | 0 | 5 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 157 | 0 |
| 15:15:00 | 235 | 12 | 823 | 33 | 130 | 4 | 10 | 0 | 23 | 3 | 5 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 164 | 7 |
| 15:30:00 | 246 | 11 | 859 | 36 | 140 | 10 | 11 | 1 | 24 | 1 | 5 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 173 | 9 |
| 15:45:00 | 257 | 11 | 898 | 39 | 149 | 9 | 11 | 0 | 25 | 1 | 5 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 177 | 4 |
| 16:00:00 | 278 | 21 | 944 | 46 | 155 | 6 | 11 | 0 | 27 | 2 | 5 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 184 | 7 |
| 16:15:00 | 289 | 11 | 984 | 40 | 167 | 12 | 11 | 0 | 28 | 1 | 5 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 192 | 8 |
| 16:30:00 | 307 | 18 | 1020 | 36 | 170 | 3 | 11 | 0 | 28 | 0 | 5 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 197 | 5 |
| 16:45:00 | 323 | 16 | 1063 | 43 | 175 | 5 | 11 | 0 | 28 | 0 | 5 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 200 | 3 |
| 17:00:00 | 331 | 8 | 1106 | 43 | 183 | 8 | 11 | 0 | 30 | 2 | 5 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 209 | 9 |
| 17:15:00 | 342 | 11 | 1143 | 37 | 194 | 11 | 11 | 0 | 31 | 1 | 5 | 0 | 0 | 0 | 7 | 11 | 0 | 0 | 213 | 4 |
| 17:30:00 | 354 | 12 | 1182 | 39 | 200 | 6 | 11 | 0 | 31 | 0 | 5 | 0 | 0 | 0 | 10 | 3 | 0 | 0 | 221 | 8 |
| 17:45:00 | 367 | 13 | 1220 | 38 | 205 | 5 | 11 | 0 | 31 | 0 | 5 | 0 | 0 | 0 | 11 | 11 | 0 | 0 | 226 | 5 |
| 18:00:00 | 376 | 9 | 1243 | 23 | 207 | 2 | 11 | 0 | 32 | 11 | 5 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 226 | 0 |
| 18:15:00 | 376 | 0 | 1243 | 0 | 207 | 0 | 11 | 0 | 32 | 0 | 5 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 226 | 0 |
| 18:15:15 | 376 | 0 | 1243 | 0 | 207 | 0 | 11 | 0 | 32 | 0 | 5 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 226 | 0 |
| | | | | | | | | | | | | | | | | | | | | |



| Count | t Date: | 1-Jun-1 | | | 160020 | 0002 | | | | | | | | | | | | | | |
|----------|---------|---------|------------|----------|---------|------|-----|------|-----------|-----------|-----|------|-----|------|------------|----------|------|------|-------|--------|
| | | Passen | ger Cars · | - West A | pproach | | | Tru | cks - Wes | st Approa | ch | | | Су | clists - W | est Appr | oach | | Pedes | trians |
| Interval | Le | eft | Th | ru | Rig | ght | Le | eft | Th | ru | Ri | ght | Le | eft | Th | ru | Ri | ght | West | Cross |
| Time | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15:00 | 6 | 6 | 7 | 7 | 1 | 1 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 4 |
| 7:30:00 | 11 | 5 | 21 | 14 | 4 | 3 | 1 | 1 | 2 | 2 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 |
| 7:45:00 | 14 | 3 | 33 | 12 | 5 | 1 | 1 | 0 | 2 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 2 |
| 8:00:00 | 18 | 4 | 48 | 15 | 8 | 3 | 2 | 11 | 4 | 2 | 3 | 0 | 0 | 0 | 1 | 11 | 0 | 0 | 8 | 2 |
| 8:15:00 | 29 | 11 | 67 | 19 | 15 | 7 | 3 | 1 | 4 | 0 | 3 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 11 | 3 |
| 8:30:00 | 33 | 4 | 93 | 26 | 21 | 6 | 5 | 2 | 6 | 2 | 3 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 19 | 8 |
| 8:45:00 | 40 | 7 | 120 | 27 | 29 | 8 | 6 | 1 | 7 | 1 | 4 | 1 | 0 | 0 | 2 | 1 | 0 | 0 | 20 | 1 |
| 9:00:00 | 51 | 11 | 149 | 29 | 38 | 9 | 6 | 0 | 9 | 2 | 4 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 24 | 4 |
| 9:15:00 | 51 | 0 | 149 | 0 | 38 | 0 | 6 | 0 | 9 | 0 | 4 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 24 | 0 |
| 11:00:00 | 51 | 0 | 149 | 0 | 38 | 0 | 6 | 0 | 9 | 0 | 4 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 24 | 0 |
| 11:15:00 | 60 | 9 | 181 | 32 | 52 | 14 | 7 | 11 | 9 | 0 | 4 | 0 | 0 | 0 | 4 | 11 | 0 | 0 | 28 | 4 |
| 11:30:00 | 70 | 10 | 209 | 28 | 65 | 13 | 7 | 0 | 11 | 2 | 7 | 3 | 0 | 0 | 4 | 0 | 0 | 0 | 36 | 8 |
| 11:45:00 | 86 | 16 | 242 | 33 | 75 | 10 | 9 | 2 | 11 | 0 | 7 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 45 | 9 |
| 12:00:00 | 96 | 10 | 279 | 37 | 92 | 17 | 9 | 0 | 13 | 2 | 9 | 2 | 1 | 1 | 4 | 0 | 0 | 0 | 53 | 8 |
| 12:15:00 | 105 | 9 | 303 | 24 | 111 | 19 | 9 | 0 | 13 | 0 | 10 | 11 | 1 | 0 | 4 | 0 | 0 | 0 | 55 | 2 |
| 12:30:00 | 112 | 7 | 338 | 35 | 124 | 13 | 10 | 1 | 15 | 2 | 10 | 0 | 1 | 0 | 4 | 0 | 0 | 0 | 83 | 28 |
| 12:45:00 | 127 | 15 | 374 | 36 | 134 | 10 | 10 | 0 | 16 | 11 | 10 | 0 | 1 | 0 | 4 | 0 | 0 | 0 | 100 | 17 |
| 13:00:00 | 139 | 12 | 413 | 39 | 152 | 18 | 11 | 1 | 17 | 11 | 11 | 11 | 1 | 0 | 4 | 0 | 0 | 0 | 117 | 17 |
| 13:15:00 | 152 | 13 | 456 | 43 | 160 | 8 | 12 | 1 | 18 | 1 | 11 | 0 | 1 | 0 | 4 | 0 | 0 | 0 | 132 | 15 |
| 13:30:00 | 163 | 11 | 491 | 35 | 176 | 16 | 13 | 1 | 20 | 2 | 11 | 0 | 1 | 0 | 4 | 0 | 0 | 0 | 138 | 6 |
| 13:45:00 | 173 | 10 | 519 | 28 | 188 | 12 | 13 | 0 | 21 | 1 | 11 | 0 | 2 | 1 | 5 | 1 | 0 | 0 | 153 | 15 |
| 14:00:00 | 183 | 10 | 548 | 29 | 200 | 12 | 14 | 1 | 23 | 2 | 14 | 3 | 2 | 0 | 5 | 0 | 0 | 0 | 167 | 14 |
| 14:15:00 | 183 | 0 | 548 | 0 | 201 | 11 | 14 | 0 | 23 | 0 | 14 | 0 | 2 | 0 | 5 | 0 | 0 | 0 | 167 | 0 |
| 15:00:00 | 183 | 0 | 548 | 0 | 201 | 0 | 14 | 0 | 23 | 0 | 14 | 0 | 2 | 0 | 5 | 0 | 0 | 0 | 167 | 0 |
| 15:15:00 | 191 | 8 | 587 | 39 | 214 | 13 | 15 | 11 | 23 | 0 | 14 | 0 | 2 | 0 | 7 | 2 | 0 | 0 | 181 | 14 |
| 15:30:00 | 202 | 11 | 624 | 37 | 230 | 16 | 16 | 11 | 25 | 2 | 14 | 0 | 2 | 0 | 9 | 2 | 0 | 0 | 201 | 20 |
| 15:45:00 | 216 | 14 | 677 | 53 | 242 | 12 | 16 | 0 | 26 | 11 | 14 | 0 | 2 | 0 | 9 | 0 | 0 | 0 | 213 | 12 |
| 16:00:00 | 229 | 13 | 716 | 39 | 252 | 10 | 16 | 0 | 30 | 4 | 14 | 0 | 2 | 0 | 10 | 11 | 0 | 0 | 224 | 11 |
| 16:15:00 | 239 | 10 | 757 | 41 | 273 | 21 | 16 | 0 | 31 | 11 | 14 | 0 | 2 | 0 | 10 | 0 | 0 | 0 | 233 | 9 |
| 16:30:00 | 248 | 9 | 795 | 38 | 282 | 9 | 16 | 0 | 33 | 2 | 14 | 0 | 2 | 0 | 11 | 1 | 1 | 1 | 237 | 4 |
| 16:45:00 | 266 | 18 | 838 | 43 | 288 | 6 | 16 | 0 | 33 | 0 | 14 | 0 | 2 | 0 | 12 | 11 | 1 | 0 | 241 | 4 |
| 17:00:00 | 280 | 14 | 886 | 48 | 309 | 21 | 16 | 0 | 33 | 0 | 14 | 0 | 2 | 0 | 12 | 0 | 1 | 0 | 258 | 17 |
| 17:15:00 | 294 | 14 | 930 | 44 | 320 | 11 | 17 | 1 | 34 | 1 | 14 | 0 | 2 | 0 | 12 | 0 | 1 | 0 | 273 | 15 |
| 17:30:00 | 303 | 9 | 972 | 42 | 335 | 15 | 17 | 0 | 35 | 1 | 14 | 0 | 2 | 0 | 12 | 0 | 1 | 0 | 280 | 7 |
| 17:45:00 | 314 | 11 | 1006 | 34 | 352 | 17 | 18 | 1 | 36 | 11 | 14 | 0 | 2 | 0 | 14 | 2 | 1 | 0 | 287 | 7 |
| 18:00:00 | 321 | 7 | 1042 | 36 | 359 | 7 | 18 | 0 | 37 | 1 | 14 | 0 | 2 | 0 | 14 | 0 | 1 | 0 | 291 | 4 |
| 18:15:00 | 321 | 0 | 1042 | 0 | 359 | 0 | 18 | 0 | 37 | 0 | 14 | 0 | 2 | 0 | 14 | 0 | 1 | 0 | 291 | 0 |
| 18:15:15 | 321 | 0 | 1042 | 0 | 359 | 0 | 18 | 0 | 37 | 0 | 14 | 0 | 2 | 0 | 14 | 0 | 1 | 0 | 291 | 0 |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |

Trans-Plan Transportation Inc.

Site ID Code: Intersection Location: Municipality: Count Date:

Weather and Temperature:

Surveyor:

Dunlop Street & Mulcaster Street Barrie, Ontario Tuesday March 19, 2019 Partly Sunny, 4 Degrees

| | | | | | ORTH. | | | | | | | | | | | | PROA | | | | | | | | | PROA | | | | | | | | W | | | OACH | | | | | 1 | Grand | | |
|------|------------|-----|----------|---|-------|---|----|--------|---|------|-------|----|-----|---|----|----------|------|----|------|---|------|-------|---|-----|-----|------|------|---|----|-------|---|------|-------|----|-----|----|------|------|---|----|-------|-----|--------|--------|-------|
| AM | | CAR | <u> </u> | T | RUCK | | C, | YCLIST | | Peds | Total | | CAR | | TI | RUCK | | C) | CLIS | | Peds | Total | | CAR | | T | RUCK | | CY | CLIS1 | | Peds | Total | | CAR | | Т | RUCK | | CY | CLIST | Do | eds To | ntal I | Total |
| | L | Т | R | L | Т | R | L | Т | R | | | L | T | R | L | <u>T</u> | R | L | Т | R | | | L | Т | R | L | Т | R | L | Т | R | | | L | T | R | L | Т | R | ш | T | R | | | |
| 7:00 | 2 | 18 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 27 | 48 | 30 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 82 | 0 | 11 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 29 | 6 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 (| 0 1 | | 155 |
| 7:15 | 1 | 19 | 7 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 28 | 47 | 34 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 88 | 0 | 46 | 54 | 0 | 1 | 1 | 0 | 0 | 0 | 3 | 105 | 8 | 13 | 1 | 0 | 0 | 0 | 0 | 0 | 0 . | 1 2 | 23 | 244 |
| 7:30 | 1 | 33 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 40 | 70 | 50 | 7 | 1 | 0 | 1 | 0 | 0 | 0 | 2 | 131 | 1 | 44 | 74 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 120 | 6 | 13 | 4 | 0 | 1 | 0 | 0 | 0 | 0 2 | 2 2 | 26 | 317 |
| 7:45 | 0 | 34 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 39 | 88 | 27 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 5 | 122 | 2 | 49 | 62 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 115 | 9 | 20 | 2 | 0 | 2 | 0 | 0 | 0 | 0 2 | 2 3 | 35 | 311 |
| 8:00 | 0 | 34 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 40 | 84 | 37 | 3 | 1 | 2 | 0 | 0 | 0 | 0 | 2 | 129 | 1 | 42 | 54 | 0 | 0 | 2 | 0 | 0 | 0 | 5 | 104 | 16 | 23 | 8 | 0 | 2 | 0 | 0 | 0 | 0 / | 5 5 | 54 | 327 |
| 8:15 | 1 | 28 | 11 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 41 | 83 | 39 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 130 | 5 | 62 | 85 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 157 | 17 | 23 | 2 | 1 | 1 | 0 | 0 | 0 | 0 / | 4 4 | 48 | 376 |
| 8:30 | 1 | 27 | 8 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 37 | 70 | 40 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 4 | 118 | 1 | 36 | 71 | 0 | 3 | 2 | 0 | 0 | 0 | 4 | 117 | 10 | 12 | 6 | 0 | 0 | 1 | 0 | 0 | 0 | 1 3 | 30 | 302 |
| 8:45 | 0 | 26 | 8 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 36 | 75 | 22 | 5 | 0 | 3 | 0 | 0 | 0 | 0 | 2 | 107 | 0 | 55 | 72 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 131 | 10 | 22 | 7 | 0 | 2 | 0 | 0 | 0 | 0 : | 5 4 | 16 | 320 |
| MD | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 11:0 | 0 1 | 35 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 45 | 47 | 30 | 2 | 4 | 1 | 0 | 0 | 0 | 0 | 6 | 90 | 0 | 28 | 52 | 0 | 2 | 0 | 0 | 0 | 0 | 6 | 88 | 8 | 29 | 7 | 1 | 3 | 1 | 0 | 0 | 0 | 8 5 | 57 | 280 |
| 11:1 | 5 3 | 31 | 13 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 48 | 37 | 33 | 5 | 0 | 1 | 0 | 0 | 0 | 0 | 9 | 85 | 5 | 25 | 63 | 0 | 0 | 2 | 0 | 0 | 0 | 8 | 103 | 16 | 37 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 5 6 | 66 | 302 |
| 11:3 | 7 | 25 | 14 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 47 | 55 | 32 | 9 | 3 | 2 | 0 | 0 | 0 | 0 | 11 | 112 | 2 | 16 | 53 | 0 | 1 | 0 | 0 | 0 | 0 | 3 | 75 | 9 | 29 | 11 | 0 | 0 | 0 | 0 | 0 | 0 1 | 12 6 | 31 | 295 |
| 11:4 | 5 0 | 36 | 12 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 51 | 60 | 34 | 3 | 1 | 1 | 0 | 0 | 0 | 0 | 10 | 109 | 4 | 33 | 62 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 107 | 14 | 38 | 11 | 0 | 0 | 0 | 0 | 0 | 0 1 | 19 8 | 32 | 349 |
| 12:0 | 2 | 47 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 81 | 67 | 29 | 9 | 1 | 0 | 0 | 0 | 0 | 0 | 9 | 115 | 5 | 30 | 63 | 0 | 2 | 1 | 0 | 0 | 0 | 5 | 106 | 18 | 27 | 9 | 1 | 0 | 0 | 0 | 0 | 0 1 | 11 6 | 66 | 368 |
| 12:1 | 5 5 | 41 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 75 | 46 | 40 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 104 | 9 | 32 | 48 | 0 | 0 | 3 | 0 | 0 | 0 | 10 | 102 | 14 | 33 | 11 | 0 | 3 | 0 | 0 | 0 | 0 1 | 12 7 | 73 | 354 |
| 12:3 | 8 0 | 35 | 11 | 1 | 0 | 0 | 0 | 0 | 0 | 8 | 63 | 58 | 36 | 6 | 1 | 1 | 1 | 0 | 0 | 0 | 7 | 110 | 7 | 44 | 70 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 128 | 11 | 30 | 7 | 0 | 1 | 0 | 0 | 0 | 0 1 | 13 6 | 52 | 363 |
| 12:4 | 5 5 | 40 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 77 | 68 | 57 | 8 | 2 | 1 | 0 | 0 | 0 | 0 | 10 | 146 | 7 | 32 | 76 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 123 | 9 | 28 | 9 | 0 | 3 | 0 | 0 | 0 | 0 2 | 20 6 | 69 | 415 |
| 13:0 | 9 | 33 | 17 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 61 | 59 | 33 | 8 | 2 | 0 | 1 | 0 | 0 | 0 | 7 | 110 | 6 | 30 | 71 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 114 | 15 | 35 | 7 | 1 | 0 | 0 | 0 | 0 | 0 ' | 6 6 | 64 | 349 |
| 13:1 | 5 2 | 40 | 12 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 56 | 72 | 43 | 7 | 2 | 2 | 0 | 0 | 0 | 0 | 10 | 136 | 3 | 36 | 73 | 0 | 0 | 1 | 0 | 0 | 0 | 8 | 121 | 13 | 37 | 9 | 1 | 2 | 1 | 0 | 0 | 0 | 7 7 | 70 | 383 |
| 13:3 | 6 | 28 | 13 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 49 | 53 | 44 | 7 | 2 | 0 | 0 | 0 | 0 | 0 | 7 | 113 | 4 | 43 | 52 | 0 | 2 | 1 | 0 | 0 | 0 | 8 | 110 | 18 | 24 | 6 | 0 | 1 | 1 | 0 | 0 | 0 1 | 11 6 | 31 | 333 |
| 13:4 | 5 3 | 35 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 57 | 60 | 40 | 6 | 1 | 1 | 0 | 0 | 0 | 0 | 10 | 118 | 4 | 35 | 73 | 0 | 0 | 1 | 0 | 0 | 0 | 13 | 126 | 16 | 42 | 4 | 1 | 1 | 0 | 0 | 0 | 0 8 | 8 7 | 72 | 373 |
| PM | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 15:0 | 3 | 38 | 13 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 57 | 54 | 42 | 3 | 1 | 1 | 0 | 0 | 0 | 0 | 7 | 108 | 5 | 35 | 78 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 127 | 18 | 33 | 9 | 0 | 3 | 0 | 0 | 0 | 0 1 | 11 7 | 74 | 366 |
| 15:1 | 5 3 | 44 | 13 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 61 | 76 | 39 | 3 | 1 | 1 | 0 | 0 | 0 | 0 | 8 | 128 | 2 | 35 | 79 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 120 | 15 | 41 | 4 | 0 | 0 | 0 | 0 | 0 | 0 8 | 8 6 | 68 | 377 |
| 15:3 | 6 | 49 | 11 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 67 | 74 | 30 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 5 | 115 | 1 | 30 | 72 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 107 | 22 | 38 | 6 | 0 | 0 | 1 | 0 | 0 | 0 (| 6 7 | 73 | 362 |
| 15:4 | 5 3 | 52 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 72 | 67 | 33 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 9 | 114 | 6 | 35 | 94 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 143 | 16 | 28 | 9 | 0 | 2 | 1 | 0 | 0 | 0 | 8 6 | 64 | 393 |
| 16:0 | 5 | 54 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 72 | 62 | 40 | 5 | 2 | 1 | 0 | 0 | 0 | 0 | 10 | 120 | 1 | 258 | 99 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 366 | 10 | 49 | 10 | 0 | 1 | 0 | 0 | 0 | 0 | 2 7 | 72 | 630 |
| 16:1 | 3 | 53 | 6 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 63 | 75 | 37 | 5 | 3 | 0 | 0 | 0 | 0 | 0 | 6 | 126 | 3 | 47 | 77 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 130 | 14 | 45 | 6 | 0 | 1 | 0 | 0 | 0 | 0 8 | 8 7 | 74 | 393 |
| 16:3 | 0 4 | 57 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 68 | 79 | 31 | 5 | 1 | 2 | 0 | 0 | 0 | 0 | 1 | 119 | 1 | 33 | 102 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 140 | 12 | 37 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 5 6 | 60 | 387 |
| 16:4 | 5 5 | 61 | 11 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 79 | 70 | 29 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 114 | 3 | 48 | 115 | 0 | 0 | 1 | 0 | 0 | 0 | 5 | 172 | 21 | 51 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 4 8 | 33 | 448 |
| 17:0 | 5 | 59 | 14 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 80 | 61 | 30 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 14 | 108 | 3 | 57 | 115 | 0 | 0 | 3 | 0 | 0 | 0 | 8 | 186 | 19 | 36 | 5 | 0 | 0 | 0 | 0 | 0 | 0 : | 5 6 | 35 | 439 |
| 17:1 | 5 2 | 49 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 57 | 57 | 40 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 11 | 112 | 1 | 46 | 102 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 152 | 6 | 43 | 10 | 0 | 1 | 0 | 0 | 0 | 0 | 6 6 | 66 | 387 |
| 17:3 | 5 | 43 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 56 | 60 | 28 | 5 | 1 | 1 | 0 | 0 | 0 | 0 | 6 | 101 | 3 | 37 | 103 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 148 | 11 | 31 | 6 | 0 | 0 | 0 | 0 | 0 | 0 ; | 3 5 | 51 | 356 |
| 17:4 | 2 | 43 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 50 | 49 | 34 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 90 | 1 | 38 | 93 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 142 | 12 | 37 | 5 | 0 | 0 | 0 | 0 | 0 | 0 4 | 4 5 | 58 | 340 |
| | | | · | · | | | | · | | - Y | | | | | | | | | | | | | | | · | · | · | | | | | | | · | | | | · | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |





Turning Movement Count Diagram

Intersection: Dunlop Street & Mulcaster Street

Municipality: Barrie, Ontario

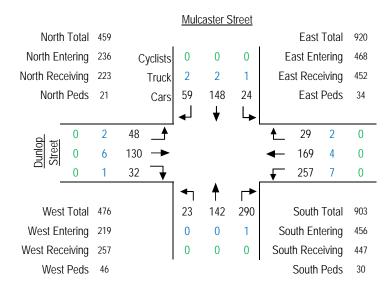
Intersection ID:

Date: Tuesday March 19, 2019

MD Peak Hour: 12:30 to 13:30

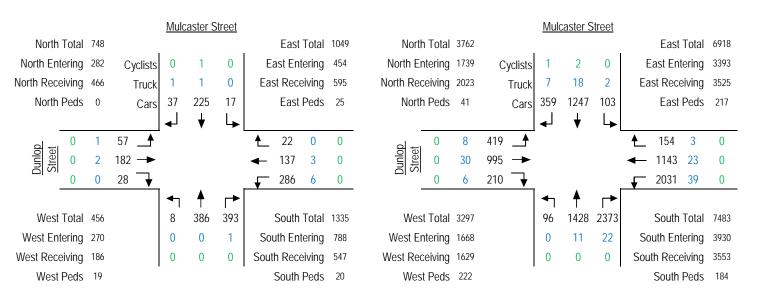
AM Peak Hour: 7:30 to 8:30

Mulcaster Street North Total 423 East Total 865 North Entering 160 0 East Entering 500 Cyclists 0 North Receiving 263 4 0 East Receiving 365 Truck North Peds 25 129 2 East Peds 12 Cars 0 1 48 16 0 Street 6 79 153 3 0 0 0 0 16 325 2 0 West Total 340 9 197 275 South Total 960 0 West Entering 150 0 3 South Entering West Receiving 190 0 0 0 South Receiving 476 West Peds 13 South Peds



PM Peak Hour: 16:00 to 17:00

Total 8-Hour Count





| Morning Peak Diagram | Specified Period One Hour Peal From: 6:00:00 From: 8:00:00 To: 9:00:00 To: 9:00:00 | k |
|--|--|----------------------|
| Municipality: Barrie Site #: 1721300001 ntersection: Dunlop St & Owen St FFR File #: 1 Count date: 11-Oct-17 ** Non-Signalized Intersection ** | Weather conditions: Person counted: Person prepared: Person checked: Major Road: Dunlop St runs W/E | |
| North Leg Total: 77 North Entering: 41 North Peds: 39 Peds Cross: ✓ Totals Heavys Trucks Cars Totals 4 3 190 197 Dunlop St | Heavys 1 Trucks 0 Cars 35 Totals 36 Cars Trucks Heavys 1 Cars Trucks Heavys 15 0 0 160 2 2 | 179 2 K |
| Heavys Trucks Cars Totals 1 | Dunlop St Cars Trucks Heavys 181 3 8 | Totals |
| Peds Cross: X West Peds: 2 West Entering: 205 West Leg Total: 402 | | |



| Afternoon Peak Diagram | Specified Period One Hour Peak From: 16:00:00 From: 16:30:00 To: 19:00:00 To: 17:30:00 |
|--|--|
| Municipality: Barrie Site #: 1721300001 ntersection: Dunlop St & Owen St FFR File #: 1 Count date: 11-Oct-17 * Non-Signalized Intersection ** | Weather conditions: Person counted: Person prepared: Person checked: Major Road: Dunlop St runs W/E |
| North Leg Total: 143 North Entering: 70 North Peds: 118 Peds Cross: Totals 62 Heavys Trucks Cars Totals 0 2 273 275 Dunlop St The avys Total: 143 Dunlop St Dunlop St | Heavys 0 |
| Heavys Trucks Cars Totals 0 0 48 48 319 1 1 365 | Dunlop St Cars Trucks Heavys Total 325 1 1 327 |
| Peds Cross: X West Peds: 0 West Entering: 367 West Leg Total: 642 | |



Total Count Diagram

Municipality: Barrie

Site #: 1721300001

Intersection: Dunlop St & Owen St

TFR File #:

Count date: 11-Oct-17 Weather conditions:

Person counted: Person prepared:

Person checked:

** Non-Signalized Intersection **

Totals

1256

Dunlop St

North Leg Total: 562 North Entering: 294 North Peds: 357

Heavys Trucks Cars

13

Peds Cross:

1232

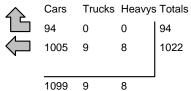






Major Road: Dunlop St runs W/E

Heavys 4 East Leg Total: 2326 Trucks 0 East Entering: Cars 264 East Peds: Totals 268 Peds Cross:



Heavys Trucks Cars Totals 0 170 174 15 1127 1150 19 1297



Owen St



1116

X

Cars Trucks Heavys Totals 1186 8 16 1210

X Peds Cross: West Peds: West Entering: 1324 West Leg Total: 2580



Accu-Traffic Inc. Traffic Count Summary

| Intersection: | North Approach Totals Hour Includes Cars, Trucks, & Heavys Total Fording Reads Read | | | | | | | | | | | | | | |
|---------------|--|------------|-------------------|-------------------|---------------|-----------------------|----------------------|-----------|-------------|------------|------------|-------|--|--|--|
| - | | | | als | | | | | | ach To | als | | | | |
| Hour | | | | | Total | | Hour | | | | | Total | | | |
| Ending | Left | | | Grand | Peds | Approaches | Ending | | | | Grand | Peds | | | |
| 6:00:00 | 0 | Thru O | Right <i>0</i> | Total 0 | 0 | 0 | 6:00:00 | Left 0 | Thru O | Right 0 | Total 0 | 0 | | | |
| 7:00:00 | 3 | 0 | 10 | 13 | 4 | 13 | 7:00:00 | 0 | 0 | 0 | 0 | 0 | | | |
| 8:00:00 | 3 | 0 | 22 | 25 | 26 | 25 | 8:00:00 | Ö | Ö | Ö | Ö | Ö | | | |
| 9:00:00 | 8 | Ō | 33 | 41 | 39 | 41 | 9:00:00 | O | Ō | Ō | Ō | Ō | | | |
| 16:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 16:00:00 | | 0 | 0 | 0 | 0 | | | |
| 17:00:00 | 11 | 0 | 57 | 68 | 83 | 68 | 17:00:00 | | 0 | 0 | 0 | 0 | | | |
| 18:00:00 | 16 | 0 | 57 | 73 | 111 | 73 | 18:00:00 | | 0 | 0 | 0 | 0 | | | |
| 19:00:00 | 19 | 0 | 55 | 74 | 94 | 74 | 19:00:00 | 0 | 0 | 0 | 0 | 0 | | | |
| | | | | | | | | | | | | | | | |
| Totals: | Fotals: 60 0 234 294 357 294 S Totals: 0 0 0 0 0 East Approach Totals Feet/West West Approach Totals | | | | | | | | | | | | | | |
| Hour | Include | es Cars. T | rucks, & H | leavvs | Total | East/West | Hour | | | rucks, & F | | Total | | | |
| Ending | | | | Grand | Peds | Total Approaches | Ending | | | | Grand | Peds | | | |
| 6:00:00 | Left O | Thru O | Right | Total 0 | 0 | 0 | 6:00:00 | Left 0 | Thru O | Right 0 | Total 0 | 0 | | | |
| 7:00:00 | 0 | 105 | 0 1 | 106 | 0 | 164 | 7:00:00 | 6 | 52 | 0 | 58 | 0 | | | |
| 8:00:00 | 0 | 138 | 8 | 146 | 0 | 263 | 8:00:00 | 12 | 105 | Ö | 117 | Ö | | | |
| 9:00:00 | Ö | 164 | 15 | 179 | 2 | 384 | 9:00:00 | 21 | 184 | Ö | 205 | 2 | | | |
| 16:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 16:00:00 | | 0 | 0 | 0 | 0 | | | |
| 17:00:00 | 0 | 199 | 21 | 220 | 0 | <i>540</i> | 17:00:00 | | 277 | 0 | 320 | 0 | | | |
| 18:00:00 | 0 | 212 | 25 | 237 | 1 | 572 | 18:00:00 | | 292 | 0 | 335 | 0 | | | |
| 19:00:00 | 0 | 204 | 24 | 228 | 1 | 517 | 19:00:00 | 49 | 240 | 0 | 289 | 2 | | | |
| | | | | | | | | | | | | | | | |
| Totals: | 0 | 1022 | 94 Calc | 1116 culated \ | 4 /alues f | 2440 or Traffic Cr | W Totals ossing N | | 1150 eet | 0 | 1324 | 4 | | | |
| Hours Er | ndina: | 6:00 | 7:00 | 8:00 | 9:00 | J. 1141110 OI | 16:00 | 17:00 | 18:00 | 19:00 | | | | | |
| Crossing | | | 3 | 3 | 9.00 12 | | 0 | 11.00 | 17 | 22 | | | | | |
| | | - | - | - | _ | | - | | - | _ | | | | | |



| | Passenger Cars - North Approach | | | | | | | Truc | cks - Nort | h Approa | ach | | | He | avys - No | rth Appr | oach | | Pedes | trians |
|----------|---------------------------------|------|-----|------|-----|------|-----|------|------------|----------|-----|------|-----|------|-----------|----------|------|------|-------|--------|
| Interval | Le | eft | Th | ru | Rig | ght | Le | eft | Th | ru | Rig | ght | Le | ft | Th | ru | Rig | ght | North | Cross |
| Time | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 6:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15:00 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30:00 | 1 | 1 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 6:45:00 | 2 | 1 | 0 | 0 | 6 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 3 | 2 |
| 7:00:00 | 2 | 0 | 0 | 0 | 9 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 4 | 1 |
| 7:15:00 | 2 | 0 | 0 | 0 | 10 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 12 | 8 |
| 7:30:00 | 3 | 1 | 0 | 0 | 19 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 17 | 5 |
| 7:45:00 | 4 | 1 | 0 | 0 | 26 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 28 | 11 |
| 8:00:00 | 5 | 1 | 0 | 0 | 31 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 30 | 2 |
| 8:15:00 | 10 | 5 | 0 | 0 | 36 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 11 | 0 | 38 | 8 |
| 8:30:00 | 10 | 0 | 0 | 0 | 46 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 42 | 4 |
| 8:45:00 | 10 | 0 | 0 | 0 | 56 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 1 | 48 | 6 |
| 9:00:00 | 13 | 3 | 0 | 0 | 61 | 5 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 3 | 1 | 69 | 21 |
| 9:15:00 | 13 | 0 | 0 | 0 | 61 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 69 | 0 |
| 16:00:00 | 13 | 0 | 0 | 0 | 61 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 69 | 0 |
| 16:15:00 | 15 | 2 | 0 | 0 | 74 | 13 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 80 | 11 |
| 16:30:00 | 19 | 4 | 0 | 0 | 85 | 11 | 0 | 0 | 0 | 0 | 3 | 2 | 1 | 0 | 0 | 0 | 3 | 0 | 95 | 15 |
| 16:45:00 | 21 | 2 | 0 | 0 | 100 | 15 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 124 | 29 |
| 17:00:00 | 24 | 3 | 0 | 0 | 116 | 16 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 152 | 28 |
| 17:15:00 | 26 | 2 | 0 | 0 | 133 | 17 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 188 | 36 |
| 17:30:00 | 27 | 1 | 0 | 0 | 147 | 14 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 213 | 25 |
| 17:45:00 | 31 | 4 | 0 | 0 | 155 | 8 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 244 | 31 |
| 18:00:00 | 40 | 9 | 0 | 0 | 172 | 17 | 0 | 0 | 0 | 0 | 4 | 1 | 1 | 0 | 0 | 0 | 3 | 0 | 263 | 19 |
| 18:15:00 | 48 | 8 | 0 | 0 | 182 | 10 | 0 | 0 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 294 | 31 |
| 18:30:00 | 49 | 1 | 0 | 0 | 198 | 16 | 0 | 0 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 312 | 18 |
| 18:45:00 | 53 | 4 | 0 | 0 | 213 | 15 | 0 | 0 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 337 | 25 |
| 19:00:00 | 59 | 6 | 0 | 0 | 227 | 14 | 0 | 0 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 357 | 20 |
| 19:15:00 | 59 | 0 | 0 | 0 | 227 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 357 | 0 |
| 19:15:15 | 59 | 0 | 0 | 0 | 227 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 357 | 0 |
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| Count | Date: | | | | 172130 | UUUT | 1 | | | | | | | | | | | | 1 | |
|----------------------|-------|--------|------------|-----------|----------|----------|-----|------|-----------|----------|-----|------|-----|------|------------|-----------|-----|------|--------|--------|
| | | Passen | ger Cars | - East Ap | proach | | | Tru | cks - Eas | t Approa | ch | | | He | eavys - Ea | ast Appro | | | Pedes | trians |
| Interval | Le | eft | Th | ru | Riç | ght | Le | eft | Th | ru | Rig | ght | Le | eft | Th | ru | Ri | ght | East (| ross |
| Time | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 6:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15:00 | 0 | 0 | 20 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 |
| 6:30:00 | 0 | 0 | 42 | 22 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| 6:45:00 | 0 | 0 | 67 | 25 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| 7:00:00 | 0 | 0 | 102 | 35 | 1 | 11 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| 7:15:00 | 0 | 0 | 127 | 25 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| 7:30:00 | 0 | 0 | 164 | 37 | 2 | 1 | 0 | 0 | 2 | 11 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| 7:45:00 | 0 | 0 | 199 | 35 | 5 | 3 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 3 | 11 | 0 | 0 | 0 | 0 |
| 8:00:00 | 0 | 0 | 236 | 37 | 9 | 4 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 5 | 2 | 0 | 0 | 0 | 0 |
| 8:15:00 | 0 | 0 | 271 | 35 | 10 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 7 | 2 | 0 | 0 | 0 | 0 |
| 8:30:00 | 0 | 0 | 316 | 45 | 15 | 5 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 |
| 8:45:00 | 0 | 0 | 356 | 40 | 18 | 3 | 0 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 1 | 1 |
| 9:00:00 | 0 | 0 | 396 | 40 | 24 | 6 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 2 | 1 |
| 9:15:00 | 0 | 0 | 396 | 0 | 24 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 2 | 0 |
| 16:00:00 | 0 | 0 | 396 | 0 | 24 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 2 | 0 |
| 16:15:00 | 0 | 0 | 439 | 43 | 27 | 3 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 2 | 0 |
| 16:30:00 | 0 | 0 | 487 | 48 | 33 | 6 | 0 | 0 | 7 | 2 | 0 | 0 | 0 | 0 | 8 | 1 | 0 | 0 | 2 | 0 |
| 16:45:00 | 0 | 0 | 540 | 53 | 37 | 4 | 0 | 0 | 8 | 1 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 2 | 0 |
| 17:00:00 | 0 | 0 | 589 | 49 | 45 | 8 | 0 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 2 | 0 |
| 17:15:00 | 0 | 0 | 652 | 63 | 50 | 5 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 2 | 0 |
| 17:30:00 | 0 | 0 | 698 | 46 | 58 | 8 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 3 | 1 |
| 17:45:00 18:00:00 | 0 | 0 | 746 801 | 48 55 | 65 70 | 7 5 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 3 | 0 |
| 18:15:00 | 0 | 0 | 860 | 55 | 73 | 3 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 8 8 | 0 | 0 | 0 | 3 | 0 |
| 18:30:00 | 0 | 0 | 905 | 45 | 78 | <u>5</u> | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 3 | 0 |
| 18:45:00 | 0 | 0 | 959 | 54 | 85 | 5 7 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 3 | 0 |
| 19:00:00 | 0 | 0 | 1005 | 46 | 94 | 9 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 4 | 1 |
| 19:00:00 | 0 | 0 | 1005 | 0 | 94 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 4 | 0 |
| 19:15:15 | 0 | 0 | 1005 | 0 | 94 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 4 | 0 |
| 19.13.13 | | 0 | 1003 | 0 | 94 | U | - | - 0 | " | U | - 0 | - 0 | 0 | U | 0 | - 0 | " | - 0 | - 4 | |
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| Count | t Date: | 11-UCt- | 17 | Site #: | 172130 | 0001 | T | | | | | | 1 | | | | | | 1 | |
|----------------------|---------|---------|-----------|---------|---------|------|-----|------|-----------|---------|-----|------|-----|------|-----------|----------|------|------|-------|--------|
| | | Passeng | er Cars - | South A | pproach | | | Truc | ks - Sout | h Appro | ach | | | He | avys - So | uth Appr | oach | | Pedes | trians |
| Interval | Le | eft | Th | ru | Rig | ght | Le | eft | Th | ru | Ri | ght | Le | eft | Th | ru | Ri | ght | South | Cross |
| Time | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 6:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
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| 8:15:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
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| 9:15:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
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| 16:30:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:45:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:15:00 17:30:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:45:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18:15:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18:30:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18:45:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19:15:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19:15:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | ō | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10.10.10 | | | | | | | | | | | | | | | | | | | | |
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| Count | Date: | | | | 172130 | UUU I | | - | -1 \4/ | . 4 . 4 | | | | | | | b | | D- 1- | |
|--------------------|----------|----------|------------|----------|----------|-------|-----|----------|-----------|---------|-----|------|-----|------|----------|------|-----|---------|-------|------|
| | | | ger Cars - | | <u> </u> | | | | cks - Wes | | | | | | avys - W | | | | Pedes | |
| Interval Time | Le | | Th | | Rig | | Le | | Th | | ` | ght | Le | | Th | | | ght | West | |
| | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 6:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15:00 | 1 | 11 | 5 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30:00 | 2 | 1 | 17 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45:00 | 3 | 1 | 36 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00:00 | 4 | 1 | 50 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 2 | 0 | 0 | 0 | 0 |
| 7:15:00 | 5 | 1 | 70 | 20 | 0 | 0 | 0 | 0 | 1 | 11 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| 7:30:00 | 6 | 7 | 85 | 15 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 2 | 0 | 3 | 1 | 0 | 0 | 0 | 0 |
| 7:45:00 8:00:00 | 13 16 | 3 | 114 150 | 29 36 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 2 2 | 0 | 3 5 | 2 | 0 | 0 | 0 | 0 |
| 8:15:00 | 21 | <u> </u> | 186 | 36 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 2 | 0 | 7 | 2 | 0 | 0 | 0 | 0 |
| 8:30:00 | 26 | 5 | 230 | 44 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 2 | 0 | 9 | 2 | 0 | 0 | 0 | 0 |
| 8:45:00 | 31 | 5 | 281 | 51 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 3 | 1 | 11 | 2 | 0 | 0 | 1 | 1 |
| 9:00:00 | 36 | 5 | 323 | 42 | 0 | 0 | 0 | 0 | 5 | 2 | 0 | 0 | 3 | 0 | 13 | 2 | 0 | 0 | 2 | 1 |
| 9:15:00 | 36 | 0 | 323 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 3 | 0 | 13 | 0 | 0 | 0 | 2 | 0 |
| 16:00:00 | 36 | 0 | 323 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 3 | 0 | 13 | 0 | Ö | 0 | 2 | 0 |
| 16:15:00 | 43 | 7 | 380 | 57 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 3 | 0 | 14 | 1 | ō | 0 | 2 | 0 |
| 16:30:00 | 55 | 12 | 434 | 54 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 4 | 1 | 14 | 0 | 0 | 0 | 2 | 0 |
| 16:45:00 | 65 | 10 | 514 | 80 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 4 | 0 | 15 | 1 | 0 | 0 | 2 | 0 |
| 17:00:00 | 78 | 13 | 598 | 84 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 4 | 0 | 15 | 0 | 0 | 0 | 2 | 0 |
| 17:15:00 | 89 | 11 | 673 | 75 | 0 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 4 | 0 | 15 | 0 | 0 | 0 | 2 | 0 |
| 17:30:00 | 103 | 14 | 751 | 78 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 4 | 0 | 15 | 0 | 0 | 0 | 2 | 0 |
| 17:45:00 | 115 | 12 | 821 | 70 | 0 | 0 | 0 | 0 | 7 | 1 | 0 | 0 | 4 | 0 | 15 | 0 | 0 | 0 | 2 | 0 |
| 18:00:00 | 121 | 6 | 887 | 66 | 0 | 0 | 0 | 0 | 8 | 1 | 0 | 0 | 4 | 0 | 15 | 0 | 0 | 0 | 2 | 0 |
| 18:15:00 | 129 | 8 | 944 | 57 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 4 | 0 | 15 | 0 | 0 | 0 | 2 | 0 |
| 18:30:00 | 141 | 12 | 1002 | 58 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 4 | 0 | 15 | 0 | 0 | 0 | 2 | 0 |
| 18:45:00 | 155 | 14 | 1075 | 73 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 4 | 0 | 15 | 0 | 0 | 0 | 2 | 0 |
| 19:00:00 | 170 | 15 | 1127 | 52 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 4 | 0 | 15 | 0 | 0 | 0 | 4 | 2 |
| 19:15:00 | 170 | 0 | 1127 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 4 | 0 | 15 | 0 | 0 | 0 | 4 | 0 |
| 19:15:15 | 170 | 0 | 1127 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 4 | 0 | 15 | 0 | 0 | 0 | 4 | 0 |
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| | | ACCU | -11a | | 1116. | | | | |
|--|---|---------------------|------------------------------------|-------------------------|-----------------------------------|---------------------|-----------------------|---|-----------------------|
| Morning Pe | ak Diag | ram | F | Specifi From: To: | ed Perio 6:00:00 9:00:00 | od | One H From: To: | | 0 |
| | 300002 r St & Owen S | t | F | Person Person | counte prepare checke | d: ed: | | | |
| ** Signalized Inters | ection ** | | | Major F | Road: | Collier St | runs W/E | | |
| North Leg Total: 120 North Entering: 46 North Peds: 16 Peds Cross: Heavys Trucks Cars Tota 5 0 156 161 | Heavys 2 Trucks 0 Cars 14 Totals 16 Cals | 1 0 0 0 18 11 19 11 | Ower | n St ► E | Heavys Truck Cars Totals | s 0 s 74 s 74 | East East Peds | Leg Total: Entering: Peds: Cross: cks Heavy 0 3 0 3 | 165 20 X |
| Heavys Trucks Cars Tota 0 0 36 36 8 1 148 157 1 1 22 24 9 2 206 | | | S wen St | - 1 | | | | cks Heavy 8 | es Totals 174 |
| Peds Cross: X West Peds: 36 West Entering: 217 West Leg Total: 378 | Cars 52 Trucks 1 Heavys 2 Totals 55 | _ | Cars Trucks Heavys Totals | 0 0 | | 36 0 0 | South | Cross: n Peds: n Entering: n Leg Tota | |



| Afternoon | Peak Dia | agrai | m | Speci From: To: | : 16 | Period :00:00 :00:00 | | ne Hour Pe om: 16:15: o: 17:15: | 00 |
|---|-----------------------------------|--------------------|-------------|-------------------------|---------------|--|--------------------|---------------------------------------|---------------------|
| Intersection: Collie FFR File #: 1 Count date: 11-C | 300002 er St & Owen S ct-17 | it | | Perso Perso Perso | n co on pr | onditions ounted: epared: necked: | | | |
| North Leg Total: 149 North Entering: 62 | Heavys 2 | • | 0 2 | Major | Roa | Heavys 1 Trucks 1 | St run | East Leg Total: East Entering: | 498 242 |
| North Peds: 24 Peds Cross: ► | Cars 25 Totals 27 | 14 | 21 60 21 | 1 | | Cars 85 Totals 87 | _ [| East Peds: Peds Cross: | 29 X |
| Heavys Trucks Cars To | cals 3 Collier St | $\hat{\mathbb{T}}$ | w V | wen St | | (- | Cars 20 206 13 239 | Trucks Heavy 0 0 1 2 0 0 | zs Total: 20 209 13 |
| 0 1 43 44 6 1 212 219 0 2 31 33 | rals \triangle | | S | 5 | \wedge | | ollier St Cars | Trucks Heavy | vs Total: |
| 6 4 286 Peds Cross: | Cars 58 | | | rs 22 ks 0 | 22 0 | 16 60 0 0 | 249 | 1 6 Peds Cross: South Peds: | 256 ⋈ 31 |
| West Entering: 296 West Leg Total: 554 | Heavys 0 | _ 1 | Heavy | | 1 23 | 0 16 | | South Entering South Leg Tota | : 61 |



Total Count Diagram

Municipality: Barrie

Site #: 1721300002

Intersection: Collier St & Owen St

TFR File #:

Count date: 11-Oct-17 Weather conditions:

Person counted: Person prepared:

Person checked:

** Signalized Intersection **

North Leg Total: 535 North Entering: 215 North Peds: Peds Cross:

Heavys 12 0 13 0 Trucks 0 0 0 Cars 65 66 202 Totals 77

Heavys 3

Trucks 1 Cars 316 Totals 320

Major Road: Collier St runs W/E

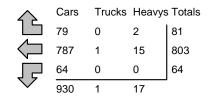
East Leg Total: 1937 East Entering: 948 East Peds: 96 X Peds Cross:

Totals Heavys Trucks Cars 970 28 941





Owen St



Collier St

Heavys Trucks Cars Totals 1 162 163 35 2 802 839 3 4 143 150 1107



Collier St



Cars Trucks Heavys Totals 951 36 989

X Peds Cross: West Peds: 222 West Entering: 1152 West Leg Total: 2122

Cars 278 Trucks 4 Heavys Totals 286

247 Cars 89 75 83 0 Trucks 0 0 0 3 Heavys 1 1 Totals 90 76 84

Peds Cross: ⋈ South Peds: 133 South Entering: 250 South Leg Total: 536



Accu-Traffic Inc. Traffic Count Summary

| Intersection: (| Collier S | St & Owe | en St | | Count D | Date: 11-Oct-17 | 7 Muni | cipality: Ba | arrie | | | |
|----------------------|---------------------|--------------------------------------|----------------|----------------|---------|---------------------------|----------------------|--------------|------------------------------------|------------|----------------|-----------------|
| | | | ach Tot | | | North/South | | | h Appro | | | |
| Hour | Includ | es Cars, T | rucks, & F | | Total | Total | Hour | Includ | es Cars, T | rucks, & H | | Total |
| Ending | Left | Thru | Right | Grand Total | Peds | Approaches | Ending | Left | Thru | Right | Grand Total | Peds |
| 6:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 6:00:00 | 0 | 0 | 0 | 0 | 0 |
| 7:00:00 | 0 | 3 | 3 | 6 | 1 | 13 | 7:00:00 | 4 | 2 | 1 | 7 | 4 |
| 8:00:00 | 4 | 4 | 4 | 12 | 6 | 32 | 8:00:00 | 9 | 5 | 6 | 20 | 6 |
| 9:00:00 | 11 | 19 | 16 | 46 | 16 | 82 | 9:00:00 | 8 | 22 | 6 | 36 | 33 |
| 16:00:00 17:00:00 | 0 21 | 0 15 | 0 26 | 0 62 | 0 29 | 0 121 | 16:00:00 17:00:00 | | 0 22 | 0 15 | <i>0</i> 59 | 0 4 5 |
| 18:00:00 | 20 | 17 | 17 | 54 | 18 | 120 | 18:00:00 | | 16 | 31 | 66 | 4 3 |
| 19:00:00 | 10 | 14 | 11 | 35 | 17 | 97 | 19:00:00 | | 9 | 25 | 62 | 18 |
| | | | | | | | | | | | | |
| Totals: | 66 Eas Includ | 72 t Appro a es Cars, T | 77 ach Tota | leavys | 87 | 465 East/West Total | S Totals: | Wes | 76 t Appro es Cars, T | | leavys | 133 Total |
| Ending | Left | Thru | Right | Grand Total | Peds | Approaches | Ending | Left | Thru | Right | Grand Total | Peds |
| 6:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 6:00:00 | 0 | 0 | 0 | 0 | 0 |
| 7:00:00 | 2 | 43 | 5 | 50 | 0 | 95 | 7:00:00 | 3 | 31 | 11 | 45 | 3 |
| 8:00:00 | 2 | 84 | 8 | 94 | 6 | 188 | 8:00:00 | 10 | 66 | 18 | 94 | 7 |
| 9:00:00 | 12 | 137 | 16 | 165 | 20 | 382 | 9:00:00 | 36 | 157 | 24 | 217 | 36 |
| 16:00:00 17:00:00 | 0 14 | 0 206 | 0 17 | 0 237 | 0 30 | 0 514 | 16:00:00 17:00:00 | | 0 204 | 0 31 | 0 277 | 0 80 |
| 18:00:00 | 18 | 186 | 20 | 224 | 26 | 522 | 18:00:00 | | 227 | 27 | 298 | 56 |
| 19:00:00 | 16 | 147 | 15 | 178 | 14 | 399 | 19:00:00 | | 154 | 39 | 221 | 40 |
| | | | | | | | | | | | | |
| Totals: | 64 | 803 | | | | 2100 or Traffic Cr | _ | ajor Str | | 150 | 1152 | 222 |
| | ndina: | 6:00 | 7:00 | 8:00 | 9:00 | | 16:00 | 17:00 | 18:00 | 19:00 | | |
| Hours En | | | 10 | 31 | 97 | | 0 | 175 | 138 | 106 | | |



| | Date: | Passeng | ger Cars - | | pproach | | | True | cks - Nort | h Approa | ach | | | He | avys - No | rth Appr | oach | | Pedes | trians |
|----------|-------|---------|------------|------|---------|------|-----|------|------------|----------|-----|------|-----|------|-----------|----------|------|------|-------|--------|
| Interval | Le | eft | Th | ru | Riç | ght | Le | eft | Th | ru | Riç | ght | Le | ft | Th | ru | Riç | ght | North | Cross |
| Time | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 6:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 |
| 6:30:00 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| 6:45:00 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 1 | 1 |
| 7:00:00 | 0 | 0 | 3 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 |
| 7:15:00 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 2 | 1 |
| 7:30:00 | 0 | 0 | 4 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 4 | 2 |
| 7:45:00 | 0 | 0 | 6 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 1 | 7 | 3 |
| 8:00:00 | 4 | 4 | 7 | 1 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 7 | 0 |
| 8:15:00 | 6 | 2 | 14 | 7 | 6 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 9 | 2 |
| 8:30:00 | 9 | 3 | 19 | 5 | 10 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 17 | 8 |
| 8:45:00 | 13 | 4 | 22 | 3 | 14 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 1 | 20 | 3 |
| 9:00:00 | 15 | 2 | 25 | 3 | 17 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 6 | 0 | 23 | 3 |
| 9:15:00 | 15 | 0 | 25 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 6 | 0 | 23 | 0 |
| 16:00:00 | 15 | 0 | 25 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 6 | 0 | 23 | 0 |
| 16:15:00 | 19 | 4 | 29 | 4 | 21 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 7 | 11 | 31 | 8 |
| 16:30:00 | 26 | 7 | 34 | 5 | 28 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 7 | 0 | 41 | 10 |
| 16:45:00 | 31 | 5 | 37 | 3 | 34 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 8 | 11 | 48 | 7 |
| 17:00:00 | 36 | 5 | 40 | 3 | 41 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 8 | 0 | 52 | 4 |
| 17:15:00 | 40 | 4 | 43 | 3 | 46 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 9 | 1 | 55 | 3 |
| 17:30:00 | 45 | 5 | 45 | 2 | 50 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 9 | 0 | 67 | 12 |
| 17:45:00 | 52 | 7 | 49 | 4 | 54 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 10 | 1 | 68 | 1 |
| 18:00:00 | 56 | 4 | 57 | 8 | 56 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 10 | 0 | 70 | 2 |
| 18:15:00 | 61 | 5 | 59 | 2 | 56 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 11 | 11 | 75 | 5 |
| 18:30:00 | 63 | 2 | 61 | 2 | 60 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 11 | 0 | 81 | 6 |
| 18:45:00 | 63 | 0 | 68 | 7 | 61 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 12 | 1 | 85 | 4 |
| 19:00:00 | 66 | 3 | 71 | 3 | 65 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 12 | 0 | 87 | 2 |
| 19:15:00 | 66 | 0 | 71 | 0 | 65 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 12 | 0 | 87 | 0 |
| 19:15:15 | 66 | 0 | 71 | 0 | 65 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 12 | 0 | 87 | 0 |
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| Count | Date: 11-Oct-17 Site #: 17213000 Passenger Cars - East Approach | | | | | | | | | | | | | | | | | | | |
|----------|--|--------|----------|-----------|--------|------|-----|------|-----------|----------|-----|------|-----|------|------------|-----------|------|------|--------|--------|
| | | Passen | ger Cars | - East Ap | proach | | | Tru | cks - Eas | t Approa | ch | | | He | eavys - Ea | ast Appro | pach | | Pedes | trians |
| Interval | Le | eft | Th | ru | Riç | ght | Le | eft | Th | ru | Ri | ght | Le | eft | Th | ru | Rig | ght | East (| Cross |
| Time | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 6:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15:00 | 1 | 1 | 7 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 2 | 0 | 0 |
| 6:30:00 | 1 | 0 | 22 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 2 | 0 | 0 | 0 |
| 6:45:00 | 2 | 1 | 35 | 13 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 |
| 7:00:00 | 2 | 0 | 39 | 4 | 3 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 2 | 2 | 0 | 0 | 0 |
| 7:15:00 | 3 | 1 | 57 | 18 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 2 | 0 | 1 | 1 |
| 7:30:00 | 3 | 0 | 74 | 17 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 11 | 2 | 0 | 1 | 0 |
| 7:45:00 | 4 | 11 | 96 | 22 | 5 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 2 | 0 | 4 | 3 |
| 8:00:00 | 4 | 0 | 121 | 25 | 11 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 1 | 2 | 0 | 6 | 2 |
| 8:15:00 | 4 | 0 | 146 | 25 | 18 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 1 | 2 | 0 | 10 | 4 |
| 8:30:00 | 5 | 1 | 176 | 30 | 21 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 2 | 0 | 16 | 6 |
| 8:45:00 | 12 | 7 | 209 | 33 | 22 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 1 | 2 | 0 | 18 | 2 |
| 9:00:00 | 16 | 4 | 255 | 46 | 27 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 11 | 2 | 0 | 26 | 8 |
| 9:15:00 | 16 | 0 | 255 | 0 | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 2 | 0 | 26 | 0 |
| 16:00:00 | 16 | 0 | 255 | 0 | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 2 | 0 | 26 | 0 |
| 16:15:00 | 19 | 3 | 307 | 52 | 31 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 2 | 0 | 33 | 7 |
| 16:30:00 | 22 | 3 | 352 | 45 | 35 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 1 | 2 | 0 | 41 | 8 |
| 16:45:00 | 23 | 1 | 409 | 57 | 40 | 5 | 0 | 0 | 1 | 11 | 0 | 0 | 0 | 0 | 10 | 0 | 2 | 0 | 46 | 5 |
| 17:00:00 | 30 | 7 | 458 | 49 | 44 | 4 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 11 | 1 | 2 | 0 | 56 | 10 |
| 17:15:00 | 32 | 2 | 513 | 55 | 51 | 7 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 2 | 0 | 62 | 6 |
| 17:30:00 | 39 | 7 | 561 | 48 | 53 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 12 | 11 | 2 | 0 | 66 | 4 |
| 17:45:00 | 42 | 3 | 598 | 37 | 60 | 7 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 2 | 0 | 73 | 7 |
| 18:00:00 | 48 | 6 | 642 | 44 | 64 | 4 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 13 | 1 | 2 | 0 | 82 | 9 |
| 18:15:00 | 52 | 4 | 684 | 42 | 69 | 5 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 2 | 0 | 83 | 1 |
| 18:30:00 | 55 | 3 | 719 | 35 | 73 | 4 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 14 | 1 | 2 | 0 | 85 | 2 |
| 18:45:00 | 60 | 5 | 760 | 41 | 76 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 15 | 1 | 2 | 0 | 90 | 5 |
| 19:00:00 | 64 | 4 | 787 | 27 | 79 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 15 | 0 | 2 | 0 | 96 | 6 |
| 19:15:00 | 64 | 0 | 787 | 0 | 79 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 15 | 0 | 2 | 0 | 96 | 0 |
| 19:15:15 | 64 | 0 | 787 | 0 | 79 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 15 | 0 | 2 | 0 | 96 | 0 |
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| Count | Date: | 11-Oct- | 17 | Site #: | 172130 | 0002 | 1 | | | | | | | | | | | | 1 | |
|----------|-------|---------|-----------|---------|---------|------|-----|------|-----------|---------|-----|------|-----|------|-----------|----------|------|------|-------|--------|
| | | Passeng | er Cars - | South A | pproach | | | Truc | ks - Sout | h Appro | ach | | | He | avys - So | uth Appr | oach | | Pedes | trians |
| Interval | Le | eft | Th | ru | Riç | ght | Le | eft | Th | ru | Rig | ght | Le | ft | Th | ru | Rig | ght | South | Cross |
| Time | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 6:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15:00 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 |
| 6:30:00 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 1 | 0 |
| 6:45:00 | 2 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 |
| 7:00:00 | 3 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 4 | 3 |
| 7:15:00 | 4 | 1 | 2 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 4 | 0 |
| 7:30:00 | 5 | 1 | 2 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 6 | 2 |
| 7:45:00 | 11 | 6 | 3 | 1 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 6 | 0 |
| 8:00:00 | 12 | 1 | 7 | 4 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 10 | 4 |
| 8:15:00 | 14 | 2 | 10 | 3 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 16 | 6 |
| 8:30:00 | 14 | 0 | 19 | 9 | 8 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 11 | 0 | 27 | 11 |
| 8:45:00 | 17 | 3 | 27 | 8 | 9 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 33 | 6 |
| 9:00:00 | 20 | 3 | 29 | 2 | 12 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 43 | 10 |
| 9:15:00 | 20 | 0 | 29 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 43 | 0 |
| 16:00:00 | 20 | 0 | 29 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 43 | 0 |
| 16:15:00 | 25 | 5 | 32 | 3 | 16 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 60 | 17 |
| 16:30:00 | 33 | 8 | 37 | 5 | 21 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 1 | 0 | 75 | 15 |
| 16:45:00 | 37 | 4 | 42 | 5 | 22 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 82 | 7 |
| 17:00:00 | 42 | 5 | 50 | 8 | 27 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 88 | 6 |
| 17:15:00 | 47 | 5 | 54 | 4 | 32 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 91 | 3 |
| 17:30:00 | 52 | 5 | 60 | 6 | 44 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 100 | 9 |
| 17:45:00 | 57 | 5 | 64 | 4 | 54 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 107 | 7 |
| 18:00:00 | 61 | 4 | 66 | 2 | 58 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 115 | 8 |
| 18:15:00 | 64 | 3 | 70 | 4 | 61 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 118 | 3 |
| 18:30:00 | 68 | 4 | 73 | 3 | 68 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 121 | 3 |
| 18:45:00 | 78 | 10 | 73 | 0 | 75 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 131 | 10 |
| 19:00:00 | 89 | 11 | 75 | 2 | 83 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 133 | 2 |
| 19:15:00 | 89 | 0 | 75 | 0 | 83 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 133 | 0 |
| 19:15:15 | 89 | 0 | 75 | 0 | 83 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 133 | 0 |
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| | | Passen | ger Cars - | West Ap | proach | | | Tru | cks - Wes | t Approa | ch | | | Не | eavys - We | est Appr | oach | | Pedes | trians |
|----------|-----|--------|------------|---------|--------|------|-----|------|-----------|----------|-----|------|-----|------|------------|----------|------|------|-------|--------|
| Interval | Le | eft | Th | ru | Riç | ght | Le | eft | Th | ru | Riç | ght | Le | ft | Th | ru | Riç | ght | West | Cross |
| Time | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 6:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15:00 | 0 | 0 | 4 | 4 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 |
| 6:30:00 | 2 | 2 | 9 | 5 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 1 | 0 | 1 | 1 |
| 6:45:00 | 2 | 0 | 15 | 6 | 6 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 1 | 2 | 1 |
| 7:00:00 | 3 | 11 | 26 | 11 | 9 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 3 | 2 | 0 | 3 | 1 |
| 7:15:00 | 4 | 1 | 31 | 5 | 11 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 2 | 0 | 5 | 2 |
| 7:30:00 | 6 | 2 | 46 | 15 | 18 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 3 | 2 | 0 | 6 | 1 |
| 7:45:00 | 8 | 2 | 62 | 16 | 23 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 2 | 0 | 10 | 4 |
| 8:00:00 | 13 | 5 | 86 | 24 | 27 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 3 | 2 | 0 | 10 | 0 |
| 8:15:00 | 22 | 9 | 106 | 20 | 34 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 11 | 3 | 1 | 12 | 2 |
| 8:30:00 | 29 | 7 | 148 | 42 | 39 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 3 | 3 | 0 | 25 | 13 |
| 8:45:00 | 41 | 12 | 188 | 40 | 41 | 2 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 16 | 11 | 3 | 0 | 31 | 6 |
| 9:00:00 | 49 | 8 | 234 | 46 | 49 | 8 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 19 | 3 | 3 | 0 | 46 | 15 |
| 9:15:00 | 49 | 0 | 234 | 0 | 49 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 19 | 0 | 3 | 0 | 46 | 0 |
| 16:00:00 | 49 | 0 | 234 | 0 | 49 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 19 | 0 | 3 | 0 | 46 | 0 |
| 16:15:00 | 62 | 13 | 275 | 41 | 55 | 6 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 19 | 0 | 3 | 0 | 67 | 21 |
| 16:30:00 | 73 | 11 | 333 | 58 | 63 | 8 | 0 | 0 | 1 | 0 | 3 | 2 | 0 | 0 | 21 | 2 | 3 | 0 | 95 | 28 |
| 16:45:00 | 81 | 8 | 379 | 46 | 71 | 8 | 1 | 1 | 2 | 1 | 3 | 0 | 0 | 0 | 22 | 1 | 3 | 0 | 112 | 17 |
| 17:00:00 | 90 | 9 | 432 | 53 | 78 | 7 | 1 | 0 | 2 | 0 | 3 | 0 | 0 | 0 | 24 | 2 | 3 | 0 | 126 | 14 |
| 17:15:00 | 105 | 15 | 487 | 55 | 86 | 8 | 1 | 0 | 2 | 0 | 3 | 0 | 0 | 0 | 25 | 1 | 3 | 0 | 143 | 17 |
| 17:30:00 | 115 | 10 | 544 | 57 | 91 | 5 | 1 | 0 | 2 | 0 | 3 | 0 | 0 | 0 | 26 | 1 | 3 | 0 | 161 | 18 |
| 17:45:00 | 127 | 12 | 595 | 51 | 94 | 3 | 1 | 0 | 2 | 0 | 3 | 0 | 0 | 0 | 27 | 1 | 3 | 0 | 165 | 4 |
| 18:00:00 | 134 | 7 | 652 | 57 | 104 | 10 | 1 | 0 | 2 | 0 | 4 | 1 | 0 | 0 | 31 | 4 | 3 | 0 | 182 | 17 |
| 18:15:00 | 144 | 10 | 693 | 41 | 115 | 11 | 1 | 0 | 2 | 0 | 4 | 0 | 0 | 0 | 31 | 0 | 3 | 0 | 195 | 13 |
| 18:30:00 | 149 | 5 | 729 | 36 | 123 | 8 | 1 | 0 | 2 | 0 | 4 | 0 | 0 | 0 | 33 | 2 | 3 | 0 | 209 | 14 |
| 18:45:00 | 155 | 6 | 764 | 35 | 132 | 9 | 1 | 0 | 2 | 0 | 4 | 0 | 0 | 0 | 34 | 1 | 3 | 0 | 216 | 7 |
| 19:00:00 | 162 | 7 | 802 | 38 | 143 | 11 | 1 | 0 | 2 | 0 | 4 | 0 | 0 | 0 | 35 | 1 | 3 | 0 | 222 | 6 |
| 19:15:00 | 162 | 0 | 802 | 0 | 143 | 0 | 1 | 0 | 2 | 0 | 4 | 0 | 0 | 0 | 35 | 0 | 3 | 0 | 222 | 0 |
| 19:15:15 | 162 | 0 | 802 | 0 | 143 | 0 | 1 | 0 | 2 | 0 | 4 | 0 | 0 | 0 | 35 | 0 | 3 | 0 | 222 | 0 |
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Appendix B: Existing Operations

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|-------------------------------|------------|------------|-------|------|------------|------------|---------|-------|-------------|----------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ۲ | ∱ Љ | | ሻ | ∱ Ъ | | | 4 | 7 | | 414 | |
| Traffic Volume (vph) | 58 | 171 | 57 | 29 | 160 | 73 | 79 | 186 | 34 | 42 | 131 | 51 |
| Future Volume (vph) | 58 | 171 | 57 | 29 | 160 | 73 | 79 | 186 | 34 | 42 | 131 | 51 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | | 1.00 | 1.00 | | 0.95 | |
| Frt | 1.00 | 0.96 | | 1.00 | 0.95 | | | 1.00 | 0.85 | | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.99 | 1.00 | | 0.99 | |
| Satd. Flow (prot) | 1738 | 3346 | | 1738 | 3313 | | | 1803 | 1555 | | 3327 | |
| Flt Permitted | 0.53 | 1.00 | | 0.60 | 1.00 | | | 0.81 | 1.00 | | 0.84 | |
| Satd. Flow (perm) | 975 | 3346 | | 1094 | 3313 | | | 1477 | 1555 | | 2821 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 63 | 186 | 62 | 32 | 174 | 79 | 86 | 202 | 37 | 46 | 142 | 55 |
| RTOR Reduction (vph) | 0 | 31 | 0 | 0 | 54 | 0 | 0 | 0 | 27 | 0 | 40 | 0 |
| Lane Group Flow (vph) | 63 | 217 | 0 | 32 | 199 | 0 | 0 | 288 | 10 | 0 | 203 | 0 |
| Turn Type | pm+pt | NA | | Perm | NA | | pm+pt | NA | Perm | Perm | NA | |
| Protected Phases | 5 | 2 | | | 6 | | 3 | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | 27.2 | 27.2 | | 17.1 | 17.1 | | | 15.2 | 15.2 | | 15.2 | |
| Effective Green, g (s) | 27.2 | 27.2 | | 17.1 | 17.1 | | | 15.2 | 15.2 | | 15.2 | |
| Actuated g/C Ratio | 0.50 | 0.50 | | 0.31 | 0.31 | | | 0.28 | 0.28 | | 0.28 | |
| Clearance Time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 601 | 1673 | | 343 | 1041 | | | 412 | 434 | | 788 | |
| v/s Ratio Prot | 0.02 | c0.06 | | | c0.06 | | | | | | | |
| v/s Ratio Perm | 0.04 | | | 0.03 | | | | c0.19 | 0.01 | | 0.07 | |
| v/c Ratio | 0.10 | 0.13 | | 0.09 | 0.19 | | | 0.70 | 0.02 | | 0.26 | |
| Uniform Delay, d1 | 7.1 | 7.3 | | 13.2 | 13.6 | | | 17.6 | 14.2 | | 15.2 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 0.4 | 0.2 | | 0.5 | 0.4 | | | 5.1 | 0.0 | | 0.2 | |
| Delay (s) | 7.4 | 7.4 | | 13.7 | 14.0 | | | 22.7 | 14.2 | | 15.4 | |
| Level of Service | А | Α | | В | В | | | С | В | | В | |
| Approach Delay (s) | | 7.4 | | | 14.0 | | | 21.7 | | | 15.4 | |
| Approach LOS | | Α | | | В | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 14.7 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.39 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 54.4 | S | um of lost | time (s) | | | 16.0 | | | |
| Intersection Capacity Utiliza | ation | | 50.5% | IC | CU Level o | of Service | 9 | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

| Movement EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT SBF Lane Configurations Traffic Volume (vph) 59 120 20 334 162 17 9 205 284 15 173 20 | و |
|---|---------------------------|
| Traffic Volume (vph) 59 120 20 334 162 17 9 205 284 15 173 20 | Movement EB |
| | Lane Configurations |
| F | Traffic Volume (vph) 5 |
| Future Volume (vph) 59 120 20 334 162 17 9 205 284 15 173 2 | Future Volume (vph) 5 |
| Ideal Flow (vphpl) 1900 1900 1900 1900 1900 1900 1900 190 | Ideal Flow (vphpl) 190 |
| Total Lost time (s) 6.0 2.0 6.0 6.0 6.0 | Total Lost time (s) |
| Lane Util. Factor 1.00 1.00 1.00 1.00 1.00 1.00 | Lane Util. Factor |
| Frt 0.99 1.00 0.99 1.00 0.85 0.98 | Frt |
| Flt Protected 0.99 0.95 1.00 1.00 1.00 1.00 | Flt Protected |
| Satd. Flow (prot) 1778 1738 1804 1826 1555 1794 | Satd. Flow (prot) |
| Flt Permitted 0.85 0.62 1.00 0.98 1.00 0.96 | Flt Permitted |
| Satd. Flow (perm) 1537 1134 1804 1795 1555 1729 | Satd. Flow (perm) |
| Peak-hour factor, PHF 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 | Peak-hour factor, PHF 0.9 |
| Adj. Flow (vph) 64 130 22 363 176 18 10 223 309 16 188 28 | Adj. Flow (vph) 6 |
| RTOR Reduction (vph) 0 6 0 0 6 0 0 242 0 9 | RTOR Reduction (vph) |
| Lane Group Flow (vph) 0 210 0 363 188 0 0 233 67 0 223 | Lane Group Flow (vph) |
| Turn Type Perm NA pm+pt NA Perm NA Perm NA | Turn Type Peri |
| Protected Phases 2 1 6 8 4 | |
| Permitted Phases 2 6 8 4 | Permitted Phases |
| Actuated Green, G (s) 20.1 32.1 32.1 12.2 12.2 12.2 | Actuated Green, G (s) |
| Effective Green, g (s) 20.1 32.1 32.1 12.2 12.2 12.2 | Effective Green, g (s) |
| Actuated g/C Ratio 0.36 0.57 0.57 0.22 0.22 0.22 | Actuated g/C Ratio |
| Clearance Time (s) 6.0 2.0 6.0 6.0 6.0 | |
| Vehicle Extension (s) 3.0 3.0 3.0 3.0 3.0 | Vehicle Extension (s) |
| Lane Grp Cap (vph) 548 753 1028 388 336 374 | Lane Grp Cap (vph) |
| v/s Ratio Prot c0.09 0.10 | v/s Ratio Prot |
| v/s Ratio Perm c0.14 0.19 c0.13 0.04 0.13 | v/s Ratio Perm |
| v/c Ratio 0.38 0.48 0.18 0.60 0.20 0.60 | v/c Ratio |
| Uniform Delay, d1 13.5 6.8 5.8 19.9 18.1 19.8 | Uniform Delay, d1 |
| Progression Factor 1.00 1.00 1.00 1.00 1.00 1.00 | Progression Factor |
| Incremental Delay, d2 2.0 2.2 0.4 2.6 0.3 2.6 | Incremental Delay, d2 |
| Delay (s) 15.5 9.0 6.2 22.5 18.3 22.4 | |
| Level of Service B A A C B C | Level of Service |
| Approach Delay (s) 15.5 8.0 20.1 22.4 | |
| Approach LOS B A C C | Approach LOS |
| Intersection Summary | Intersection Summary |
| HCM 2000 Control Delay 15.5 HCM 2000 Level of Service B | HCM 2000 Control Delay |
| HCM 2000 Volume to Capacity ratio 0.46 | |
| Actuated Cycle Length (s) 56.3 Sum of lost time (s) 14.0 | |
| Intersection Capacity Utilization 67.6% ICU Level of Service C | |
| Analysis Period (min) 15 | Analysis Period (min) |

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| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ٦ | f) | | ሻ | 4 | | | 4 | | | 4 | |
| Traffic Volume (vph) | 37 | 274 | 25 | 12 | 261 | 16 | 8 | 23 | 6 | 11 | 20 | 16 |
| Future Volume (vph) | 37 | 274 | 25 | 12 | 261 | 16 | 8 | 23 | 6 | 11 | 20 | 16 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frt | 1.00 | 0.99 | | 1.00 | 0.99 | | | 0.98 | | | 0.95 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.99 | | | 0.99 | |
| Satd. Flow (prot) | 1789 | 1808 | | 1789 | 1867 | | | 1820 | | | 1701 | |
| Flt Permitted | 0.58 | 1.00 | | 0.56 | 1.00 | | | 0.91 | | | 0.91 | |
| Satd. Flow (perm) | 1086 | 1808 | | 1062 | 1867 | | | 1674 | | | 1560 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 40 | 298 | 27 | 13 | 284 | 17 | 9 | 25 | 7 | 12 | 22 | 17 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 2 | 0 | 0 | 6 | 0 | 0 | 16 | 0 |
| Lane Group Flow (vph) | 40 | 321 | 0 | 13 | 299 | 0 | 0 | 35 | 0 | 0 | 35 | 0 |
| Heavy Vehicles (%) | 2% | 5% | 4% | 2% | 2% | 2% | 2% | 2% | 2% | 2% | 5% | 12% |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 36.2 | 36.2 | | 36.2 | 36.2 | | | 3.9 | | | 3.9 | |
| Effective Green, g (s) | 36.2 | 36.2 | | 36.2 | 36.2 | | | 3.9 | | | 3.9 | |
| Actuated g/C Ratio | 0.69 | 0.69 | | 0.69 | 0.69 | | | 0.07 | | | 0.07 | |
| Clearance Time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 754 | 1256 | | 737 | 1297 | | | 125 | | | 116 | |
| v/s Ratio Prot | | c0.18 | | | 0.16 | | | | | | | |
| v/s Ratio Perm | 0.04 | | | 0.01 | | | | 0.02 | | | c0.02 | |
| v/c Ratio | 0.05 | 0.26 | | 0.02 | 0.23 | | | 0.28 | | | 0.30 | |
| Uniform Delay, d1 | 2.5 | 3.0 | | 2.5 | 2.9 | | | 22.8 | | | 22.8 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.1 | 0.5 | | 0.0 | 0.4 | | | 1.2 | | | 1.5 | |
| Delay (s) | 2.7 | 3.4 | | 2.5 | 3.3 | | | 24.0 | | | 24.3 | |
| Level of Service | Α | Α | | Α | Α | | | С | | | С | |
| Approach Delay (s) | | 3.4 | | | 3.3 | | | 24.0 | | | 24.3 | |
| Approach LOS | | Α | | | Α | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 5.8 | H | CM 2000 | Level of | Service | | Α | | | |
| HCM 2000 Volume to Capac | city ratio | | 0.26 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 52.1 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utilizat | tion | | 49.1% | IC | CU Level | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-------------------------------|-------------|------|-------|------------|-----------|-------------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † 1> | | | † † | | 7 |
| Traffic Volume (veh/h) | 282 | 10 | 0 | 290 | 0 | 5 |
| Future Volume (Veh/h) | 282 | 10 | 0 | 290 | 0 | 5 |
| Sign Control | Free | | | Free | Stop | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 307 | 11 | 0 | 315 | 0 | 5 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | | | None | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | 134 | | | 53 | | |
| pX, platoon unblocked | | | | | 1.00 | |
| vC, conflicting volume | | | 318 | | 470 | 159 |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | | | 318 | | 465 | 159 |
| tC, single (s) | | | 4.2 | | 6.9 | 7.0 |
| tC, 2 stage (s) | | | | | | |
| tF (s) | | | 2.2 | | 3.5 | 3.3 |
| p0 queue free % | | | 100 | | 100 | 99 |
| cM capacity (veh/h) | | | 1217 | | 517 | 849 |
| Direction, Lane # | EB 1 | EB 2 | WB 1 | WB 2 | NB 1 | |
| Volume Total | 205 | 113 | 158 | 158 | 5 | |
| Volume Left | 0 | 0 | 0 | 0 | 0 | |
| Volume Right | 0 | 11 | 0 | 0 | 5 | |
| cSH | 1700 | 1700 | 1700 | 1700 | 849 | |
| Volume to Capacity | 0.12 | 0.07 | 0.09 | 0.09 | 0.01 | |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 9.3 | |
| Lane LOS | | | | | Α | |
| Approach Delay (s) | 0.0 | | 0.0 | | 9.3 | |
| Approach LOS | | | | | Α | |
| Intersection Summary | | | | | | |
| Average Delay | | | 0.1 | | | |
| Intersection Capacity Utiliza | ation | | 18.1% | IC | U Level o | f Service |
| Analysis Period (min) | | | 15 | | | |

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|------------------------------|-------------|-------------|-------|------|------------|------------|---------|----------|------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ∱ 1> | | ሻ | ∱ Ъ | | | 4 | 7 | | 414 | |
| Traffic Volume (vph) | 61 | 195 | 57 | 47 | 181 | 57 | 51 | 183 | 32 | 54 | 195 | 51 |
| Future Volume (vph) | 61 | 195 | 57 | 47 | 181 | 57 | 51 | 183 | 32 | 54 | 195 | 51 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | | 1.00 | 1.00 | | 0.95 | |
| Frt | 1.00 | 0.97 | | 1.00 | 0.96 | | | 1.00 | 0.85 | | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.99 | 1.00 | | 0.99 | |
| Satd. Flow (prot) | 1738 | 3358 | | 1738 | 3351 | | | 1810 | 1555 | | 3358 | |
| Flt Permitted | 0.53 | 1.00 | | 0.58 | 1.00 | | | 0.83 | 1.00 | | 0.83 | |
| Satd. Flow (perm) | 969 | 3358 | | 1067 | 3351 | | | 1521 | 1555 | | 2802 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 66 | 212 | 62 | 51 | 197 | 62 | 55 | 199 | 35 | 59 | 212 | 55 |
| RTOR Reduction (vph) | 0 | 30 | 0 | 0 | 42 | 0 | 0 | 0 | 26 | 0 | 26 | 0 |
| Lane Group Flow (vph) | 66 | 244 | 0 | 51 | 217 | 0 | 0 | 254 | 9 | 0 | 300 | 0 |
| Turn Type | pm+pt | NA | | Perm | NA | | pm+pt | NA | Perm | Perm | NA | |
| Protected Phases | 5 | 2 | | | 6 | | 3 | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | 27.1 | 27.1 | | 17.1 | 17.1 | | | 13.4 | 13.4 | | 13.4 | |
| Effective Green, g (s) | 27.1 | 27.1 | | 17.1 | 17.1 | | | 13.4 | 13.4 | | 13.4 | |
| Actuated g/C Ratio | 0.52 | 0.52 | | 0.33 | 0.33 | | | 0.26 | 0.26 | | 0.26 | |
| Clearance Time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 617 | 1733 | | 347 | 1091 | | | 388 | 396 | | 715 | |
| v/s Ratio Prot | 0.02 | c0.07 | | | c0.06 | | | | | | | |
| v/s Ratio Perm | 0.04 | | | 0.05 | | | | c0.17 | 0.01 | | 0.11 | |
| v/c Ratio | 0.11 | 0.14 | | 0.15 | 0.20 | | | 0.65 | 0.02 | | 0.42 | |
| Uniform Delay, d1 | 6.4 | 6.6 | | 12.5 | 12.8 | | | 17.5 | 14.6 | | 16.3 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 0.3 | 0.2 | | 0.9 | 0.4 | | | 3.9 | 0.0 | | 0.4 | |
| Delay (s) | 6.8 | 6.8 | | 13.4 | 13.2 | | | 21.4 | 14.7 | | 16.7 | |
| Level of Service | А | Α | | В | В | | | С | В | | В | |
| Approach Delay (s) | | 6.8 | | | 13.2 | | | 20.6 | | | 16.7 | |
| Approach LOS | | А | | | В | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 14.1 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capa | acity ratio | | 0.36 | | | | | | | | | |
| Actuated Cycle Length (s) | • | | 52.5 | S | um of lost | time (s) | | | 16.0 | | | |
| Intersection Capacity Utiliz | ation | | 51.6% | IC | CU Level o | of Service | 9 | | Α | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-----------------------------------|----------|----------|-------|-------|------------|------------|---------|----------|-------------|-------------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | ř | f) | | | र्स | 7 | | 4 | |
| Traffic Volume (vph) | 72 | 232 | 35 | 298 | 186 | 22 | 12 | 195 | 401 | 17 | 232 | 49 |
| Future Volume (vph) | 72 | 232 | 35 | 298 | 186 | 22 | 12 | 195 | 401 | 17 | 232 | 49 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Frt | | 0.99 | | 1.00 | 0.98 | | | 1.00 | 0.85 | | 0.98 | |
| Flt Protected | | 0.99 | | 0.95 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Satd. Flow (prot) | | 1785 | | 1738 | 1800 | | | 1824 | 1555 | | 1784 | |
| Flt Permitted | | 0.88 | | 0.48 | 1.00 | | | 0.97 | 1.00 | | 0.97 | |
| Satd. Flow (perm) | | 1580 | | 878 | 1800 | | | 1777 | 1555 | | 1736 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 78 | 252 | 38 | 324 | 202 | 24 | 13 | 212 | 436 | 18 | 252 | 53 |
| RTOR Reduction (vph) | 0 | 7 | 0 | 0 | 7 | 0 | 0 | 0 | 329 | 0 | 12 | 0 |
| Lane Group Flow (vph) | 0 | 361 | 0 | 324 | 219 | 0 | 0 | 225 | 107 | 0 | 311 | 0 |
| Turn Type | Perm | NA | | pm+pt | NA | | Perm | NA | Perm | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | | 21.1 | | 31.1 | 31.1 | | | 14.1 | 14.1 | | 14.1 | |
| Effective Green, g (s) | | 21.1 | | 31.1 | 31.1 | | | 14.1 | 14.1 | | 14.1 | |
| Actuated g/C Ratio | | 0.37 | | 0.54 | 0.54 | | | 0.25 | 0.25 | | 0.25 | |
| Clearance Time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | | 582 | | 597 | 978 | | | 438 | 383 | | 427 | |
| v/s Ratio Prot | | | | c0.08 | 0.12 | | | | | | | |
| v/s Ratio Perm | | c0.23 | | 0.22 | | | | 0.13 | 0.07 | | c0.18 | |
| v/c Ratio | | 0.62 | | 0.54 | 0.22 | | | 0.51 | 0.28 | | 0.73 | |
| Uniform Delay, d1 | | 14.8 | | 8.0 | 6.8 | | | 18.6 | 17.4 | | 19.8 | |
| Progression Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | | 4.9 | | 3.5 | 0.5 | | | 1.0 | 0.4 | | 6.1 | |
| Delay (s) | | 19.7 | | 11.5 | 7.3 | | | 19.6 | 17.8 | | 25.9 | |
| Level of Service | | В | | В | Α | | | В | В | | С | |
| Approach Delay (s) | | 19.7 | | | 9.8 | | | 18.4 | | | 25.9 | |
| Approach LOS | | В | | | Α | | | В | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 17.4 | Н | CM 2000 | Level of S | Service | | В | | | |
| HCM 2000 Volume to Capaci | ty ratio | | 0.63 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 57.2 | S | um of lost | time (s) | | | 14.0 | | | |
| Intersection Capacity Utilization | on | | 79.3% | | U Level o | | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

| | Joiner 3 | | | | | | | | | | | |
|-------------------------------|------------|----------|-------|------|------------|------------|---------|----------|------|-------------|----------|------|
| | ٠ | → | • | • | ← | • | 4 | † | / | > | ↓ | 1 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ۲ | 4 | | ሻ | 4 | | | 4 | | | 4 | |
| Traffic Volume (vph) | 45 | 270 | 34 | 13 | 249 | 21 | 23 | 24 | 16 | 22 | 14 | 28 |
| Future Volume (vph) | 45 | 270 | 34 | 13 | 249 | 21 | 23 | 24 | 16 | 22 | 14 | 28 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frt | 1.00 | 0.98 | | 1.00 | 0.99 | | | 0.97 | | | 0.94 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.98 | | | 0.98 | |
| Satd. Flow (prot) | 1789 | 1801 | | 1789 | 1861 | | | 1787 | | | 1661 | |
| Flt Permitted | 0.58 | 1.00 | | 0.56 | 1.00 | | | 0.85 | | | 0.86 | |
| Satd. Flow (perm) | 1093 | 1801 | | 1057 | 1861 | | | 1547 | | | 1449 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 49 | 293 | 37 | 14 | 271 | 23 | 25 | 26 | 17 | 24 | 15 | 30 |
| RTOR Reduction (vph) | 0 | 6 | 0 | 0 | 4 | 0 | 0 | 15 | 0 | 0 | 27 | 0 |
| Lane Group Flow (vph) | 49 | 324 | 0 | 14 | 290 | 0 | 0 | 53 | 0 | 0 | 42 | 0 |
| Heavy Vehicles (%) | 2% | 5% | 4% | 2% | 2% | 2% | 2% | 2% | 2% | 2% | 5% | 12% |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 33.5 | 33.5 | | 33.5 | 33.5 | | | 5.9 | | | 5.9 | |
| Effective Green, g (s) | 33.5 | 33.5 | | 33.5 | 33.5 | | | 5.9 | | | 5.9 | |
| Actuated g/C Ratio | 0.65 | 0.65 | | 0.65 | 0.65 | | | 0.11 | | | 0.11 | |
| Clearance Time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 712 | 1173 | | 688 | 1212 | | | 177 | | | 166 | |
| v/s Ratio Prot | | c0.18 | | | 0.16 | | | | | | | |
| v/s Ratio Perm | 0.04 | | | 0.01 | | | | c0.03 | | | 0.03 | |
| v/c Ratio | 0.07 | 0.28 | | 0.02 | 0.24 | | | 0.30 | | | 0.26 | |
| Uniform Delay, d1 | 3.3 | 3.8 | | 3.2 | 3.7 | | | 20.9 | | | 20.7 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.2 | 0.6 | | 0.1 | 0.5 | | | 1.0 | | | 8.0 | |
| Delay (s) | 3.4 | 4.4 | | 3.2 | 4.2 | | | 21.8 | | | 21.6 | |
| Level of Service | А | Α | | Α | Α | | | С | | | С | |
| Approach Delay (s) | | 4.3 | | | 4.1 | | | 21.8 | | | 21.6 | |
| Approach LOS | | Α | | | Α | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 7.1 | H | CM 2000 | Level of S | Service | | Α | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.28 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 51.4 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utiliza | ition | | 55.7% | IC | CU Level | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| | - | • | • | • | • | <i>></i> |
|------------------------------|------------|------|-------|------------|-----------|-------------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † † | | | † † | | 7 |
| Traffic Volume (veh/h) | 303 | 5 | 0 | 283 | 0 | 10 |
| Future Volume (Veh/h) | 303 | 5 | 0 | 283 | 0 | 10 |
| Sign Control | Free | | | Free | Stop | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 329 | 5 | 0 | 308 | 0 | 11 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | | | None | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | 134 | | | 53 | | |
| pX, platoon unblocked | | | | | 0.98 | |
| vC, conflicting volume | | | 334 | | 486 | 167 |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | | | 334 | | 439 | 167 |
| tC, single (s) | | | 4.2 | | 6.9 | 7.0 |
| tC, 2 stage (s) | | | | | | |
| tF (s) | | | 2.2 | | 3.5 | 3.3 |
| p0 queue free % | | | 100 | | 100 | 99 |
| cM capacity (veh/h) | | | 1201 | | 529 | 839 |
| Direction, Lane # | EB 1 | EB 2 | WB 1 | WB 2 | NB 1 | |
| Volume Total | 219 | 115 | 154 | 154 | 11 | |
| Volume Left | 0 | 0 | 0 | 0 | 0 | |
| Volume Right | 0 | 5 | 0 | 0 | 11 | |
| cSH | 1700 | 1700 | 1700 | 1700 | 839 | |
| Volume to Capacity | 0.13 | 0.07 | 0.09 | 0.09 | 0.01 | |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 | |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 9.4 | |
| Lane LOS | | | | | Α | |
| Approach Delay (s) | 0.0 | | 0.0 | | 9.4 | |
| Approach LOS | | | | | Α | |
| Intersection Summary | | | | | | |
| Average Delay | | | 0.2 | | | |
| Intersection Capacity Utiliz | ation | | 18.5% | IC | U Level c | f Service |
| Analysis Period (min) | | | 15 | | | |

Appendix C: Background Development



Enhancing our communities



Downtown Barrie Retirement Residence

TRAFFIC IMPACT STUDY

Revera Inc.

Proposed Development 4

This section will provide additional details with respect to the proposed Downtown Barrie Retirement Residence development, including its location, the projected site generated traffic volumes and the assignment of such to the adjacent road network.

4.1 SITE LOCATION

The subject site is located on the southeast corner of the intersection of Collier Street with Owen Street in the City of Barrie (as per Figure 1). The property is bounded by Collier Street to the north, Owen Street to the west, a public laneway to the south and existing commercial development to the east.

4.2 **PROPOSED LAND-USE & PHASING**

The proposed retirement development will consist of the following:

- 252 retirement residence units (1 & 2 bedrooms);
- 62 assisted living units (studio & 1 bedroom);
- 171 m² (1841 ft²) of commercial space; and
- a 65-space parking garage.

Access to the parking garage is provided via the existing public laneway which connects to Owen Street.

A site plan is provided in Figure 7. Full build-out has been assumed by 2021.

SITE ACCESS 4.3

As illustrated in Figure 7, access to the parking garage will be located on the south side of the building via the public lane, which connects to Owen Street. The parking garage access provides two-way operations (i.e. one inbound lane and one outbound lane). Full moves are permitted at the public laneway access on Owen Street.

The loading area and garbage enclosure, both located to the rear of the building, will be accessed via the existing public laneway. Furthermore, an internal garage space is also located at the rear of the building (adjacent to the garbage enclosure) for tour bus operations serving the residents of the development.



4.5 SITE TRAFFIC

4.5.1 **Trip Generation**

The number of vehicle trips to be generated by the proposed development has been determined based on type of use, development size, and trip generation rates as per the ITE Trip Generation Manual⁸ 9th Edition. Based on the proposed development, the following ITE land-uses have been considered:

- senior adult housing attached (ITE code 252);
- assisted living (ITE code 254); and
- shopping centre (ITE code 820).

The ITE Trip Generation Manual notes that the peak trip generation for the senior adult housing (attached) and assisted living land uses do not typically coincide with the peak hour of the adjacent street (i.e. trips to/from these developments will be greatest during the off-peak period of the road). However, for the purpose of this study, the trip generation rates associated with the peak hour of the proposed land use have been assumed to coincide with the peak hour of the adjacent road. This approach considers a conservative or "worst case" scenario as both peaks are assumed to occur simultaneously.

A specific commercial use has not been identified at this time, but it is anticipated to be consistent with other specialty retail shops located along Collier Street and Dunlop Street. As such, the shopping centre trip rates have been applied.

The associated trip rates and trip estimates are provided in Table 6 and Table 7.

Table 6: Trip Generation Rates

| LAND USE | VARIABLE | | VEEKDA PEAK H | | WEEKDAY PM PEAK HOUR | | | |
|------------------------------------|-----------------|------|------------------|-------|-------------------------|------|-------|--|
| | | IN | OUT | TOTAL | IN | OUT | TOTAL | |
| senior adult housing – attached | units | 0.18 | 0.21 | 0.39 | 0.19 | 0.16 | 0.35 | |
| assisted living | units | 0.12 | 0.06 | 0.18 | 0.16 | 0.19 | 0.35 | |
| shopping centre | 1000 ft² GLA | 0.60 | 0.36 | 0.96 | 1.78 | 1.93 | 3.71 | |



⁸ ITE Trip Generation Manual, 9th Edition. Institute of Transportation Engineers, 2012.

Table 7: Trip Generation Estimates

| LAND USE | SIZE | AM | PEAK H | OUR | PM PEAK HOUR | | | |
|------------------------------------|-----------|----|--------|-------|--------------|-----|-------|--|
| LAND USE | 3126 | IN | OUT | TOTAL | IN | OUT | TOTAL | |
| senior adult housing - attached | 252 units | 17 | 31 | 48 | 35 | 23 | 58 | |
| assisted living | 62 units | 6 | 3 | 9 | 6 | 8 | 14 | |
| shopping centre | 1,841 ft² | 1 | 1 | 2 | 3 | 4 | 7 | |
| Total | | 24 | 35 | 59 | 44 | 35 | 79 | |

Overall, the proposed development is expected to generate 59 trips during the weekday AM peak hour and 79 trips during the weekday PM peak hour (total of inbound and outbound trips). It is reiterated that the trip estimates for the senior related uses reflect the peak hours of the specific uses (based on ITE trip generation data) rather than the peak hour of the adjacent street. Thus, the approach employed in this study is conservative.

4.5.2 **Trip Distribution & Assignment**

The distribution of the new trips generated by the site has been developed based on the results of the Transportation Tomorrow Survey (TTS) completed in 2016. The TTS is a survey of a random sampling of 5% of the households in the Greater Toronto Area and surrounding area of Central Ontario, including the City of Barrie. Based on a review of the TTS data with respect to trips to/from Barrie, the following trip distribution was identified:

- to/from locations within Barrie 70%;
- to/from the east beyond Barrie 5%;
- to/from the west beyond Barrie 5%;
- to/from the north beyond Barrie 10%; and
- to/from the south beyond Barrie 10%.

As indicated, 70% of the trips remain wholly within Barrie whereas only 30% originate from, or are destined to, areas outside of the City. The trips that remain within Barrie were distributed based on additional TTS trip data for the traffic zone within which the development is located. When considering the distribution of trips that remain within the City, the ultimate trip distribution for the site is as follows:

to/from the east - 5%;

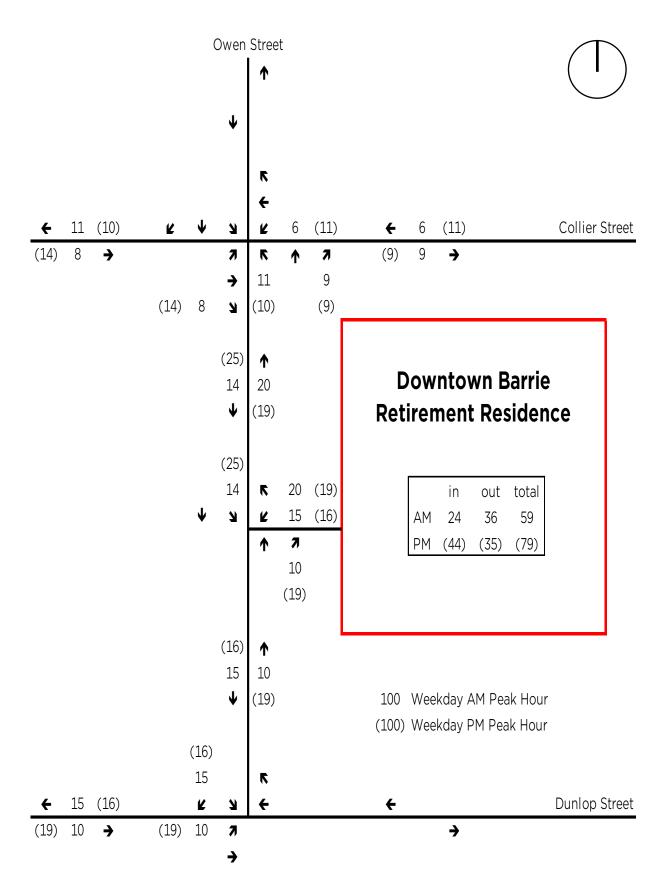


- to/from the west 20%;
- to/from the north 40%; and
- to/from the south 35%.

The assignment of the trips generated by the development to the area road network is based on the trip distribution noted above with consideration given to the expected travel routes. It is noted that the commercial generated trips made by private automobile will not utilize the site access (i.e. the commercial trips will be dispersed along the adjacent road network based on the location of available municipal parking). However, to ensure a conservative approach, it has been assumed that the commercial trips will use the site access (i.e. all site generated trips are assumed to be vehicle trips concentrated at the access to the parking garage).

The resulting site generated traffic volumes assigned to the road network, are illustrated in Figure 8.





Downtown Barrie Retirement Residence

Figure 8: Site Traffic





Owen Street City of Barrie

Traffic Impact Study for Barrie Owen Service Inc.

Type of Document: Final Report

> Project Number: JDE – 1796

Date Submitted: November 30th, 2017

John Northcote, P.Eng.

Professional License #: 100124071





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Table 8 - Background (2031) LOS

| Location | | | lay AM Peak H | lour | Wee | ekday PM Pe | ak Hour |
|---|----|------|---------------|------|------|-------------|---------|
| (N-S Street / E-W Street) | | V/C | Delay (s) | LOS | V/C | Delay (s) | LOS |
| Owen Street / McDonald Street (signalized) | | 0.26 | 12.5 | В | 0.40 | 13.6 | В |
| E | EΒ | 0.39 | 12.2 | В | 0.47 | 12.9 | В |
| V | VB | 0.39 | 12.3 | В | 0.52 | 13.5 | В |
| l l | NΒ | 0.07 | 13.9 | В | 0.24 | 15.7 | В |
| 5 | SB | 0.09 | 14.1 | В | 0.04 | 13.7 | В |
| Owen Street / Worsley Street (unsignalized) | | - | 8.6 | Α | ı | 9.3 | Α |
| E | ЕВ | 0.25 | 8.9 | Α | 0.17 | 8.8 | Α |
| V | VB | 0.13 | 8.3 | Α | 0.29 | 9.7 | Α |
| 1 | NΒ | 0.13 | 8.3 | Α | 0.23 | 9.4 | Α |
| | SB | 0.15 | 8.6 | Α | 0.15 | 8.8 | Α |

The results of the LOS analysis indicate that all intersections are operating within the typical design limits noted in Section 3.1.

For right turn movements at the Owen Street / Worsley Street intersection, the criteria outlined in Section E.7 of the MTO GDSOH (60 vph minimum right turn volume warrant) were applied. Based on the above-noted criteria, no right turn lanes are warranted.

Based on the Ontario Traffic Manual Book 12 *Signal Justification*, traffic signals are not warranted at any of the unsignalized study area intersections (results are provided in **Appendix D**).

No improvements are recommended within the study area.

4 Proposed Development Traffic Generation and Assignment

4.1 Existing Municipal Parking Lot

The subject site is to be built at the same location as the existing municipal parking lot. The current plan for the development of the site involves the removal of the municipal parking lot (and consequently traffic associated with that facility) prior to the 2021 horizon year. The traffic distribution for the trips generated by the existing municipal parking lot during the AM and PM peak hour is assumed to follow the distribution of the existing traffic volumes within the study area. The traffic assignment for the existing municipal parking lot was calculated for the AM and PM peak hour and has been illustrated in **Figure 8**.

Additional traffic generated by the existing development in the south half of the site also generates traffic that would be captured in the existing traffic counts; however, for the purpose of our analysis we have ignored this traffic reduction, as it is anticipated to be relatively minor.

4.2 Traffic Generation

The traffic generation for the subject site has been based on the ITE Trip Generation Manual. The following ITE land use has been applied to estimate the traffic from the proposed development:



ITE land use 231 (Mid-Rise Residential with 1st-Floor Commercial)
 Dense Multi-Use Urban Setting

The estimated trip generation of the proposed development for Phase 1 and the ultimate development is illustrated below in **Table 9**. The AM and PM peak traffic generation for the proposed development is not anticipated to exactly align with the AM and PM peak hour in the traffic counts; consequently, we have applied the peak hour of adjacent street traffic values provided in the ITE Trip Generation Manual.

Table 9 – Estimated Traffic Generation of Proposed Development

| DI | | 0: | Α | M Peak H | our | PM Peak Hour | | | |
|-------------------------|---|-----------|----|----------|-------|--------------|-----|-------|--|
| Phase | Land Use | Size | IN | OUT | TOTAL | IN | OUT | TOTAL | |
| Ultimate Development | Mid-Rise Residential with 1 st -Floor Commercial ITE Land Use: 231 | 307 units | 39 | 56 | 95 | 63 | 81 | 144 | |

No transportation modal split has been applied to the above-noted traffic generation calculation.

4.3 Traffic Assignment

For the purposes of this study, it has been assumed that all residential traffic generated by the proposed development will be new traffic and would not be in the study area if the development was not constructed.

The ITE data provides the anticipated percentage of new traffic entering and exiting during the peak hour. The distribution of traffic has been calculated based on the 2011 Transportation Tomorrow Survey [TTS] data for traffic zone 8501 retrieved using the TTS Internet Data Retrieval System [IDRS] (output attached as **Appendix F**). TTS data provides historical origin and destination work trip percentages for specific areas within the County and the Greater Toronto and Hamilton Area [GTHA].

Traffic distribution for the trips generated by the subject site during the AM and PM peak hour is expected to generally follow commuter travel patterns. Our analysis is based on egress traffic during the AM peak hour. Logically, the distribution of ingress traffic will follow the inverse of the exiting traffic distribution. For each of the individual areas identified in the TTS data, we have selected the probable route of travel, assuming that people will select their route primarily based on travel time.

The distribution of trips is illustrated in **Table 10** using the methodology outlined above.



Table 10 - Proposed Development Traffic Distribution

| Travel Direction (to / from) | Percentage of Total Traffic Generation |
|------------------------------|---|
| East via McDonald Street | 4.4% |
| West via McDonald Street | 52.4% |
| East via Worsley Street | 1.6% |
| West via Worsley Street | 17.5% |
| North via Owen Street | 13.7% |
| South via Owen Street | 10.4% |
| TOTAL | 100% |

Using the traffic distribution pattern noted above, the site traffic assignment for the and ultimate buildout of the proposed development was calculated for the AM and PM peak hour and is illustrated in **Figures 9**.

The net site traffic assignment, the site traffic minus the existing municipal parking lot traffic volumes, for the ultimate buildout of the proposed development was calculated for the AM and PM peak hour and is illustrated in **Figures 10**.

4.4 Total Horizon Year Traffic Volumes with the Proposed Development

For the total (2021, 2026 and 2031) horizon year traffic volumes, the proposed development traffic was added to the background (2021, 2026 and 2031) traffic volumes. The resulting total (2021, 2026 and 2031) horizon year traffic volume for the AM and PM peak hour are illustrated in **Figures 11, 12** and **13**.



Figure 8 – Existing Municipal Parking Lot Traffic Volumes

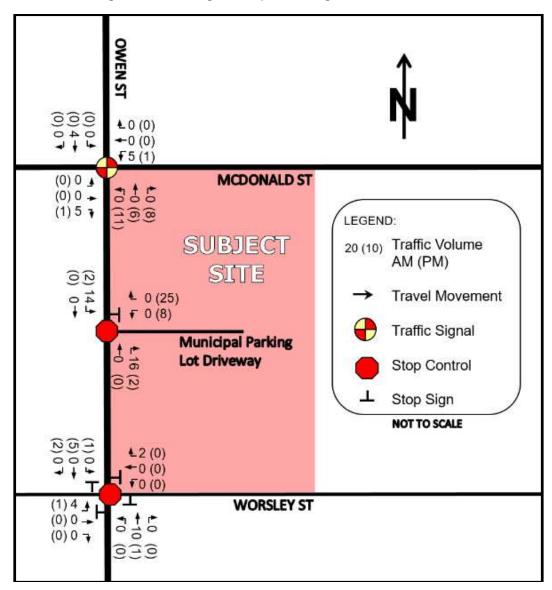




Figure 9 -Site Traffic Assignment - Ultimate Buildout

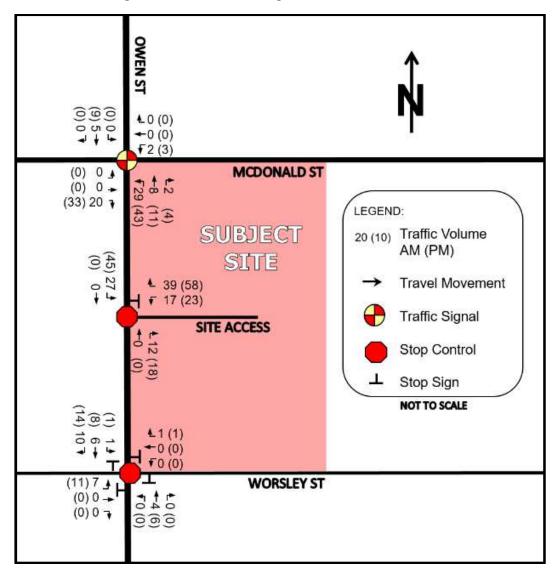
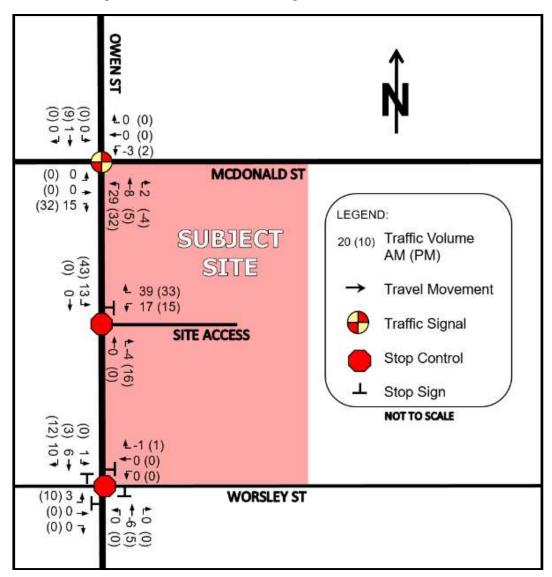




Figure 10 - Net Site Traffic Assignment - Ultimate Buildout







October 31st, 2019 JDE Project 17124

Aalto Developments Inc. 190 Dunlop Street East Barrie, ON L4M 1B3

RE: Traffic Impact Study – Revised Addendum

185 Dunlop Street, City of Barrie

This letter was prepared by **JD Northcote Engineering Inc.** [JD Engineering] for the account of the **AALTO Developments Inc.** [The Developer].

Any use which a third party makes of this report, or any reliance on or decisions to be made based on it, are the responsibility of such third parties. JD Engineering accept no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this project.

1.0 BACKGROUND

JD Engineering prepared a traffic impact study for the proposed 185 Dunlop Street mixed-use development [Subject Site], located in the City of Barrie [City] (dated December 21, 2017) [TIS]. The above noted TIS assessed the traffic-related impact of the proposed development on the adjacent roadway and provided recommendations to accommodate this traffic in a safe and efficient manner.

A development proposal is now underway for the property located directly west of the Subject Site [New Adjacent Development]. The New Adjacent Development extends from Dunlop Street East to the lake, between Mulcaster Street and the Subject Site. The New Adjacent Development will include one access onto Mulcaster Street [Mulcaster Access] and one access onto a proposed extension of Poyntz Street, south of Dunlop Street East [Adjacent Development Access], directly across from the proposed access for the Subject Site [West P1 Access]. To accommodate the New Adjacent Development, the proposed extension of Poyntz Street has been redesigned to accommodate traffic from the New Adjacent Development. The City has requested an update letter to the TIS to review the impact of the additional traffic volumes from the New Adjacent Development at the future Poyntz Street / Dunlop Street East intersection.

Furthermore, following the completion of the TIS, the Site Plan for the Subject Site has been revised to include 178 residential units and approximately 1,764 sq.m. commercial space (site plan provided in the **Appendix**). Included in the 1,764 sq.m. of commercial space will be a 5,600 sq.ft. health and fitness club.

This revised addendum also addresses Item #2 from the City Traffic and Parking Services' Comments from July 31, 2019 (Excerpt in **Appendix**).



2.0 PROPOSED DEVELOPMENT – REVISED TRAFFIC GENERATION

The revised traffic generation for the Subject Site has been based on the Institute of Transportation Engineers [ITE] *Trip Generation Manual* (10th Edition) [ITE Trip Generation Manual]. The following ITE land use has been applied to estimate the revised traffic from the proposed development:

- ITE land use 231 (Mid-Rise Residential with 1st-Floor Commercial)
 - o Dense Multi-Use Urban Setting
- ITE land use 492 (Health/Fitness Club)
 - o General Urban / Suburban Setting

The estimated trip generation for the proposed development is illustrated below in **Table 1**. The AM and PM peak traffic generation for the proposed development is not anticipated to exactly align with the AM and PM peak hour in the traffic counts; consequently, we have applied the peak hour of adjacent street traffic values provided in the ITE Trip Generation Manual.

Table 1 – Estimated Traffic Generation of Proposed Development

| Landillan | C: | А | M Peak H | our | PM Peak Hour | | | | |
|---|--------------|----|----------|-------|--------------|-----|-------|--|--|
| Land Use | Size | IN | OUT | TOTAL | IN | OUT | TOTAL | | |
| Mid-Rise Residential with 1 st -Floor Commercial ITE Land Use: 231 | 178 units | 23 | 32 | 55 | 37 | 47 | 84 | | |
| Health/Fitness Club ITE Land Use: 492 | 5,600 sq.ft. | 4 | 3 | 7 | 11 | 8 | 19 | | |
| TOTAL TRIP GENERATION | | 27 | 35 | 62 | 48 | 55 | 103 | | |
| Internal Captur | 0 | 0 | 0 | -3 | -3 | -6 | | | |
| NET TRIP GENERAL | TION | 27 | 35 | 62 | 45 | 52 | 97 | | |

It is noted that ITE land use 231 accounts for commercial space within a mixed-use building; however, we have accounted for additional traffic for the Health and Fitness Club as the commercial space in ITE land use 231 is typically considered to be retail.

No transportation modal split has been applied to the above-noted traffic generation calculation.

3.0 PROPOSED DEVELOPMENT – REVISED TRAFFIC ASSIGNMENT

The distribution of residential traffic for the proposed development is assumed to follow the trip distribution calculated for residential traffic as illustrated in Table 10 in Section 4.2 in the TIS.

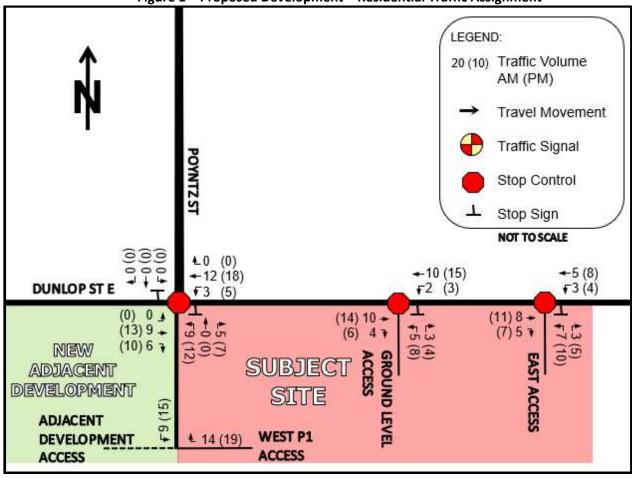
The distribution of health and fitness club traffic for the proposed development is assumed to follow the existing trip distribution in the study area as illustrated in Table 11 in Section 4.2 in the TIS.



The distribution of traffic entering at each site access driveway is based on our review of the internal parking and building layout, in conjunction with the external traffic distribution.

Using the traffic distribution patterns noted above, the residential and health and fitness club traffic assignments for the proposed development was calculated for the AM and PM peak hour and is illustrated in **Figures 1** and **2**, respectively.







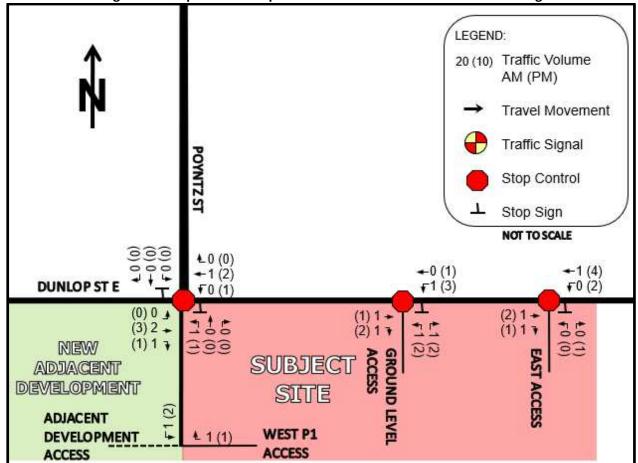


Figure 2 – Proposed Development – Health and Fitness Club Traffic Assignment

4.0 New Adjacent Development Traffic Generation

The New Adjacent Development includes 130 hotel rooms, 136 condominium units and 500 sq.m. of commercial space. It has been assumed that this development will be occupied prior to the 2027 horizon year.

A traffic impact study is not available for the New Adjacent Development. The traffic generation for the New Adjacent Development has been calculated based on the data provided in the ITE Trip Generation Manual. The following ITE land uses have been applied to estimate the traffic from the New Adjacent Development:

- ITE land use 231 (Mid-Rise Residential with 1st-Floor Commercial)
 - o Dense Multi-Use Urban Setting
- ITE land use 310 (Hotel) General Urban/Suburban Setting



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The AM and PM peak hour traffic generation for the New Adjacent Development does not exactly align with the AM and PM peak hour in the traffic counts; consequently, we have applied the peak hour of adjacent street traffic values provided in the ITE Trip Generation Manual.

The estimated trip generation of the New Adjacent Development is illustrated below in **Table 2**.

Table 2 - Estimated Traffic Generation for the New Adjacent Development

| Land Hea | C: | Α | M Peak H | our | PM Peak Hour | | | |
|---|-----------|----|----------|-------|--------------|-----|-------|--|
| Land Use | Size | IN | OUT | TOTAL | IN | OUT | TOTAL | |
| Mid-Rise Residential with 1 st -Floor Commercial ITE Land Use: 231 | 136 units | 17 | 25 | 42 | 28 | 36 | 64 | |
| Hotel ITE Land Use: 310 | 130 units | 36 | 25 | 61 | 40 | 38 | 78 | |
| TOTAL TRIP GENERA | 53 | 50 | 103 | 68 | 74 | 142 | | |

No transportation modal split has been applied to the above-noted traffic generation calculation.

5.0 New Adjacent Development Traffic Assignment

The distribution of residential traffic for the New Adjacent Development is assumed to follow the trip distribution calculated for residential traffic as illustrated in Table 10 in Section 4.2 in the TIS.

The distribution of hotel traffic for the New Adjacent Development is assumed to follow the existing trip distribution in the study area traffic as illustrated in Table 11 in Section 4.2 in the TIS.

The distribution of traffic entering at each access driveway for the New Adjacent Development is based on our review of the internal parking and building layout, in conjunction with the external traffic distribution.

Using the traffic distribution patterns noted above, the residential and hotel traffic assignments for the New Adjacent Development was calculated for the AM and PM peak hour within the study area and is illustrated in **Figures 3** and **4**, respectively. It is noted that some of the New Adjacent Development traffic will not be within the study area due to the use of the Mulcaster Access.



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Figure 3 – New Adjacent Development – Residential Traffic Assignment LEGEND: 20 (10) Traffic Volume AM (PM) Travel Movement Traffic Signal Stop Control Stop Sign NOT TO SCALE £0 (0) +2 (4) ₹3 (6) DUNLOP ST E (0) 0 A (5) 3 + +5 (7) +7 (10) (7) 4 7 NEW SUBJECT ADJACENT DEVELOPMENT SITE (13)ADJACENT DEVELOPMENT WEST P1

ACCESS



ACCESS

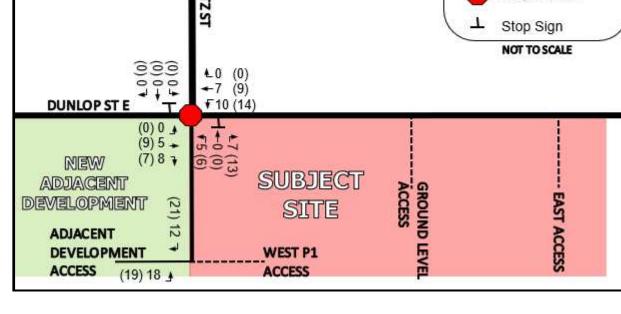
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Addendum Project No.: 17124

Figure 4 – New Adjacent Development – Hotel Traffic Assignment

LEGEND:
20 (10) Traffic Volume
AM (PM)

Travel Movement



6.0 TOTAL HORIZON YEAR TRAFFIC VOLUMES WITH THE PROPOSED DEVELOPMENT

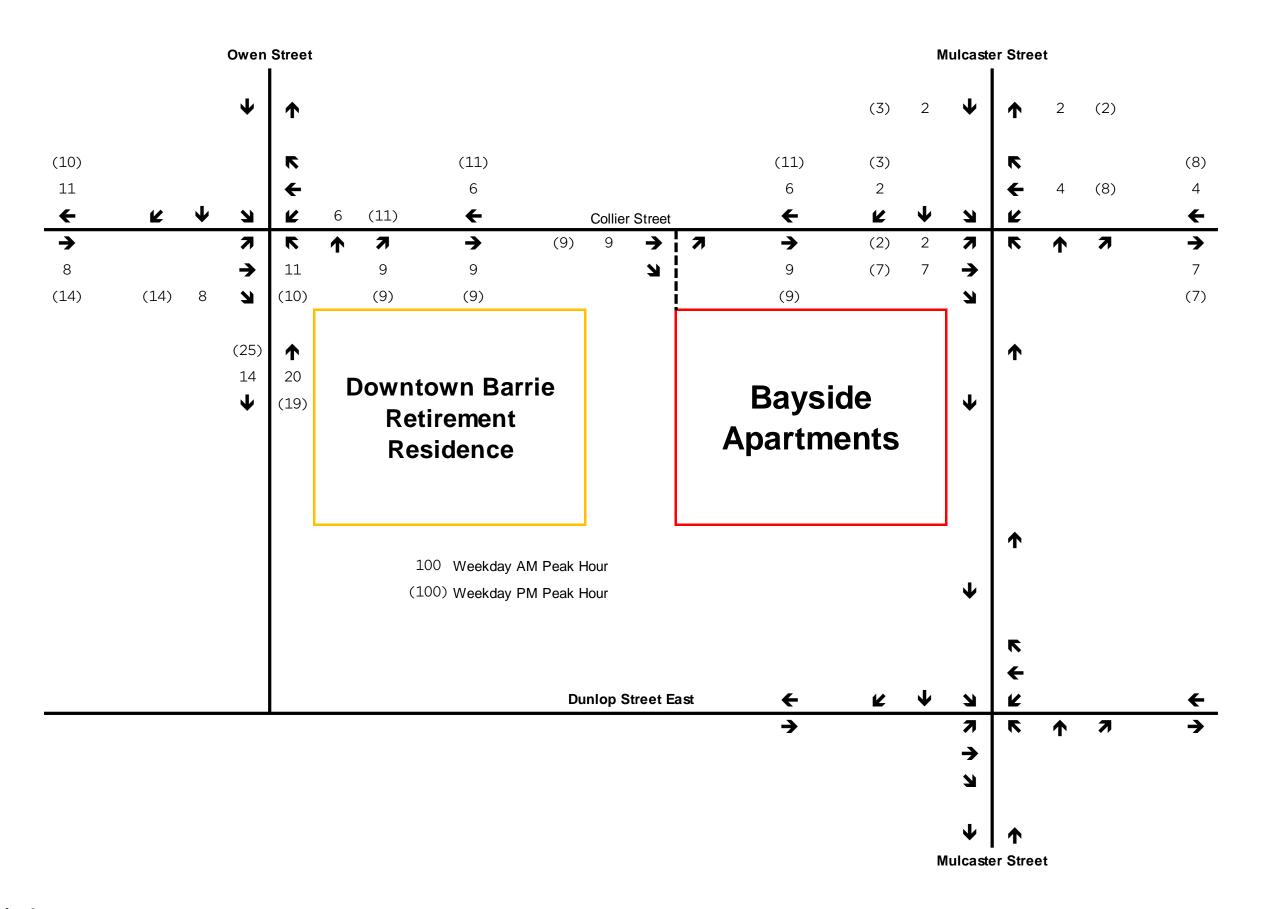
For the revised total (2027) horizon year traffic volumes, the revised proposed development traffic and New Adjacent Development traffic was added to the background (2027) traffic volumes from the TIS. The resulting total (2027) horizon year traffic volumes for the AM and PM peak hour are illustrated in **Figure 5**.



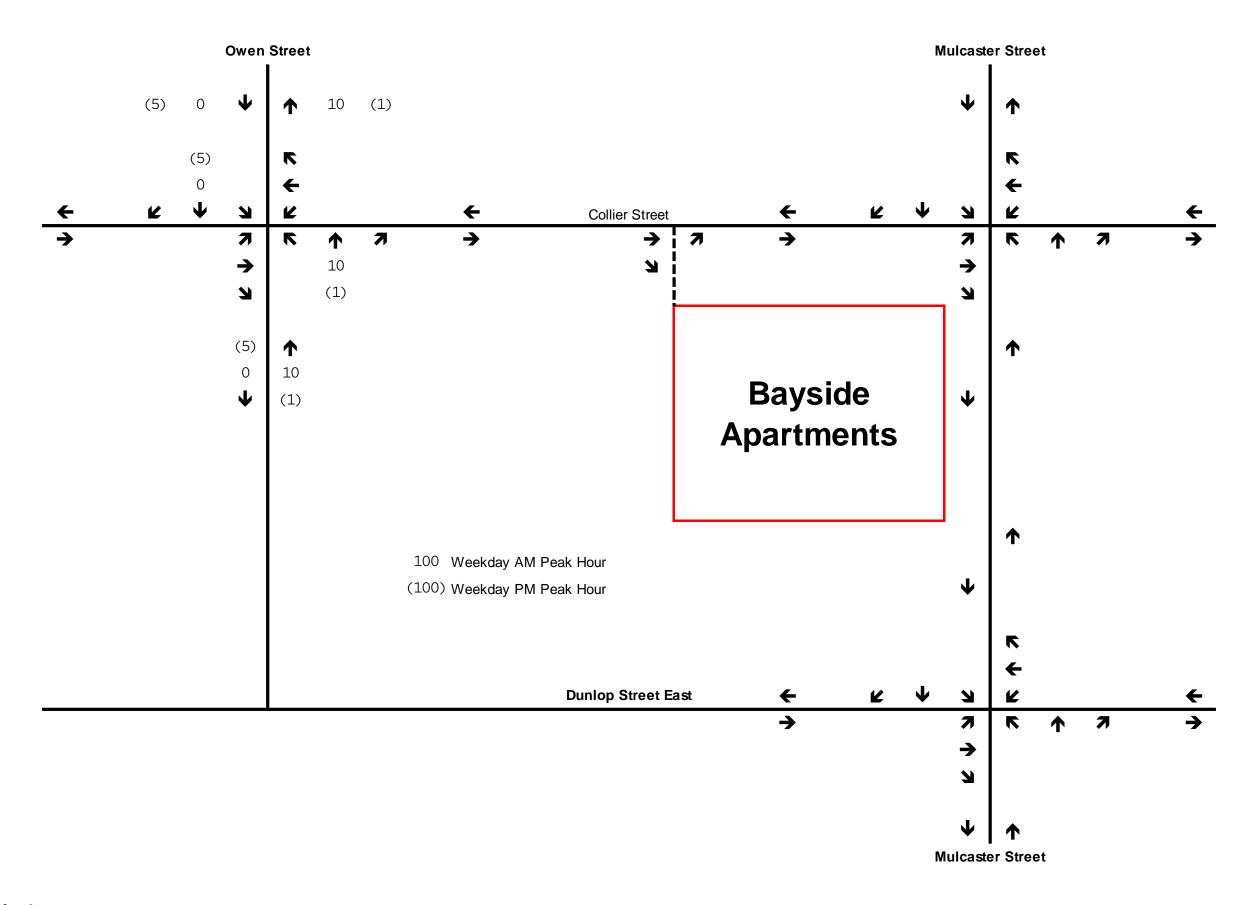
Date: 10/31/19

Traffic Signal

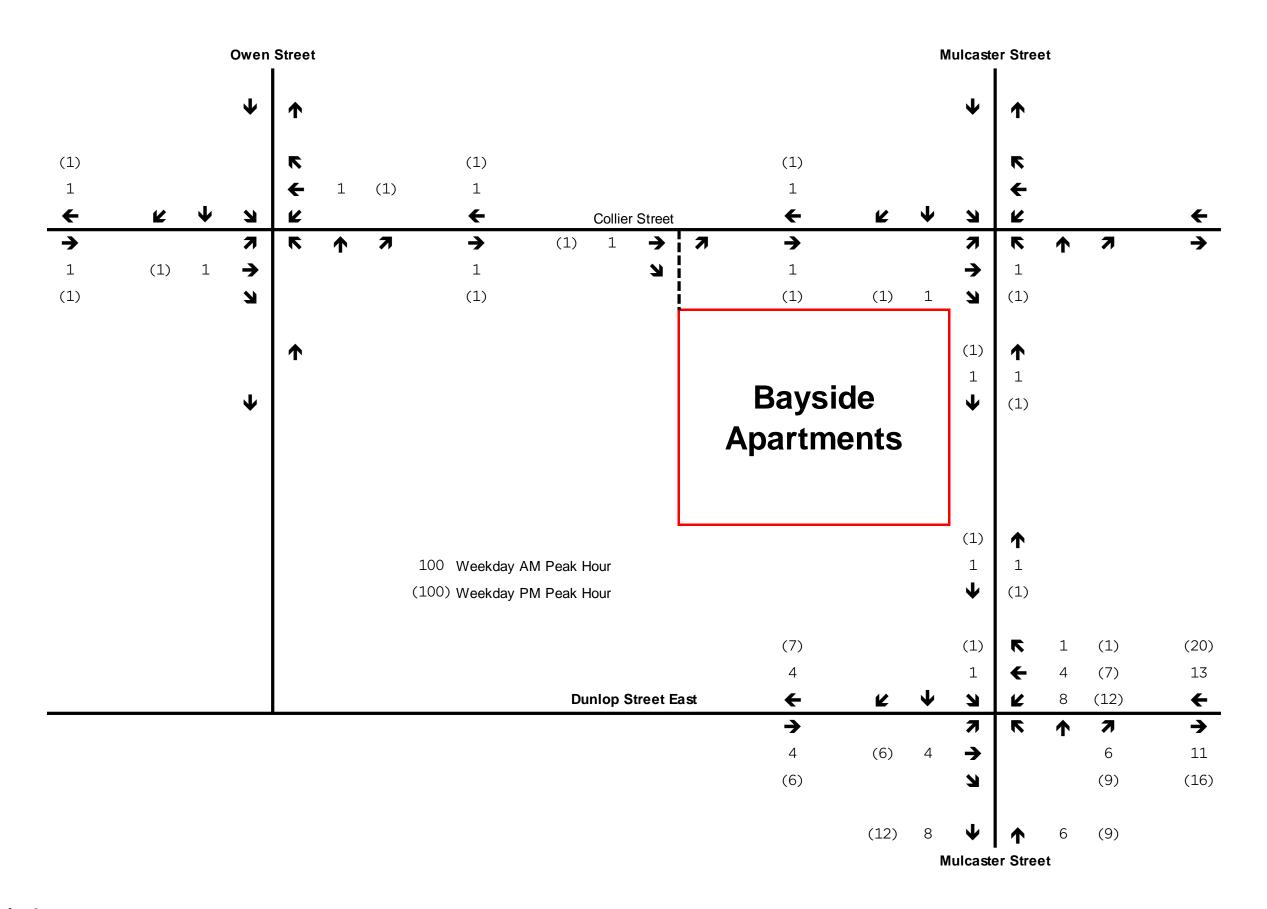
Stop Control

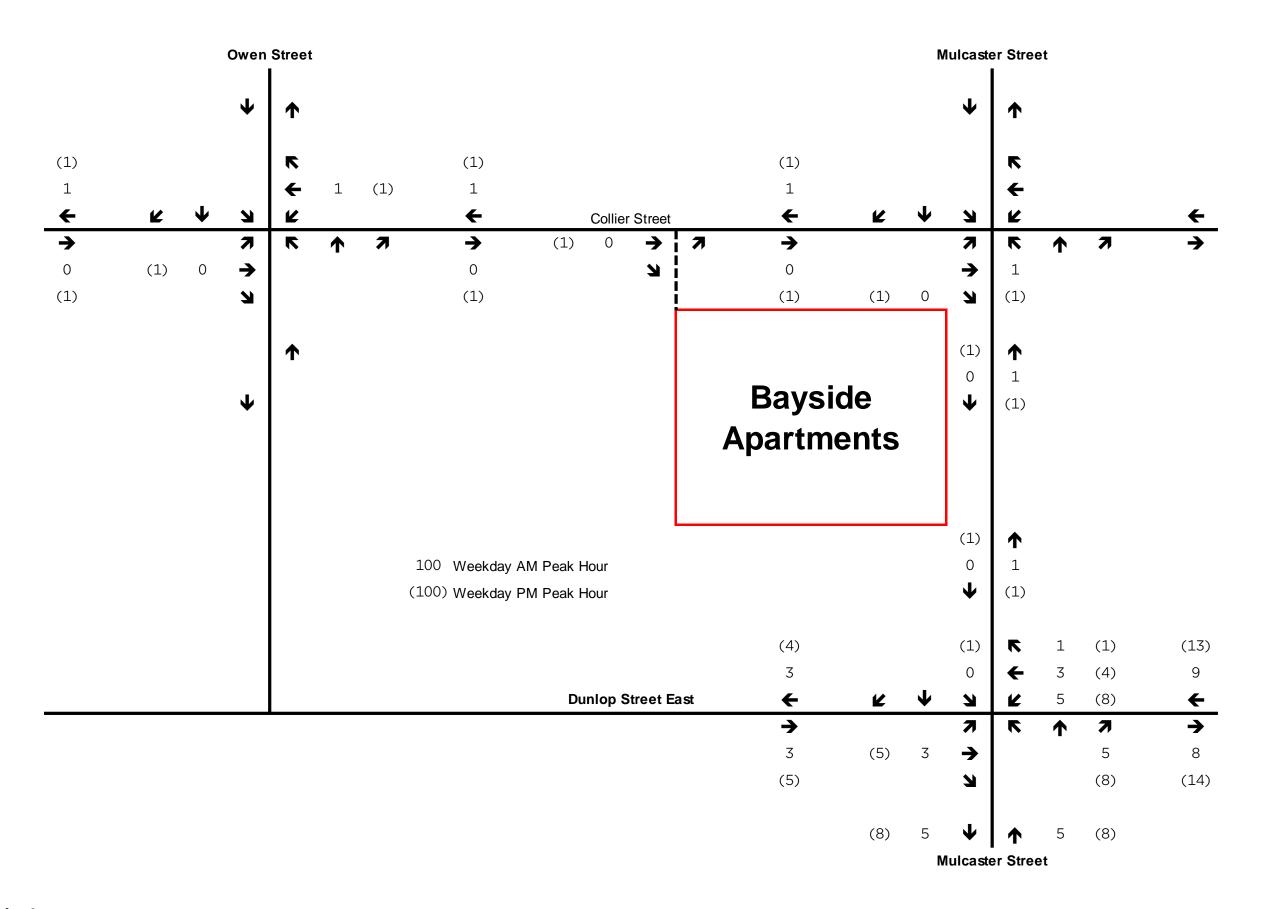












Appendix D: Future Background Operations

| | ۶ | → | • | • | ← | • | • | † | / | > | ļ | 4 |
|-------------------------------|-------------|-------------|-------|------|-------------|------------|---------|----------|------|-------------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | † 1> | | ሻ | ∱ Ъ | | | 4 | 7 | | 414 | |
| Traffic Volume (vph) | 64 | 188 | 62 | 31 | 174 | 77 | 85 | 198 | 36 | 45 | 139 | 55 |
| Future Volume (vph) | 64 | 188 | 62 | 31 | 174 | 77 | 85 | 198 | 36 | 45 | 139 | 55 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | | 1.00 | 1.00 | | 0.95 | |
| Frt | 1.00 | 0.96 | | 1.00 | 0.95 | | | 1.00 | 0.85 | | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.99 | 1.00 | | 0.99 | |
| Satd. Flow (prot) | 1738 | 3347 | | 1738 | 3316 | | | 1803 | 1555 | | 3325 | |
| Flt Permitted | 0.52 | 1.00 | | 0.58 | 1.00 | | | 0.80 | 1.00 | | 0.83 | |
| Satd. Flow (perm) | 956 | 3347 | | 1070 | 3316 | | | 1465 | 1555 | | 2795 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 70 | 204 | 67 | 34 | 189 | 84 | 92 | 215 | 39 | 49 | 151 | 60 |
| RTOR Reduction (vph) | 0 | 34 | 0 | 0 | 58 | 0 | 0 | 0 | 28 | 0 | 40 | 0 |
| Lane Group Flow (vph) | 70 | 237 | 0 | 34 | 215 | 0 | 0 | 307 | 11 | 0 | 220 | 0 |
| Turn Type | pm+pt | NA | | Perm | NA | | pm+pt | NA | Perm | Perm | NA | |
| Protected Phases | 5 | 2 | | | 6 | | 3 | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | 27.2 | 27.2 | | 17.1 | 17.1 | | | 16.3 | 16.3 | | 16.3 | |
| Effective Green, g (s) | 27.2 | 27.2 | | 17.1 | 17.1 | | | 16.3 | 16.3 | | 16.3 | |
| Actuated g/C Ratio | 0.49 | 0.49 | | 0.31 | 0.31 | | | 0.29 | 0.29 | | 0.29 | |
| Clearance Time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 582 | 1640 | | 329 | 1021 | | | 430 | 456 | | 820 | |
| v/s Ratio Prot | 0.02 | c0.07 | | | c0.06 | | | | | | | |
| v/s Ratio Perm | 0.04 | | | 0.03 | | | | c0.21 | 0.01 | | 0.08 | |
| v/c Ratio | 0.12 | 0.14 | | 0.10 | 0.21 | | | 0.71 | 0.03 | | 0.27 | |
| Uniform Delay, d1 | 7.6 | 7.8 | | 13.7 | 14.2 | | | 17.5 | 13.9 | | 15.0 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 0.4 | 0.2 | | 0.6 | 0.5 | | | 5.5 | 0.0 | | 0.2 | |
| Delay (s) | 8.0 | 7.9 | | 14.4 | 14.7 | | | 23.1 | 14.0 | | 15.2 | |
| Level of Service | Α | Α | | В | В | | | С | В | | В | |
| Approach Delay (s) | | 8.0 | | | 14.6 | | | 22.0 | | | 15.2 | |
| Approach LOS | | Α | | | В | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 15.0 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capa | acity ratio | | 0.41 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 55.5 | | um of lost | | | | 16.0 | | | |
| Intersection Capacity Utiliza | ation | | 52.5% | IC | CU Level of | of Service |) | | Α | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-------------------------------|------------|----------|-------|-------|------------|------------|---------|------|-------------|----------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | ሻ | f) | | | 4 | 7 | | 4 | |
| Traffic Volume (vph) | 62 | 141 | 21 | 367 | 190 | 20 | 10 | 218 | 312 | 17 | 184 | 27 |
| Future Volume (vph) | 62 | 141 | 21 | 367 | 190 | 20 | 10 | 218 | 312 | 17 | 184 | 27 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Frt | | 0.99 | | 1.00 | 0.99 | | | 1.00 | 0.85 | | 0.98 | |
| Flt Protected | | 0.99 | | 0.95 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Satd. Flow (prot) | | 1782 | | 1738 | 1803 | | | 1826 | 1555 | | 1794 | |
| Flt Permitted | | 0.85 | | 0.58 | 1.00 | | | 0.98 | 1.00 | | 0.96 | |
| Satd. Flow (perm) | | 1527 | | 1069 | 1803 | | | 1794 | 1555 | | 1723 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 67 | 153 | 23 | 399 | 207 | 22 | 11 | 237 | 339 | 18 | 200 | 29 |
| RTOR Reduction (vph) | 0 | 6 | 0 | 0 | 6 | 0 | 0 | 0 | 264 | 0 | 9 | 0 |
| Lane Group Flow (vph) | 0 | 237 | 0 | 399 | 223 | 0 | 0 | 248 | 75 | 0 | 238 | 0 |
| Turn Type | Perm | NA | | pm+pt | NA | | Perm | NA | Perm | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | | 19.1 | | 32.1 | 32.1 | | | 12.6 | 12.6 | | 12.6 | |
| Effective Green, g (s) | | 19.1 | | 32.1 | 32.1 | | | 12.6 | 12.6 | | 12.6 | |
| Actuated g/C Ratio | | 0.34 | | 0.57 | 0.57 | | | 0.22 | 0.22 | | 0.22 | |
| Clearance Time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | | 514 | | 734 | 1020 | | | 398 | 345 | | 382 | |
| v/s Ratio Prot | | | | c0.11 | 0.12 | | | | | | | |
| v/s Ratio Perm | | c0.16 | | 0.20 | | | | 0.14 | 0.05 | | c0.14 | |
| v/c Ratio | | 0.46 | | 0.54 | 0.22 | | | 0.62 | 0.22 | | 0.62 | |
| Uniform Delay, d1 | | 14.8 | | 7.2 | 6.1 | | | 19.9 | 18.0 | | 19.9 | |
| Progression Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | | 3.0 | | 2.9 | 0.5 | | | 3.0 | 0.3 | | 3.2 | |
| Delay (s) | | 17.7 | | 10.1 | 6.6 | | | 22.9 | 18.3 | | 23.1 | |
| Level of Service | | В | | В | Α | | | С | В | | С | |
| Approach Delay (s) | | 17.7 | | | 8.8 | | | 20.3 | | | 23.1 | |
| Approach LOS | | В | | | А | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 16.1 | Н | CM 2000 | Level of S | Service | | В | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.52 | | | | | | | | | |
| Actuated Cycle Length (s) | - | | 56.7 | S | um of lost | time (s) | | | 14.0 | | | |
| Intersection Capacity Utiliza | ition | | 73.0% | | U Level o | | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Analysis Period (min) c Critical Lane Group

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|--------------------------------|-----------|----------|-------|------|------------|------------|---------|-------|-------------|----------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 4î | | ň | ₽ | | | 4 | | | 4 | |
| Traffic Volume (vph) | 38 | 292 | 33 | 19 | 279 | 17 | 19 | 33 | 15 | 12 | 20 | 17 |
| Future Volume (vph) | 38 | 292 | 33 | 19 | 279 | 17 | 19 | 33 | 15 | 12 | 20 | 17 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frt | 1.00 | 0.98 | | 1.00 | 0.99 | | | 0.97 | | | 0.95 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.99 | | | 0.99 | |
| Satd. Flow (prot) | 1789 | 1803 | | 1789 | 1868 | | | 1802 | | | 1698 | |
| Flt Permitted | 0.57 | 1.00 | | 0.55 | 1.00 | | | 0.88 | | | 0.89 | |
| Satd. Flow (perm) | 1066 | 1803 | | 1035 | 1868 | | | 1616 | | | 1536 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 41 | 317 | 36 | 21 | 303 | 18 | 21 | 36 | 16 | 13 | 22 | 18 |
| RTOR Reduction (vph) | 0 | 5 | 0 | 0 | 3 | 0 | 0 | 14 | 0 | 0 | 16 | 0 |
| Lane Group Flow (vph) | 41 | 348 | 0 | 21 | 318 | 0 | 0 | 59 | 0 | 0 | 37 | 0 |
| Heavy Vehicles (%) | 2% | 5% | 4% | 2% | 2% | 2% | 2% | 2% | 2% | 2% | 5% | 12% |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 33.9 | 33.9 | | 33.9 | 33.9 | | | 5.9 | | | 5.9 | |
| Effective Green, g (s) | 33.9 | 33.9 | | 33.9 | 33.9 | | | 5.9 | | | 5.9 | |
| Actuated g/C Ratio | 0.65 | 0.65 | | 0.65 | 0.65 | | | 0.11 | | | 0.11 | |
| Clearance Time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 697 | 1179 | | 677 | 1222 | | | 184 | | | 174 | |
| v/s Ratio Prot | | c0.19 | | | 0.17 | | | | | | | |
| v/s Ratio Perm | 0.04 | | | 0.02 | | | | c0.04 | | | 0.02 | |
| v/c Ratio | 0.06 | 0.30 | | 0.03 | 0.26 | | | 0.32 | | | 0.21 | |
| Uniform Delay, d1 | 3.2 | 3.8 | | 3.2 | 3.7 | | | 21.1 | | | 20.8 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.2 | 0.6 | | 0.1 | 0.5 | | | 1.0 | | | 0.6 | |
| Delay (s) | 3.4 | 4.5 | | 3.2 | 4.2 | | | 22.1 | | | 21.5 | |
| Level of Service | Α | A | | A | A | | | C | | | C | |
| Approach Delay (s) | | 4.4 | | | 4.2 | | | 22.1 | | | 21.5 | |
| Approach LOS | | А | | | А | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 6.8 | H | CM 2000 | Level of : | Service | | А | | | |
| HCM 2000 Volume to Capac | ity ratio | | 0.30 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 51.8 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utilizat | ion | | 49.9% | IC | U Level o | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| | - | • | • | • | 4 | <i>></i> |
|------------------------------|------------|------|-------|----------|-----------|-------------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † ‡ | | | ^ | | 7 |
| Traffic Volume (veh/h) | 309 | 10 | 0 | 315 | 0 | 5 |
| Future Volume (Veh/h) | 309 | 10 | 0 | 315 | 0 | 5 |
| Sign Control | Free | | | Free | Stop | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 336 | 11 | 0 | 342 | 0 | 5 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | | | None | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | 134 | | | 53 | | |
| pX, platoon unblocked | | | | | 0.99 | |
| vC, conflicting volume | | | 347 | | 512 | 174 |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | | | 347 | | 486 | 174 |
| tC, single (s) | | | 4.2 | | 6.9 | 7.0 |
| tC, 2 stage (s) | | | | | | |
| tF (s) | | | 2.2 | | 3.5 | 3.3 |
| p0 queue free % | | | 100 | | 100 | 99 |
| cM capacity (veh/h) | | | 1187 | | 498 | 830 |
| Direction, Lane # | EB 1 | EB 2 | WB 1 | WB 2 | NB 1 | |
| Volume Total | 224 | 123 | 171 | 171 | 5 | |
| Volume Left | 0 | 0 | 0 | 0 | 0 | |
| Volume Right | 0 | 11 | 0 | 0 | 5 | |
| cSH | 1700 | 1700 | 1700 | 1700 | 830 | |
| Volume to Capacity | 0.13 | 0.07 | 0.10 | 0.10 | 0.01 | |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 9.4 | |
| Lane LOS | | | | | Α | |
| Approach Delay (s) | 0.0 | | 0.0 | | 9.4 | |
| Approach LOS | | | | | Α | |
| Intersection Summary | | | | | | |
| Average Delay | | | 0.1 | | | |
| Intersection Capacity Utiliz | ation | | 18.9% | IC | U Level c | f Service |
| Analysis Period (min) | | | 15 | | | |

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|-------------------------------|-------------|-------------|-------|------|-------------|------------|---------|----------|------|-------------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | † 1> | | ሻ | ∱ Ъ | | | 4 | 7 | | 414 | |
| Traffic Volume (vph) | 67 | 214 | 62 | 50 | 200 | 61 | 56 | 194 | 34 | 57 | 207 | 57 |
| Future Volume (vph) | 67 | 214 | 62 | 50 | 200 | 61 | 56 | 194 | 34 | 57 | 207 | 57 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | | 1.00 | 1.00 | | 0.95 | |
| Frt | 1.00 | 0.97 | | 1.00 | 0.97 | | | 1.00 | 0.85 | | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.99 | 1.00 | | 0.99 | |
| Satd. Flow (prot) | 1738 | 3360 | | 1738 | 3355 | | | 1809 | 1555 | | 3354 | |
| Flt Permitted | 0.52 | 1.00 | | 0.57 | 1.00 | | | 0.82 | 1.00 | | 0.81 | |
| Satd. Flow (perm) | 948 | 3360 | | 1041 | 3355 | | | 1498 | 1555 | | 2750 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 73 | 233 | 67 | 54 | 217 | 66 | 61 | 211 | 37 | 62 | 225 | 62 |
| RTOR Reduction (vph) | 0 | 33 | 0 | 0 | 41 | 0 | 0 | 0 | 27 | 0 | 27 | 0 |
| Lane Group Flow (vph) | 73 | 267 | 0 | 54 | 242 | 0 | 0 | 272 | 10 | 0 | 322 | 0 |
| Turn Type | pm+pt | NA | | Perm | NA | | pm+pt | NA | Perm | Perm | NA | |
| Protected Phases | 5 | 2 | | | 6 | | 3 | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | 27.2 | 27.2 | | 17.2 | 17.2 | | | 14.2 | 14.2 | | 14.2 | |
| Effective Green, g (s) | 27.2 | 27.2 | | 17.2 | 17.2 | | | 14.2 | 14.2 | | 14.2 | |
| Actuated g/C Ratio | 0.51 | 0.51 | | 0.32 | 0.32 | | | 0.27 | 0.27 | | 0.27 | |
| Clearance Time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 601 | 1711 | | 335 | 1080 | | | 398 | 413 | | 731 | |
| v/s Ratio Prot | 0.02 | c0.08 | | | c0.07 | | | | | | | |
| v/s Ratio Perm | 0.04 | | | 0.05 | | | | c0.18 | 0.01 | | 0.12 | |
| v/c Ratio | 0.12 | 0.16 | | 0.16 | 0.22 | | | 0.68 | 0.02 | | 0.44 | |
| Uniform Delay, d1 | 6.7 | 7.0 | | 12.9 | 13.2 | | | 17.6 | 14.5 | | 16.3 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 0.4 | 0.2 | | 1.0 | 0.5 | | | 4.8 | 0.0 | | 0.4 | |
| Delay (s) | 7.2 | 7.2 | | 14.0 | 13.7 | | | 22.4 | 14.5 | | 16.7 | |
| Level of Service | А | Α | | В | В | | | С | В | | В | |
| Approach Delay (s) | | 7.2 | | | 13.7 | | | 21.4 | | | 16.7 | |
| Approach LOS | | Α | | | В | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 14.5 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capa | acity ratio | | 0.39 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 53.4 | | um of lost | | | | 16.0 | | | |
| Intersection Capacity Utiliza | ation | | 53.7% | IC | CU Level of | of Service | 9 | | Α | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-------------------------------|------------|-------|-------|-------|-------------|------------|---------|----------|-------------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | ሻ | 1} | | | र्स | 7 | | 4 | |
| Traffic Volume (vph) | 76 | 271 | 37 | 336 | 220 | 25 | 13 | 207 | 443 | 20 | 246 | 52 |
| Future Volume (vph) | 76 | 271 | 37 | 336 | 220 | 25 | 13 | 207 | 443 | 20 | 246 | 52 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Frt | | 0.99 | | 1.00 | 0.98 | | | 1.00 | 0.85 | | 0.98 | |
| Flt Protected | | 0.99 | | 0.95 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Satd. Flow (prot) | | 1788 | | 1738 | 1802 | | | 1824 | 1555 | | 1783 | |
| Flt Permitted | | 0.87 | | 0.44 | 1.00 | | | 0.97 | 1.00 | | 0.96 | |
| Satd. Flow (perm) | | 1574 | | 812 | 1802 | | | 1768 | 1555 | | 1724 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 83 | 295 | 40 | 365 | 239 | 27 | 14 | 225 | 482 | 22 | 267 | 57 |
| RTOR Reduction (vph) | 0 | 6 | 0 | 0 | 7 | 0 | 0 | 0 | 363 | 0 | 12 | 0 |
| Lane Group Flow (vph) | 0 | 412 | 0 | 365 | 259 | 0 | 0 | 239 | 119 | 0 | 334 | 0 |
| Turn Type | Perm | NA | | pm+pt | NA | | Perm | NA | Perm | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | | 22.0 | | 32.0 | 32.0 | | | 14.4 | 14.4 | | 14.4 | |
| Effective Green, g (s) | | 22.0 | | 32.0 | 32.0 | | | 14.4 | 14.4 | | 14.4 | |
| Actuated g/C Ratio | | 0.38 | | 0.55 | 0.55 | | | 0.25 | 0.25 | | 0.25 | |
| Clearance Time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | | 592 | | 571 | 987 | | | 435 | 383 | | 425 | |
| v/s Ratio Prot | | | | c0.09 | 0.14 | | | | | | | |
| v/s Ratio Perm | | c0.26 | | 0.26 | | | | 0.14 | 0.08 | | c0.19 | |
| v/c Ratio | | 0.70 | | 0.64 | 0.26 | | | 0.55 | 0.31 | | 0.79 | |
| Uniform Delay, d1 | | 15.4 | | 8.5 | 7.0 | | | 19.2 | 17.9 | | 20.6 | |
| Progression Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | | 6.6 | | 5.4 | 0.6 | | | 1.4 | 0.5 | | 9.2 | |
| Delay (s) | | 22.0 | | 13.9 | 7.6 | | | 20.6 | 18.4 | | 29.8 | |
| Level of Service | | С | | В | Α | | | С | В | | С | |
| Approach Delay (s) | | 22.0 | | | 11.3 | | | 19.1 | | | 29.8 | |
| Approach LOS | | С | | | В | | | В | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 19.1 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.71 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 58.4 | | um of lost | | | | 14.0 | | | |
| Intersection Capacity Utiliza | ition | | 87.2% | IC | CU Level of | of Service | ! | | Е | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|--------------------------------|-----------|----------|-------|------|-------------|------------|---------|-------|-------------|----------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ř | f) | | ሻ | f) | | | 4 | | | 4 | |
| Traffic Volume (vph) | 47 | 288 | 49 | 25 | 265 | 21 | 33 | 25 | 26 | 22 | 20 | 29 |
| Future Volume (vph) | 47 | 288 | 49 | 25 | 265 | 21 | 33 | 25 | 26 | 22 | 20 | 29 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frt | 1.00 | 0.98 | | 1.00 | 0.99 | | | 0.96 | | | 0.94 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.98 | | | 0.98 | |
| Satd. Flow (prot) | 1789 | 1792 | | 1789 | 1863 | | | 1770 | | | 1671 | |
| Flt Permitted | 0.57 | 1.00 | | 0.54 | 1.00 | | | 0.84 | | | 0.86 | |
| Satd. Flow (perm) | 1076 | 1792 | | 1023 | 1863 | | | 1510 | | | 1465 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 51 | 313 | 53 | 27 | 288 | 23 | 36 | 27 | 28 | 24 | 22 | 32 |
| RTOR Reduction (vph) | 0 | 8 | 0 | 0 | 4 | 0 | 0 | 25 | 0 | 0 | 28 | 0 |
| Lane Group Flow (vph) | 51 | 358 | 0 | 27 | 307 | 0 | 0 | 66 | 0 | 0 | 50 | 0 |
| Heavy Vehicles (%) | 2% | 5% | 4% | 2% | 2% | 2% | 2% | 2% | 2% | 2% | 5% | 12% |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 33.1 | 33.1 | | 33.1 | 33.1 | | | 6.0 | | | 6.0 | |
| Effective Green, g (s) | 33.1 | 33.1 | | 33.1 | 33.1 | | | 6.0 | | | 6.0 | |
| Actuated g/C Ratio | 0.65 | 0.65 | | 0.65 | 0.65 | | | 0.12 | | | 0.12 | |
| Clearance Time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 696 | 1160 | | 662 | 1206 | | | 177 | | | 172 | |
| v/s Ratio Prot | | c0.20 | | | 0.17 | | | | | | | |
| v/s Ratio Perm | 0.05 | | | 0.03 | | | | c0.04 | | | 0.03 | |
| v/c Ratio | 0.07 | 0.31 | | 0.04 | 0.25 | | | 0.37 | | | 0.29 | |
| Uniform Delay, d1 | 3.3 | 4.0 | | 3.3 | 3.8 | | | 20.8 | | | 20.6 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.2 | 0.7 | | 0.1 | 0.5 | | | 1.3 | | | 0.9 | |
| Delay (s) | 3.5 | 4.7 | | 3.4 | 4.3 | | | 22.2 | | | 21.5 | |
| Level of Service | А | A | | Α | A | | | С | | | C | |
| Approach Delay (s) | | 4.5 | | | 4.2 | | | 22.2 | | | 21.5 | |
| Approach LOS | | Α | | | Α | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 7.6 | H | CM 2000 | Level of | Service | | Α | | | |
| HCM 2000 Volume to Capac | ity ratio | | 0.32 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 51.1 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utilizat | ion | | 57.4% | IC | CU Level of | of Service |) | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-------------------------------|------------|----------|-------|----------|---------|-------------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † ‡ | | | † | | Ť |
| Traffic Volume (veh/h) | 332 | 5 | 0 | 312 | 0 | 10 |
| Future Volume (Veh/h) | 332 | 5 | 0 | 312 | 0 | 10 |
| Sign Control | Free | | | Free | Stop | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 361 | 5 | 0.72 | 339 | 0.72 | 11 |
| Pedestrians | 301 | <u> </u> | O . | 337 | - U | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | | | None | | |
| | None | | | None | | |
| Median storage veh) | 134 | | | 53 | | |
| Upstream signal (m) | 134 | | | 53 | 0.07 | |
| pX, platoon unblocked | | | 2// | | 0.97 | 100 |
| vC, conflicting volume | | | 366 | | 533 | 183 |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | 2// | | 1// | 100 |
| vCu, unblocked vol | | | 366 | | 466 | 183 |
| tC, single (s) | | | 4.2 | | 6.9 | 7.0 |
| tC, 2 stage (s) | | | 2.2 | | 2.5 | 2.2 |
| tF (s) | | | 2.2 | | 3.5 | 3.3 |
| p0 queue free % | | | 100 | | 100 | 99 |
| cM capacity (veh/h) | | | 1168 | | 504 | 819 |
| Direction, Lane # | EB 1 | EB 2 | WB 1 | WB 2 | NB 1 | |
| Volume Total | 241 | 125 | 170 | 170 | 11 | |
| Volume Left | 0 | 0 | 0 | 0 | 0 | |
| Volume Right | 0 | 5 | 0 | 0 | 11 | |
| cSH | 1700 | 1700 | 1700 | 1700 | 819 | |
| Volume to Capacity | 0.14 | 0.07 | 0.10 | 0.10 | 0.01 | |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 | |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 9.5 | |
| Lane LOS | | | | | Α | |
| Approach Delay (s) | 0.0 | | 0.0 | | 9.5 | |
| Approach LOS | | | | | Α | |
| Intersection Summary | | | | | | |
| Average Delay | | | 0.1 | | | |
| Intersection Capacity Utiliza | ation | | 19.3% | IC. | ULevelo | f Service |
| Analysis Period (min) | | | 15 | .0 | 2 20001 | |
| Analysis i Gilou (IIIII) | | | 15 | | | |

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|-------------------------------|-------------|------------|-------|------|-------------|------------|---------|----------|-------------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ↑ ↑ | | ሻ | ∱ Ъ | | | 4 | 7 | | 414 | |
| Traffic Volume (vph) | 71 | 207 | 68 | 34 | 192 | 85 | 94 | 218 | 39 | 49 | 153 | 61 |
| Future Volume (vph) | 71 | 207 | 68 | 34 | 192 | 85 | 94 | 218 | 39 | 49 | 153 | 61 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | | 1.00 | 1.00 | | 0.95 | |
| Frt | 1.00 | 0.96 | | 1.00 | 0.95 | | | 1.00 | 0.85 | | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.99 | 1.00 | | 0.99 | |
| Satd. Flow (prot) | 1738 | 3347 | | 1738 | 3317 | | | 1803 | 1555 | | 3325 | |
| Flt Permitted | 0.51 | 1.00 | | 0.57 | 1.00 | | | 0.79 | 1.00 | | 0.81 | |
| Satd. Flow (perm) | 931 | 3347 | | 1042 | 3317 | | | 1446 | 1555 | | 2733 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 77 | 225 | 74 | 37 | 209 | 92 | 102 | 237 | 42 | 53 | 166 | 66 |
| RTOR Reduction (vph) | 0 | 39 | 0 | 0 | 65 | 0 | 0 | 0 | 29 | 0 | 40 | 0 |
| Lane Group Flow (vph) | 77 | 260 | 0 | 37 | 236 | 0 | 0 | 339 | 13 | 0 | 245 | 0 |
| Turn Type | pm+pt | NA | | Perm | NA | | pm+pt | NA | Perm | Perm | NA | |
| Protected Phases | 5 | 2 | | | 6 | | 3 | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | 27.2 | 27.2 | | 17.1 | 17.1 | | | 18.2 | 18.2 | | 18.2 | |
| Effective Green, g (s) | 27.2 | 27.2 | | 17.1 | 17.1 | | | 18.2 | 18.2 | | 18.2 | |
| Actuated g/C Ratio | 0.47 | 0.47 | | 0.30 | 0.30 | | | 0.32 | 0.32 | | 0.32 | |
| Clearance Time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 555 | 1586 | | 310 | 988 | | | 458 | 493 | | 866 | |
| v/s Ratio Prot | 0.02 | c0.08 | | | c0.07 | | | | | | | |
| v/s Ratio Perm | 0.05 | | | 0.04 | | | | c0.23 | 0.01 | | 0.09 | |
| v/c Ratio | 0.14 | 0.16 | | 0.12 | 0.24 | | | 0.74 | 0.03 | | 0.28 | |
| Uniform Delay, d1 | 8.4 | 8.6 | | 14.7 | 15.2 | | | 17.5 | 13.5 | | 14.7 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 0.5 | 0.2 | | 0.8 | 0.6 | | | 6.3 | 0.0 | | 0.2 | |
| Delay (s) | 8.9 | 8.8 | | 15.5 | 15.8 | | | 23.8 | 13.5 | | 14.9 | |
| Level of Service | А | Α | | В | В | | | С | В | | В | |
| Approach Delay (s) | | 8.8 | | | 15.8 | | | 22.7 | | | 14.9 | |
| Approach LOS | | Α | | | В | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 15.6 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capa | acity ratio | | 0.45 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 57.4 | | um of lost | | | | 16.0 | | | |
| Intersection Capacity Utiliza | ation | | 55.5% | IC | CU Level of | of Service |) | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-----------------------------------|----------|----------|-------|-------|------------|------------|---------|----------|-------------|-------------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | ħ | f) | | | र्स | 7 | | 4 | |
| Traffic Volume (vph) | 69 | 171 | 23 | 404 | 229 | 22 | 11 | 240 | 343 | 19 | 203 | 30 |
| Future Volume (vph) | 69 | 171 | 23 | 404 | 229 | 22 | 11 | 240 | 343 | 19 | 203 | 30 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Frt | | 0.99 | | 1.00 | 0.99 | | | 1.00 | 0.85 | | 0.98 | |
| Flt Protected | | 0.99 | | 0.95 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Satd. Flow (prot) | | 1785 | | 1738 | 1806 | | | 1826 | 1555 | | 1793 | |
| Flt Permitted | | 0.83 | | 0.54 | 1.00 | | | 0.98 | 1.00 | | 0.95 | |
| Satd. Flow (perm) | | 1507 | | 986 | 1806 | | | 1793 | 1555 | | 1714 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 75 | 186 | 25 | 439 | 249 | 24 | 12 | 261 | 373 | 21 | 221 | 33 |
| RTOR Reduction (vph) | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 287 | 0 | 8 | 0 |
| Lane Group Flow (vph) | 0 | 281 | 0 | 439 | 268 | 0 | 0 | 273 | 86 | 0 | 267 | 0 |
| Turn Type | Perm | NA | | pm+pt | NA | | Perm | NA | Perm | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | | 19.1 | | 32.1 | 32.1 | | | 13.2 | 13.2 | | 13.2 | |
| Effective Green, g (s) | | 19.1 | | 32.1 | 32.1 | | | 13.2 | 13.2 | | 13.2 | |
| Actuated g/C Ratio | | 0.33 | | 0.56 | 0.56 | | | 0.23 | 0.23 | | 0.23 | |
| Clearance Time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | | 502 | | 696 | 1011 | | | 413 | 358 | | 394 | |
| v/s Ratio Prot | | | | c0.12 | 0.15 | | | | | | | |
| v/s Ratio Perm | | c0.19 | | 0.23 | | | | 0.15 | 0.06 | | c0.16 | |
| v/c Ratio | | 0.56 | | 0.63 | 0.26 | | | 0.66 | 0.24 | | 0.68 | |
| Uniform Delay, d1 | | 15.6 | | 7.9 | 6.5 | | | 20.0 | 18.0 | | 20.1 | |
| Progression Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | | 4.4 | | 4.3 | 0.6 | | | 3.9 | 0.3 | | 4.6 | |
| Delay (s) | | 20.1 | | 12.2 | 7.1 | | | 24.0 | 18.3 | | 24.7 | |
| Level of Service | | С | | В | А | | | С | В | | С | |
| Approach Delay (s) | | 20.1 | | | 10.3 | | | 20.7 | | | 24.7 | |
| Approach LOS | | С | | | В | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 17.3 | Н | CM 2000 | Level of S | Service | | В | | | |
| HCM 2000 Volume to Capaci | ty ratio | | 0.61 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 57.3 | S | um of lost | time (s) | | | 14.0 | | | |
| Intersection Capacity Utilization | on | | 80.1% | | CU Level o | | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-------------------------------|------------|-------|-------|------|----------------|------------|---------|----------|----------|------|------|------|
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| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ۲ | î, | | ۲ | (Î | | | 4 | | | 4 | |
| Traffic Volume (vph) | 40 | 322 | 35 | 19 | 307 | 18 | 20 | 35 | 16 | 12 | 21 | 18 |
| Future Volume (vph) | 40 | 322 | 35 | 19 | 307 | 18 | 20 | 35 | 16 | 12 | 21 | 18 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frt | 1.00 | 0.99 | | 1.00 | 0.99 | | | 0.97 | | | 0.95 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.99 | | | 0.99 | |
| Satd. Flow (prot) | 1789 | 1804 | | 1789 | 1867 | | | 1802 | | | 1692 | |
| Flt Permitted | 0.55 | 1.00 | | 0.53 | 1.00 | | | 0.88 | | | 0.90 | |
| Satd. Flow (perm) | 1034 | 1804 | | 1003 | 1867 | | | 1615 | | | 1536 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 43 | 350 | 38 | 21 | 334 | 20 | 22 | 38 | 17 | 13 | 23 | 20 |
| RTOR Reduction (vph) | 0 | 5 | 0 | 0 | 3 | 0 | 0 | 15 | 0 | 0 | 18 | 0 |
| Lane Group Flow (vph) | 43 | 383 | 0 | 21 | 351 | 0 | 0 | 62 | 0 | 0 | 38 | 0 |
| Heavy Vehicles (%) | 2% | 5% | 4% | 2% | 2% | 2% | 2% | 2% | 2% | 2% | 5% | 12% |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 33.6 | 33.6 | | 33.6 | 33.6 | | | 5.9 | | | 5.9 | |
| Effective Green, g (s) | 33.6 | 33.6 | | 33.6 | 33.6 | | | 5.9 | | | 5.9 | |
| Actuated g/C Ratio | 0.65 | 0.65 | | 0.65 | 0.65 | | | 0.11 | | | 0.11 | |
| Clearance Time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 674 | 1176 | | 654 | 1218 | | | 185 | | | 175 | |
| v/s Ratio Prot | | c0.21 | | | 0.19 | | | | | | | |
| v/s Ratio Perm | 0.04 | | | 0.02 | | | | c0.04 | | | 0.02 | |
| v/c Ratio | 0.06 | 0.33 | | 0.03 | 0.29 | | | 0.33 | | | 0.22 | |
| Uniform Delay, d1 | 3.2 | 4.0 | | 3.2 | 3.8 | | | 21.0 | | | 20.7 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.2 | 0.7 | | 0.1 | 0.6 | | | 1.1 | | | 0.6 | |
| Delay (s) | 3.4 | 4.7 | | 3.3 | 4.4 | | | 22.1 | | | 21.3 | |
| Level of Service | А | A | | А | Α | | | C | | | C | |
| Approach Delay (s) | | 4.6 | | | 4.4 | | | 22.1 | | | 21.3 | |
| Approach LOS | | А | | | Α | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 6.9 | Н | CM 2000 | Level of | Service | | А | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.33 | | | | | | | | | |
| Actuated Cycle Length (s) | ,, | | 51.5 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utiliza | tion | | 51.6% | IC | U Level | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| | → | • | • | ← | 4 | <i>></i> |
|-------------------------------|------------|------|--------|------------|------------|-------------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † ‡ | | | † † | | 7 |
| Traffic Volume (veh/h) | 341 | 10 | 0 | 347 | 0 | 5 |
| Future Volume (Veh/h) | 341 | 10 | 0 | 347 | 0 | 5 |
| Sign Control | Free | | | Free | Stop | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 371 | 11 | 0.72 | 377 | 0.72 | 5 |
| Pedestrians | 371 | - '' | - U | 377 | - U | 3 |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | | | None | | |
| | None | | | None | | |
| Median storage veh) | 134 | | | 53 | | |
| Upstream signal (m) | 134 | | | 53 | 0.00 | |
| pX, platoon unblocked | | | 202 | | 0.98 | 101 |
| vC, conflicting volume | | | 382 | | 565 | 191 |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | 202 | | Г11 | 101 |
| vCu, unblocked vol | | | 382 | | 511 | 191 |
| tC, single (s) | | | 4.2 | | 6.9 | 7.0 |
| tC, 2 stage (s) | | | 2.2 | | 2.5 | 2.2 |
| tF (s) | | | 2.2 | | 3.5 | 3.3 |
| p0 queue free % | | | 100 | | 100 | 99 |
| cM capacity (veh/h) | | | 1152 | | 474 | 809 |
| Direction, Lane # | EB 1 | EB 2 | WB 1 | WB 2 | NB 1 | |
| Volume Total | 247 | 135 | 188 | 188 | 5 | |
| Volume Left | 0 | 0 | 0 | 0 | 0 | |
| Volume Right | 0 | 11 | 0 | 0 | 5 | |
| cSH | 1700 | 1700 | 1700 | 1700 | 809 | |
| Volume to Capacity | 0.15 | 0.08 | 0.11 | 0.11 | 0.01 | |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 9.5 | |
| Lane LOS | | | | | Α | |
| Approach Delay (s) | 0.0 | | 0.0 | | 9.5 | |
| Approach LOS | | | | | Α | |
| Intersection Summary | | | | | | |
| Average Delay | | | 0.1 | | | |
| Intersection Capacity Utiliza | ation | | 19.7% | IC | III evel d | f Service |
| Analysis Period (min) | auon | | 15.776 | 10 | O LOVOI C | , JOI VICE |
| Aliaiysis Feliou (IIIIII) | | | 13 | | | |

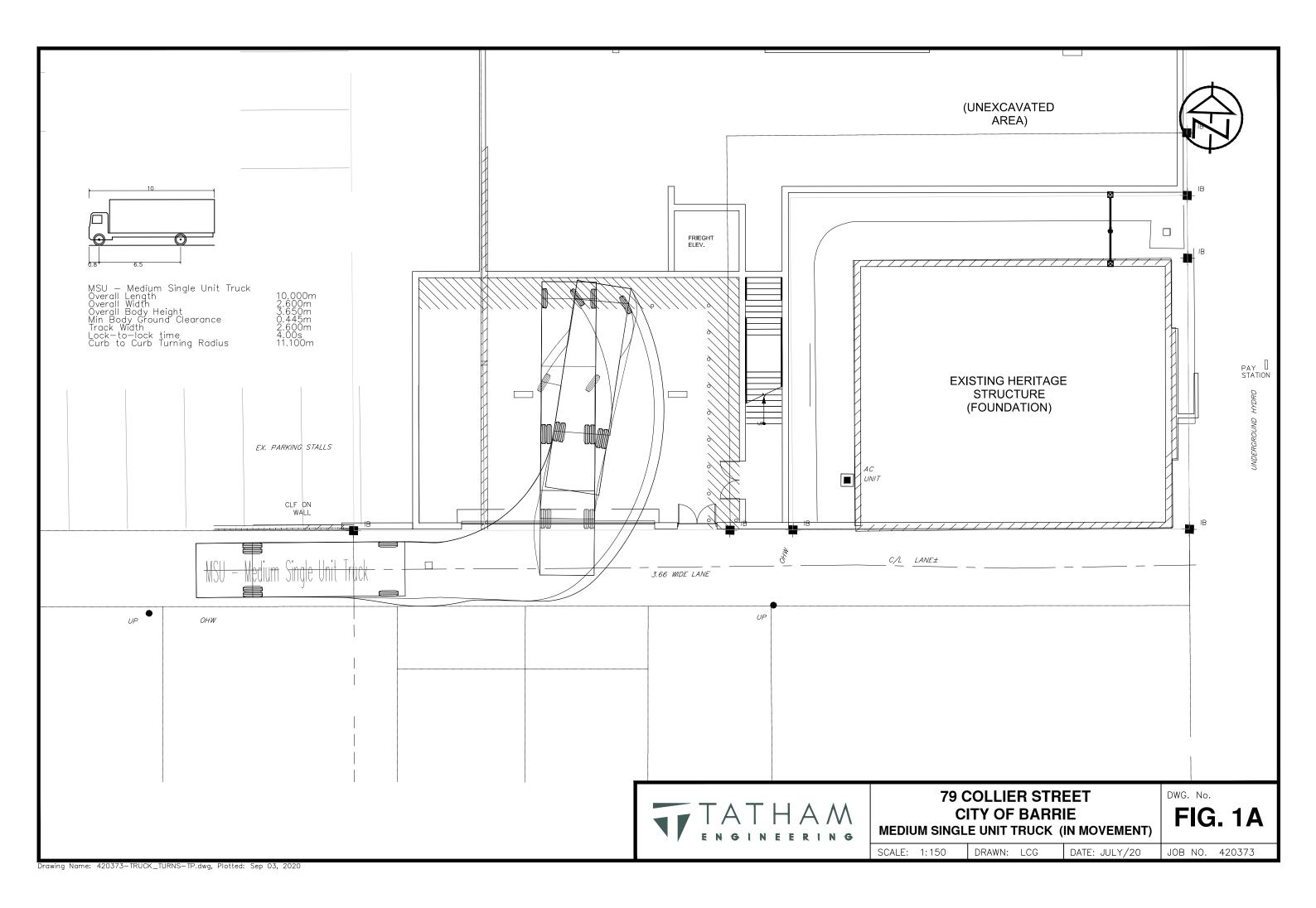
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|-------------------------------|-------------|----------|-------|------|-------------|------------|---------|----------|-------------|----------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ۲ | ħβ | | ň | ∱ Ъ | | | 4 | 7 | | 414 | |
| Traffic Volume (vph) | 73 | 235 | 69 | 55 | 220 | 67 | 61 | 214 | 38 | 63 | 229 | 62 |
| Future Volume (vph) | 73 | 235 | 69 | 55 | 220 | 67 | 61 | 214 | 38 | 63 | 229 | 62 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | | 1.00 | 1.00 | | 0.95 | |
| Frt | 1.00 | 0.97 | | 1.00 | 0.96 | | | 1.00 | 0.85 | | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.99 | 1.00 | | 0.99 | |
| Satd. Flow (prot) | 1738 | 3358 | | 1738 | 3354 | | | 1810 | 1555 | | 3356 | |
| Flt Permitted | 0.50 | 1.00 | | 0.55 | 1.00 | | | 0.81 | 1.00 | | 0.79 | |
| Satd. Flow (perm) | 921 | 3358 | | 1011 | 3354 | | | 1487 | 1555 | | 2670 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 79 | 255 | 75 | 60 | 239 | 73 | 66 | 233 | 41 | 68 | 249 | 67 |
| RTOR Reduction (vph) | 0 | 36 | 0 | 0 | 41 | 0 | 0 | 0 | 29 | 0 | 26 | 0 |
| Lane Group Flow (vph) | 79 | 294 | 0 | 60 | 271 | 0 | 0 | 299 | 12 | 0 | 358 | 0 |
| Turn Type | pm+pt | NA | | Perm | NA | | pm+pt | NA | Perm | Perm | NA | |
| Protected Phases | 5 | 2 | | | 6 | | 3 | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | 27.2 | 27.2 | | 17.1 | 17.1 | | | 15.5 | 15.5 | | 15.5 | |
| Effective Green, g (s) | 27.2 | 27.2 | | 17.1 | 17.1 | | | 15.5 | 15.5 | | 15.5 | |
| Actuated g/C Ratio | 0.50 | 0.50 | | 0.31 | 0.31 | | | 0.28 | 0.28 | | 0.28 | |
| Clearance Time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 578 | 1669 | | 316 | 1048 | | | 421 | 440 | | 756 | |
| v/s Ratio Prot | 0.02 | c0.09 | | | c0.08 | | | | | | | |
| v/s Ratio Perm | 0.05 | | | 0.06 | | | | c0.20 | 0.01 | | 0.13 | |
| v/c Ratio | 0.14 | 0.18 | | 0.19 | 0.26 | | | 0.71 | 0.03 | | 0.47 | |
| Uniform Delay, d1 | 7.3 | 7.6 | | 13.7 | 14.1 | | | 17.6 | 14.2 | | 16.2 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 0.5 | 0.2 | | 1.3 | 0.6 | | | 5.6 | 0.0 | | 0.5 | |
| Delay (s) | 7.8 | 7.8 | | 15.1 | 14.7 | | | 23.2 | 14.2 | | 16.7 | |
| Level of Service | Α | Α | | В | В | | | С | В | | В | |
| Approach Delay (s) | | 7.8 | | | 14.7 | | | 22.1 | | | 16.7 | |
| Approach LOS | | А | | | В | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 15.0 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capa | acity ratio | | 0.43 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 54.7 | | um of lost | | | | 16.0 | | | |
| Intersection Capacity Utiliza | ation | | 56.8% | IC | CU Level of | of Service | 9 | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

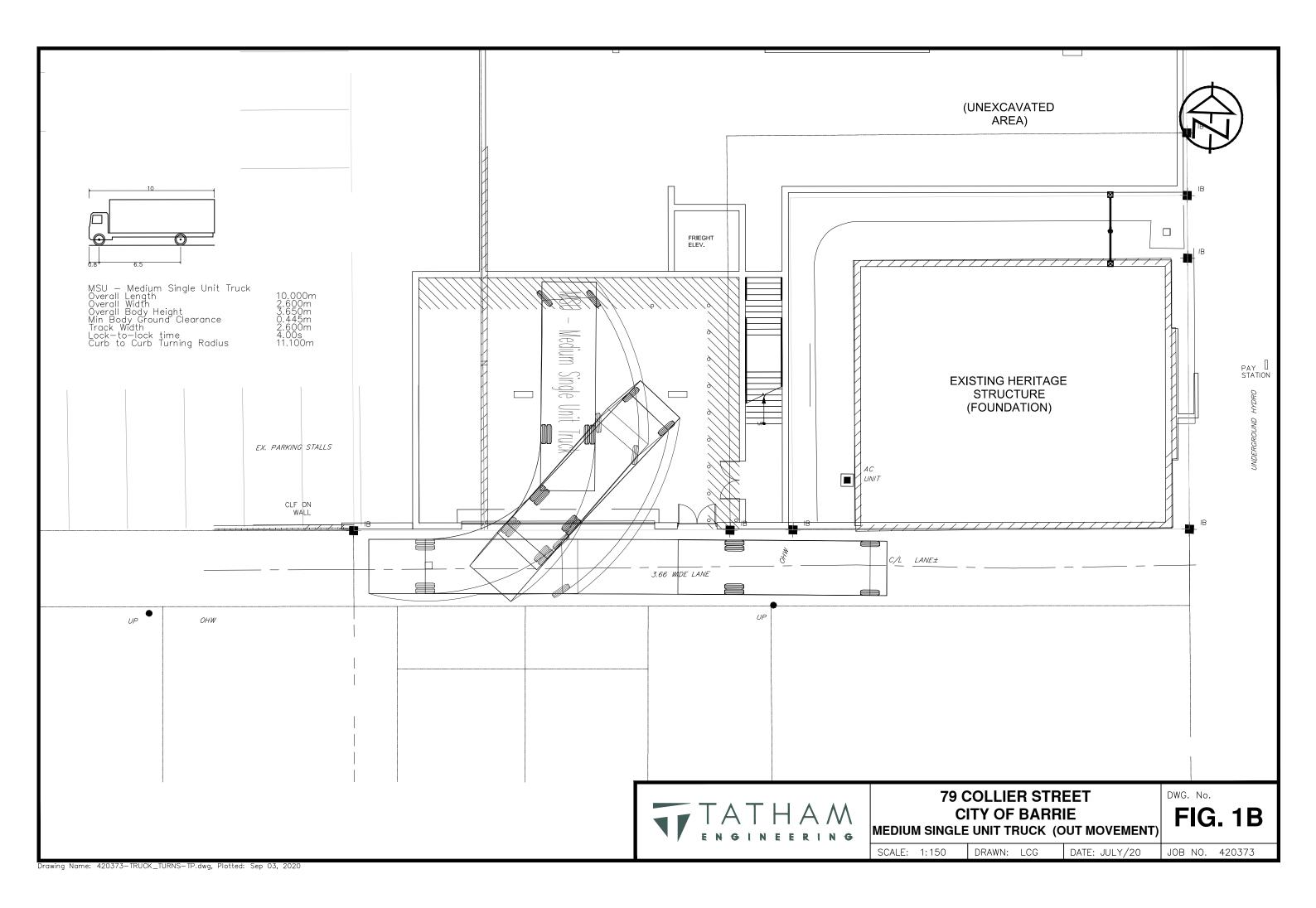
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|-----------------------------------|----------|----------|-------|-------|------------|------------|---------|----------|-------------|----------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | ħ | f) | | | र्स | 7 | | 4 | |
| Traffic Volume (vph) | 84 | 328 | 41 | 369 | 265 | 28 | 14 | 228 | 487 | 21 | 271 | 57 |
| Future Volume (vph) | 84 | 328 | 41 | 369 | 265 | 28 | 14 | 228 | 487 | 21 | 271 | 57 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Frt | | 0.99 | | 1.00 | 0.99 | | | 1.00 | 0.85 | | 0.98 | |
| Flt Protected | | 0.99 | | 0.95 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Satd. Flow (prot) | | 1791 | | 1738 | 1804 | | | 1824 | 1555 | | 1784 | |
| Flt Permitted | | 0.86 | | 0.39 | 1.00 | | | 0.96 | 1.00 | | 0.96 | |
| Satd. Flow (perm) | | 1561 | | 713 | 1804 | | | 1761 | 1555 | | 1725 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 91 | 357 | 45 | 401 | 288 | 30 | 15 | 248 | 529 | 23 | 295 | 62 |
| RTOR Reduction (vph) | 0 | 6 | 0 | 0 | 6 | 0 | 0 | 0 | 385 | 0 | 12 | 0 |
| Lane Group Flow (vph) | 0 | 487 | 0 | 401 | 312 | 0 | 0 | 263 | 144 | 0 | 368 | 0 |
| Turn Type | Perm | NA | | pm+pt | NA | | Perm | NA | Perm | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | | 22.0 | | 32.0 | 32.0 | | | 15.1 | 15.1 | | 15.1 | |
| Effective Green, g (s) | | 22.0 | | 32.0 | 32.0 | | | 15.1 | 15.1 | | 15.1 | |
| Actuated g/C Ratio | | 0.37 | | 0.54 | 0.54 | | | 0.26 | 0.26 | | 0.26 | |
| Clearance Time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | | 581 | | 524 | 976 | | | 449 | 397 | | 440 | |
| v/s Ratio Prot | | | | c0.10 | 0.17 | | | | | | | |
| v/s Ratio Perm | | c0.31 | | 0.31 | | | | 0.15 | 0.09 | | c0.21 | |
| v/c Ratio | | 0.84 | | 0.77 | 0.32 | | | 0.59 | 0.36 | | 0.84 | |
| Uniform Delay, d1 | | 16.9 | | 9.6 | 7.5 | | | 19.3 | 18.1 | | 20.8 | |
| Progression Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | | 13.5 | | 10.2 | 0.9 | | | 2.0 | 0.6 | | 13.0 | |
| Delay (s) | | 30.4 | | 19.8 | 8.4 | | | 21.2 | 18.6 | | 33.8 | |
| Level of Service | | С | | В | А | | | С | В | | С | |
| Approach Delay (s) | | 30.4 | | | 14.8 | | | 19.5 | | | 33.8 | |
| Approach LOS | | С | | | В | | | В | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 22.6 | Н | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capacit | ty ratio | | 0.82 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 59.1 | S | um of lost | time (s) | | | 14.0 | | | |
| Intersection Capacity Utilization | on | | 95.2% | | CU Level o | | | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

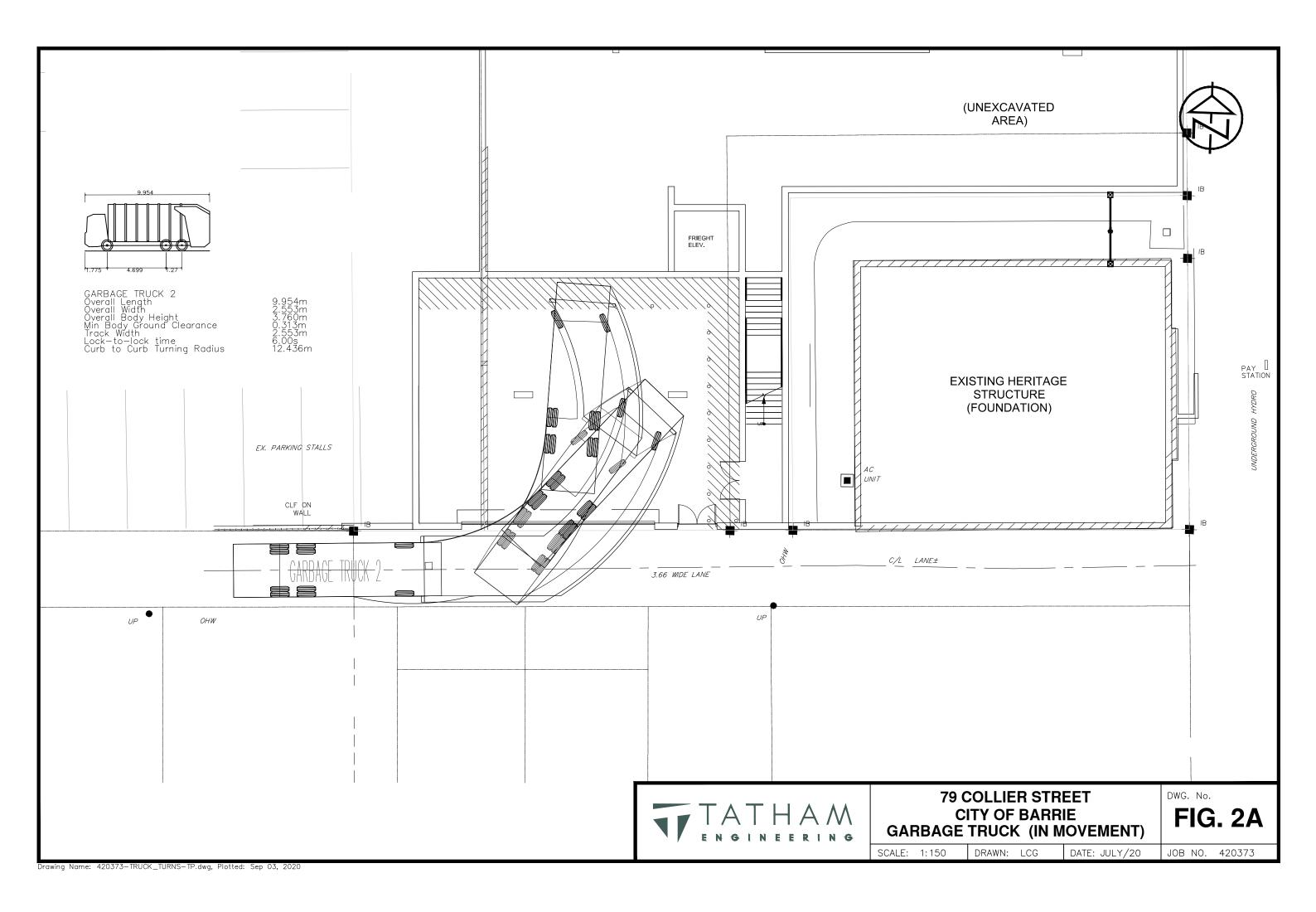
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|-------------------------------|------------|-------|-------|------|-------------|------------|---------|----------|------|------|------|------|
| | ۶ | - | • | • | ← | • | • | † | ~ | - | ţ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ¥ | 4î | | ሻ | f) | | | 4 | | | 4 | |
| Traffic Volume (vph) | 49 | 317 | 51 | 26 | 293 | 22 | 35 | 27 | 27 | 23 | 21 | 30 |
| Future Volume (vph) | 49 | 317 | 51 | 26 | 293 | 22 | 35 | 27 | 27 | 23 | 21 | 30 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frt | 1.00 | 0.98 | | 1.00 | 0.99 | | | 0.96 | | | 0.94 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.98 | | | 0.98 | |
| Satd. Flow (prot) | 1789 | 1794 | | 1789 | 1864 | | | 1772 | | | 1672 | |
| Flt Permitted | 0.56 | 1.00 | | 0.53 | 1.00 | | | 0.83 | | | 0.86 | |
| Satd. Flow (perm) | 1046 | 1794 | | 992 | 1864 | | | 1508 | | | 1462 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 53 | 345 | 55 | 28 | 318 | 24 | 38 | 29 | 29 | 25 | 23 | 33 |
| RTOR Reduction (vph) | 0 | 7 | 0 | 0 | 4 | 0 | 0 | 26 | 0 | 0 | 29 | 0 |
| Lane Group Flow (vph) | 53 | 393 | 0 | 28 | 338 | 0 | 0 | 70 | 0 | 0 | 52 | 0 |
| Heavy Vehicles (%) | 2% | 5% | 4% | 2% | 2% | 2% | 2% | 2% | 2% | 2% | 5% | 12% |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 33.1 | 33.1 | | 33.1 | 33.1 | | | 6.1 | | | 6.1 | |
| Effective Green, g (s) | 33.1 | 33.1 | | 33.1 | 33.1 | | | 6.1 | | | 6.1 | |
| Actuated g/C Ratio | 0.65 | 0.65 | | 0.65 | 0.65 | | | 0.12 | | | 0.12 | |
| Clearance Time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 676 | 1159 | | 641 | 1205 | | | 179 | | | 174 | |
| v/s Ratio Prot | | c0.22 | | | 0.18 | | | | | | | |
| v/s Ratio Perm | 0.05 | | | 0.03 | | | | c0.05 | | | 0.04 | |
| v/c Ratio | 0.08 | 0.34 | | 0.04 | 0.28 | | | 0.39 | | | 0.30 | |
| Uniform Delay, d1 | 3.4 | 4.1 | | 3.3 | 3.9 | | | 20.8 | | | 20.6 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.2 | 0.8 | | 0.1 | 0.6 | | | 1.4 | | | 1.0 | |
| Delay (s) | 3.6 | 4.9 | | 3.4 | 4.5 | | | 22.3 | | | 21.6 | |
| Level of Service | Α | Α | | Α | A | | | C | | | C | |
| Approach Delay (s) | | 4.7 | | | 4.4 | | | 22.3 | | | 21.6 | |
| Approach LOS | | А | | | Α | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 7.7 | Н | CM 2000 | Level of | Service | | Α | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.35 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 51.2 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utiliza | tion | | 59.1% | IC | CU Level of | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

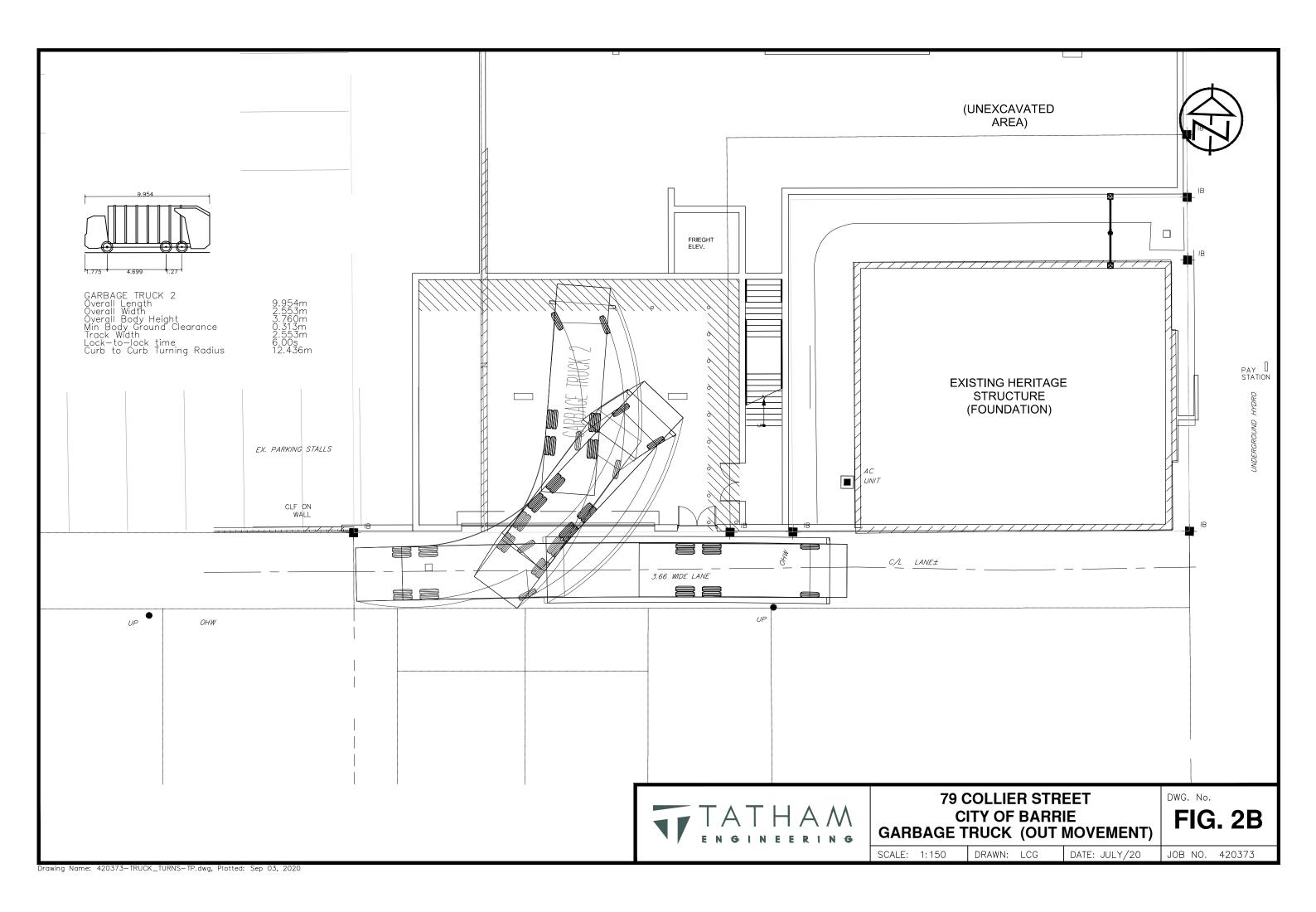
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|-------------------------------|------------|------|-------|------------|-----------|-------------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † ‡ | | | † † | | 7 |
| Traffic Volume (veh/h) | 367 | 5 | 0 | 344 | 0 | 10 |
| Future Volume (Veh/h) | 367 | 5 | 0 | 344 | 0 | 10 |
| Sign Control | Free | | | Free | Stop | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 399 | 5 | 0 | 374 | 0 | 11 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | | | None | | |
| Median storage veh) | None | | | NOTIC | | |
| Upstream signal (m) | 134 | | | 53 | | |
| pX, platoon unblocked | 134 | | | 55 | 0.96 | |
| vC, conflicting volume | | | 404 | | 588 | 202 |
| | | | 404 | | 300 | 202 |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | 101 | | 407 | 202 |
| vCu, unblocked vol | | | 404 | | 497 | 202 |
| tC, single (s) | | | 4.2 | | 6.9 | 7.0 |
| tC, 2 stage (s) | | | 0.0 | | 0.5 | 0.0 |
| tF (s) | | | 2.2 | | 3.5 | 3.3 |
| p0 queue free % | | | 100 | | 100 | 99 |
| cM capacity (veh/h) | | | 1130 | | 477 | 796 |
| Direction, Lane # | EB 1 | EB 2 | WB 1 | WB 2 | NB 1 | |
| Volume Total | 266 | 138 | 187 | 187 | 11 | |
| Volume Left | 0 | 0 | 0 | 0 | 0 | |
| Volume Right | 0 | 5 | 0 | 0 | 11 | |
| cSH | 1700 | 1700 | 1700 | 1700 | 796 | |
| Volume to Capacity | 0.16 | 0.08 | 0.11 | 0.11 | 0.01 | |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 | |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 9.6 | |
| Lane LOS | | | | | A | |
| Approach Delay (s) | 0.0 | | 0.0 | | 9.6 | |
| Approach LOS | | | | | Α | |
| Intersection Summary | | | | | | |
| Average Delay | | | 0.1 | | | |
| Intersection Capacity Utiliza | ation | | 20.3% | IC | U Level o | f Service |
| Analysis Period (min) | I | | 15 | 10 | 2 200010 | . 50, 1100 |
| Alialysis Fellou (IIIIII) | | | 10 | | | |

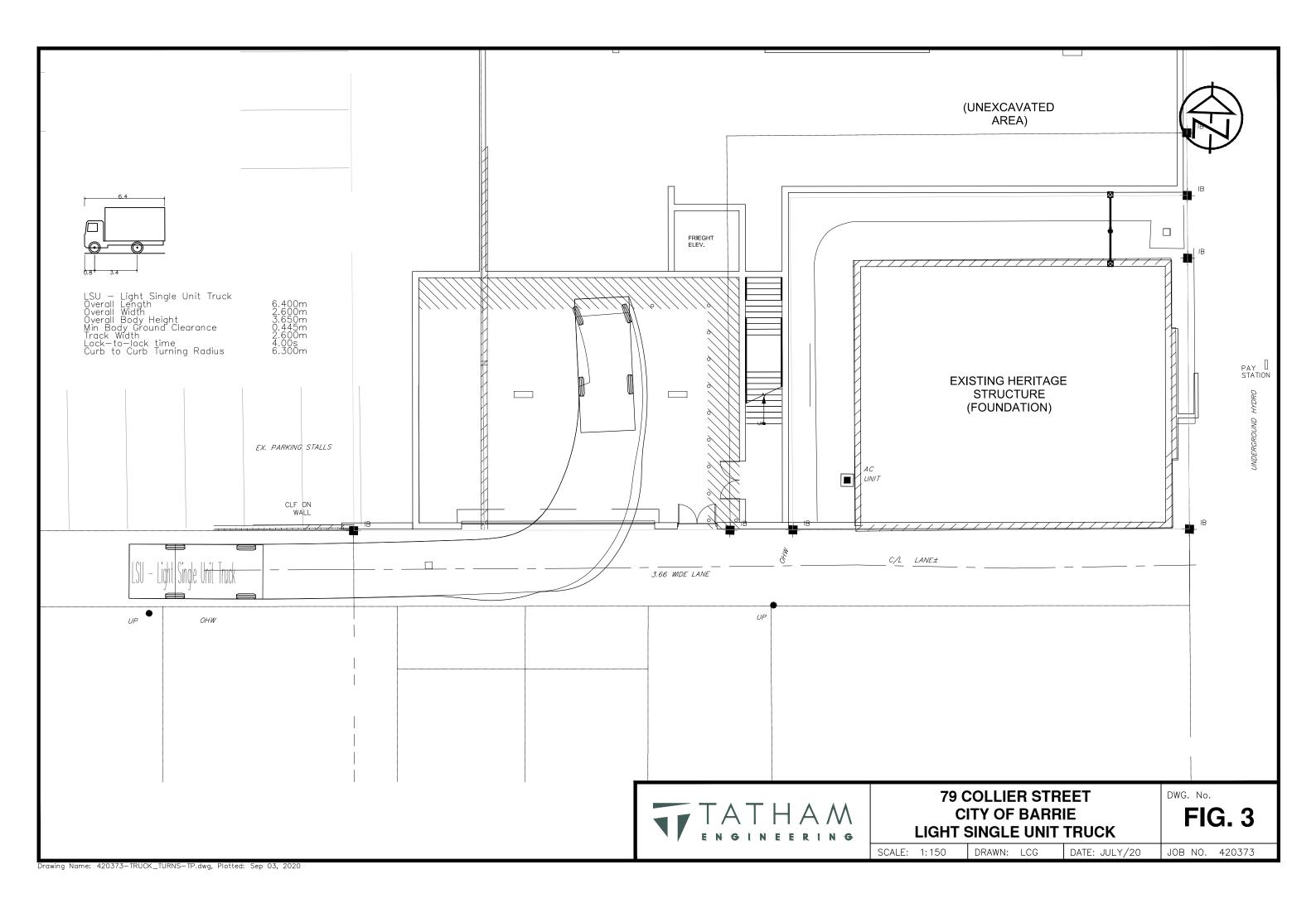
Appendix E: AutoTurn Assesment











Appendix F: Future Total Operations

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|------------------------------|-------------|------------|-------|------|------------|----------|---------|----------|-------------|----------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | Ť | ↑ ↑ | | ň | ↑ ↑ | | | 4 | 7 | | 414 | |
| Traffic Volume (vph) | 76 | 190 | 78 | 31 | 174 | 77 | 85 | 198 | 36 | 45 | 139 | 55 |
| Future Volume (vph) | 76 | 190 | 78 | 31 | 174 | 77 | 85 | 198 | 36 | 45 | 139 | 55 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | | 1.00 | 1.00 | | 0.95 | |
| Frt | 1.00 | 0.96 | | 1.00 | 0.95 | | | 1.00 | 0.85 | | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.99 | 1.00 | | 0.99 | |
| Satd. Flow (prot) | 1738 | 3325 | | 1738 | 3316 | | | 1803 | 1555 | | 3325 | |
| Flt Permitted | 0.52 | 1.00 | | 0.57 | 1.00 | | | 0.80 | 1.00 | | 0.83 | |
| Satd. Flow (perm) | 956 | 3325 | | 1049 | 3316 | | | 1465 | 1555 | | 2795 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 83 | 207 | 85 | 34 | 189 | 84 | 92 | 215 | 39 | 49 | 151 | 60 |
| RTOR Reduction (vph) | 0 | 43 | 0 | 0 | 58 | 0 | 0 | 0 | 28 | 0 | 40 | 0 |
| Lane Group Flow (vph) | 83 | 249 | 0 | 34 | 215 | 0 | 0 | 307 | 11 | 0 | 220 | 0 |
| Turn Type | pm+pt | NA | | Perm | NA | | pm+pt | NA | Perm | Perm | NA | |
| Protected Phases | 5 | 2 | | | 6 | | 3 | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | 27.2 | 27.2 | | 17.1 | 17.1 | | | 16.3 | 16.3 | | 16.3 | |
| Effective Green, g (s) | 27.2 | 27.2 | | 17.1 | 17.1 | | | 16.3 | 16.3 | | 16.3 | |
| Actuated g/C Ratio | 0.49 | 0.49 | | 0.31 | 0.31 | | | 0.29 | 0.29 | | 0.29 | |
| Clearance Time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 582 | 1629 | | 323 | 1021 | | | 430 | 456 | | 820 | |
| v/s Ratio Prot | 0.02 | c0.07 | | | c0.06 | | | | | | | |
| v/s Ratio Perm | 0.05 | | | 0.03 | | | | c0.21 | 0.01 | | 0.08 | |
| v/c Ratio | 0.14 | 0.15 | | 0.11 | 0.21 | | | 0.71 | 0.03 | | 0.27 | |
| Uniform Delay, d1 | 7.6 | 7.8 | | 13.7 | 14.2 | | | 17.5 | 13.9 | | 15.0 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 0.5 | 0.2 | | 0.7 | 0.5 | | | 5.5 | 0.0 | | 0.2 | |
| Delay (s) | 8.1 | 8.0 | | 14.4 | 14.7 | | | 23.1 | 14.0 | | 15.2 | |
| Level of Service | А | Α | | В | В | | | С | В | | В | |
| Approach Delay (s) | | 8.0 | | | 14.6 | | | 22.0 | | | 15.2 | |
| Approach LOS | | Α | | | В | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 14.8 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capa | acity ratio | | 0.41 | | | | | | | | | |
| Actuated Cycle Length (s) | • | | 55.5 | S | um of lost | time (s) | | | 16.0 | | | |
| Intersection Capacity Utiliz | ation | | 53.1% | | CU Level o | | е | | Α | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Analysis Period (min) c Critical Lane Group

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|-------------------------------|------------|-------|-------|-------|-------------|------------|---------|----------|----------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | ሻ | 1> | | | 4 | 7 | | 4 | |
| Traffic Volume (vph) | 62 | 141 | 21 | 367 | 190 | 20 | 10 | 218 | 312 | 17 | 189 | 38 |
| Future Volume (vph) | 62 | 141 | 21 | 367 | 190 | 20 | 10 | 218 | 312 | 17 | 189 | 38 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Frt | | 0.99 | | 1.00 | 0.99 | | | 1.00 | 0.85 | | 0.98 | |
| Flt Protected | | 0.99 | | 0.95 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Satd. Flow (prot) | | 1782 | | 1738 | 1803 | | | 1826 | 1555 | | 1785 | |
| Flt Permitted | | 0.85 | | 0.58 | 1.00 | | | 0.98 | 1.00 | | 0.96 | |
| Satd. Flow (perm) | | 1527 | | 1068 | 1803 | | | 1794 | 1555 | | 1719 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 67 | 153 | 23 | 399 | 207 | 22 | 11 | 237 | 339 | 18 | 205 | 41 |
| RTOR Reduction (vph) | 0 | 6 | 0 | 0 | 6 | 0 | 0 | 0 | 263 | 0 | 12 | 0 |
| Lane Group Flow (vph) | 0 | 237 | 0 | 399 | 223 | 0 | 0 | 248 | 76 | 0 | 252 | 0 |
| Turn Type | Perm | NA | | pm+pt | NA | | Perm | NA | Perm | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | | 19.1 | | 32.1 | 32.1 | | | 12.7 | 12.7 | | 12.7 | |
| Effective Green, g (s) | | 19.1 | | 32.1 | 32.1 | | | 12.7 | 12.7 | | 12.7 | |
| Actuated g/C Ratio | | 0.34 | | 0.57 | 0.57 | | | 0.22 | 0.22 | | 0.22 | |
| Clearance Time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | | 513 | | 733 | 1018 | | | 401 | 347 | | 384 | |
| v/s Ratio Prot | | | | c0.11 | 0.12 | | | | | | | |
| v/s Ratio Perm | | c0.16 | | 0.20 | | | | 0.14 | 0.05 | | c0.15 | |
| v/c Ratio | | 0.46 | | 0.54 | 0.22 | | | 0.62 | 0.22 | | 0.66 | |
| Uniform Delay, d1 | | 14.8 | | 7.3 | 6.1 | | | 19.9 | 18.0 | | 20.1 | |
| Progression Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | | 3.0 | | 2.9 | 0.5 | | | 2.8 | 0.3 | | 4.0 | |
| Delay (s) | | 17.8 | | 10.2 | 6.6 | | | 22.7 | 18.3 | | 24.1 | |
| Level of Service | | В | | В | Α | | | С | В | | С | |
| Approach Delay (s) | | 17.8 | | | 8.9 | | | 20.2 | | | 24.1 | |
| Approach LOS | | В | | | А | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 16.3 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.53 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 56.8 | | um of lost | | | | 14.0 | | | |
| Intersection Capacity Utiliza | ition | | 74.0% | IC | CU Level of | of Service | : | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

| e: ewen eneet a e | , o | | | | | | | | | | | |
|-------------------------------|------------|----------|-------|------|----------------|------------|---------|----------|------|------|------|------|
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| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ۲ | 4 | | ۲ | (Î | | | 4 | | | 4 | |
| Traffic Volume (vph) | 38 | 299 | 33 | 19 | 279 | 17 | 19 | 33 | 16 | 14 | 20 | 17 |
| Future Volume (vph) | 38 | 299 | 33 | 19 | 279 | 17 | 19 | 33 | 16 | 14 | 20 | 17 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frt | 1.00 | 0.99 | | 1.00 | 0.99 | | | 0.97 | | | 0.96 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.99 | | | 0.99 | |
| Satd. Flow (prot) | 1789 | 1804 | | 1789 | 1868 | | | 1799 | | | 1701 | |
| Flt Permitted | 0.57 | 1.00 | | 0.55 | 1.00 | | | 0.88 | | | 0.88 | |
| Satd. Flow (perm) | 1066 | 1804 | | 1028 | 1868 | | | 1615 | | | 1522 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 41 | 325 | 36 | 21 | 303 | 18 | 21 | 36 | 17 | 15 | 22 | 18 |
| RTOR Reduction (vph) | 0 | 5 | 0 | 0 | 3 | 0 | 0 | 15 | 0 | 0 | 16 | 0 |
| Lane Group Flow (vph) | 41 | 356 | 0 | 21 | 318 | 0 | 0 | 59 | 0 | 0 | 39 | 0 |
| Heavy Vehicles (%) | 2% | 5% | 4% | 2% | 2% | 2% | 2% | 2% | 2% | 2% | 5% | 12% |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 33.8 | 33.8 | | 33.8 | 33.8 | | | 5.9 | | | 5.9 | |
| Effective Green, g (s) | 33.8 | 33.8 | | 33.8 | 33.8 | | | 5.9 | | | 5.9 | |
| Actuated g/C Ratio | 0.65 | 0.65 | | 0.65 | 0.65 | | | 0.11 | | | 0.11 | |
| Clearance Time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 696 | 1179 | | 672 | 1221 | | | 184 | | | 173 | |
| v/s Ratio Prot | | c0.20 | | | 0.17 | | | | | | | |
| v/s Ratio Perm | 0.04 | | | 0.02 | | | | c0.04 | | | 0.03 | |
| v/c Ratio | 0.06 | 0.30 | | 0.03 | 0.26 | | | 0.32 | | | 0.23 | |
| Uniform Delay, d1 | 3.2 | 3.9 | | 3.2 | 3.7 | | | 21.1 | | | 20.8 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.2 | 0.7 | | 0.1 | 0.5 | | | 1.0 | | | 0.7 | |
| Delay (s) | 3.4 | 4.5 | | 3.2 | 4.3 | | | 22.1 | | | 21.5 | |
| Level of Service | А | A | | А | A | | | C | | | C | |
| Approach Delay (s) | | 4.4 | | | 4.2 | | | 22.1 | | | 21.5 | |
| Approach LOS | | А | | | Α | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 6.9 | Н | CM 2000 | Level of | Service | | Α | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.30 | | | | | | | | | |
| Actuated Cycle Length (s) | ,, | | 51.7 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utiliza | tion | | 49.9% | IC | U Level (| of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|------------------------------|-------------|------|-------|------------|------------|-------------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ∱ 1> | | | † † | | 7 |
| Traffic Volume (veh/h) | 309 | 19 | 0 | 315 | 0 | 35 |
| Future Volume (Veh/h) | 309 | 19 | 0 | 315 | 0 | 35 |
| Sign Control | Free | | | Free | Stop | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 336 | 21 | 0 | 342 | 0 | 38 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | | | None | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | 134 | | | 53 | | |
| pX, platoon unblocked | | | | | 0.99 | |
| vC, conflicting volume | | | 357 | | 518 | 178 |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | | | 357 | | 491 | 178 |
| tC, single (s) | | | 4.2 | | 6.9 | 7.0 |
| tC, 2 stage (s) | | | | | | |
| tF (s) | | | 2.2 | | 3.5 | 3.3 |
| p0 queue free % | | | 100 | | 100 | 95 |
| cM capacity (veh/h) | | | 1177 | | 494 | 824 |
| Direction, Lane # | EB 1 | EB 2 | WB 1 | WB 2 | NB 1 | |
| Volume Total | 224 | 133 | 171 | 171 | 38 | |
| Volume Left | 0 | 0 | 0 | 0 | 0 | |
| Volume Right | 0 | 21 | 0 | 0 | 38 | |
| cSH | 1700 | 1700 | 1700 | 1700 | 824 | |
| Volume to Capacity | 0.13 | 0.08 | 0.10 | 0.10 | 0.05 | |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 | 0.0 | 1.1 | |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 9.6 | |
| Lane LOS | 0.0 | 0.0 | 0.0 | 0.0 | A | |
| Approach Delay (s) | 0.0 | | 0.0 | | 9.6 | |
| Approach LOS | 0.0 | | 0.0 | | A | |
| Intersection Summary | | | | | | |
| | | | 0.5 | | | |
| Average Delay | zotion | | | 10 | III ovel s | of Convios |
| Intersection Capacity Utiliz | Zati0[1 | | 19.1% | IC | U Level C | of Service |
| Analysis Period (min) | | | 15 | | | |

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|-------------------------------|------------|------------|-------|------|------------|------------|---------|----------|-------------|----------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ∱ Љ | | ۲ | ∱ Ъ | | | 4 | 7 | | 414 | |
| Traffic Volume (vph) | 74 | 214 | 72 | 50 | 200 | 61 | 56 | 194 | 34 | 57 | 207 | 57 |
| Future Volume (vph) | 74 | 214 | 72 | 50 | 200 | 61 | 56 | 194 | 34 | 57 | 207 | 57 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | | 1.00 | 1.00 | | 0.95 | |
| Frt | 1.00 | 0.96 | | 1.00 | 0.97 | | | 1.00 | 0.85 | | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.99 | 1.00 | | 0.99 | |
| Satd. Flow (prot) | 1738 | 3346 | | 1738 | 3355 | | | 1809 | 1555 | | 3354 | |
| Flt Permitted | 0.52 | 1.00 | | 0.56 | 1.00 | | | 0.82 | 1.00 | | 0.81 | |
| Satd. Flow (perm) | 948 | 3346 | | 1030 | 3355 | | | 1498 | 1555 | | 2750 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 80 | 233 | 78 | 54 | 217 | 66 | 61 | 211 | 37 | 62 | 225 | 62 |
| RTOR Reduction (vph) | 0 | 38 | 0 | 0 | 41 | 0 | 0 | 0 | 27 | 0 | 27 | 0 |
| Lane Group Flow (vph) | 80 | 273 | 0 | 54 | 242 | 0 | 0 | 272 | 10 | 0 | 322 | 0 |
| Turn Type | pm+pt | NA | | Perm | NA | | pm+pt | NA | Perm | Perm | NA | |
| Protected Phases | 5 | 2 | | | 6 | | 3 | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | 27.2 | 27.2 | | 17.2 | 17.2 | | | 14.2 | 14.2 | | 14.2 | |
| Effective Green, g (s) | 27.2 | 27.2 | | 17.2 | 17.2 | | | 14.2 | 14.2 | | 14.2 | |
| Actuated g/C Ratio | 0.51 | 0.51 | | 0.32 | 0.32 | | | 0.27 | 0.27 | | 0.27 | |
| Clearance Time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 601 | 1704 | | 331 | 1080 | | | 398 | 413 | | 731 | |
| v/s Ratio Prot | 0.02 | c0.08 | | | c0.07 | | | | | | | |
| v/s Ratio Perm | 0.05 | | | 0.05 | | | | c0.18 | 0.01 | | 0.12 | |
| v/c Ratio | 0.13 | 0.16 | | 0.16 | 0.22 | | | 0.68 | 0.02 | | 0.44 | |
| Uniform Delay, d1 | 6.8 | 7.0 | | 13.0 | 13.2 | | | 17.6 | 14.5 | | 16.3 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 0.5 | 0.2 | | 1.1 | 0.5 | | | 4.8 | 0.0 | | 0.4 | |
| Delay (s) | 7.2 | 7.2 | | 14.0 | 13.7 | | | 22.4 | 14.5 | | 16.7 | |
| Level of Service | А | Α | | В | В | | | С | В | | В | |
| Approach Delay (s) | | 7.2 | | | 13.8 | | | 21.4 | | | 16.7 | |
| Approach LOS | | Α | | | В | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 14.4 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.39 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 53.4 | | um of lost | | | | 16.0 | | | |
| Intersection Capacity Utiliza | ation | | 54.1% | IC | CU Level o | of Service | 9 | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-------------------------------|------------|-------|-------|-------|----------------|------------|---------|----------|-------------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | ሻ | f _r | | | 4 | 7 | | 4 | |
| Traffic Volume (vph) | 76 | 271 | 37 | 336 | 222 | 25 | 13 | 207 | 443 | 20 | 249 | 58 |
| Future Volume (vph) | 76 | 271 | 37 | 336 | 222 | 25 | 13 | 207 | 443 | 20 | 249 | 58 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Frt | | 0.99 | | 1.00 | 0.98 | | | 1.00 | 0.85 | | 0.98 | |
| Flt Protected | | 0.99 | | 0.95 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Satd. Flow (prot) | | 1788 | | 1738 | 1802 | | | 1824 | 1555 | | 1780 | |
| Flt Permitted | | 0.87 | | 0.44 | 1.00 | | | 0.97 | 1.00 | | 0.96 | |
| Satd. Flow (perm) | | 1573 | | 810 | 1802 | | | 1766 | 1555 | | 1723 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 83 | 295 | 40 | 365 | 241 | 27 | 14 | 225 | 482 | 22 | 271 | 63 |
| RTOR Reduction (vph) | 0 | 6 | 0 | 0 | 6 | 0 | 0 | 0 | 362 | 0 | 14 | 0 |
| Lane Group Flow (vph) | 0 | 412 | 0 | 365 | 262 | 0 | 0 | 239 | 120 | 0 | 342 | 0 |
| Turn Type | Perm | NA | | pm+pt | NA | | Perm | NA | Perm | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | | 22.0 | | 32.0 | 32.0 | | | 14.6 | 14.6 | | 14.6 | |
| Effective Green, g (s) | | 22.0 | | 32.0 | 32.0 | | | 14.6 | 14.6 | | 14.6 | |
| Actuated g/C Ratio | | 0.38 | | 0.55 | 0.55 | | | 0.25 | 0.25 | | 0.25 | |
| Clearance Time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | | 590 | | 569 | 984 | | | 439 | 387 | | 429 | |
| v/s Ratio Prot | | | | c0.09 | 0.15 | | | | | | | |
| v/s Ratio Perm | | c0.26 | | 0.26 | | | | 0.14 | 0.08 | | c0.20 | |
| v/c Ratio | | 0.70 | | 0.64 | 0.27 | | | 0.54 | 0.31 | | 0.80 | |
| Uniform Delay, d1 | | 15.5 | | 8.6 | 7.1 | | | 19.1 | 17.9 | | 20.6 | |
| Progression Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | | 6.7 | | 5.5 | 0.7 | | | 1.4 | 0.5 | | 10.0 | |
| Delay (s) | | 22.2 | | 14.1 | 7.7 | | | 20.5 | 18.4 | | 30.6 | |
| Level of Service | | С | | В | А | | | С | В | | С | |
| Approach Delay (s) | | 22.2 | | | 11.4 | | | 19.1 | | | 30.6 | |
| Approach LOS | | С | | | В | | | В | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 19.3 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.71 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 58.6 | | um of lost | | | | 14.0 | | | |
| Intersection Capacity Utiliza | ition | | 87.8% | IC | CU Level of | of Service | ! | | Е | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

| e: ewen eneet a e | - CC. | | | | | | | | | | | |
|--------------------------------|------------|-------|-------|------|------------|------------|---------|----------|------|------|------|------|
| | ۶ | - | • | • | ← | • | • | † | ~ | - | ţ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ¥ | f) | | Ť | f) | | | 4 | | | 4 | |
| Traffic Volume (vph) | 47 | 309 | 49 | 25 | 265 | 21 | 33 | 25 | 27 | 28 | 20 | 29 |
| Future Volume (vph) | 47 | 309 | 49 | 25 | 265 | 21 | 33 | 25 | 27 | 28 | 20 | 29 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frt | 1.00 | 0.98 | | 1.00 | 0.99 | | | 0.96 | | | 0.95 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.98 | | | 0.98 | |
| Satd. Flow (prot) | 1789 | 1795 | | 1789 | 1863 | | | 1769 | | | 1680 | |
| Flt Permitted | 0.57 | 1.00 | | 0.53 | 1.00 | | | 0.84 | | | 0.84 | |
| Satd. Flow (perm) | 1076 | 1795 | | 1002 | 1863 | | | 1506 | | | 1443 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 51 | 336 | 53 | 27 | 288 | 23 | 36 | 27 | 29 | 30 | 22 | 32 |
| RTOR Reduction (vph) | 0 | 7 | 0 | 0 | 4 | 0 | 0 | 26 | 0 | 0 | 28 | 0 |
| Lane Group Flow (vph) | 51 | 382 | 0 | 27 | 307 | 0 | 0 | 66 | 0 | 0 | 56 | 0 |
| Heavy Vehicles (%) | 2% | 5% | 4% | 2% | 2% | 2% | 2% | 2% | 2% | 2% | 5% | 12% |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 33.1 | 33.1 | | 33.1 | 33.1 | | | 6.0 | | | 6.0 | |
| Effective Green, g (s) | 33.1 | 33.1 | | 33.1 | 33.1 | | | 6.0 | | | 6.0 | |
| Actuated g/C Ratio | 0.65 | 0.65 | | 0.65 | 0.65 | | | 0.12 | | | 0.12 | |
| Clearance Time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 696 | 1162 | | 649 | 1206 | | | 176 | | | 169 | |
| v/s Ratio Prot | | c0.21 | | | 0.17 | | | | | | | |
| v/s Ratio Perm | 0.05 | | | 0.03 | | | | c0.04 | | | 0.04 | |
| v/c Ratio | 0.07 | 0.33 | | 0.04 | 0.25 | | | 0.38 | | | 0.33 | |
| Uniform Delay, d1 | 3.3 | 4.0 | | 3.3 | 3.8 | | | 20.8 | | | 20.7 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.2 | 0.8 | | 0.1 | 0.5 | | | 1.4 | | | 1.1 | |
| Delay (s) | 3.5 | 4.8 | | 3.4 | 4.3 | | | 22.2 | | | 21.9 | |
| Level of Service | Α | Α | | Α | А | | | С | | | С | |
| Approach Delay (s) | | 4.6 | | | 4.2 | | | 22.2 | | | 21.9 | |
| Approach LOS | | Α | | | Α | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 7.7 | Н | CM 2000 | Level of S | Service | | Α | | | |
| HCM 2000 Volume to Capac | city ratio | | 0.34 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 51.1 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utilizat | tion | | 57.4% | IC | U Level of | of Service | ! | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-------------------------------|-------------|------|-------|------------|------------|-----------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † 1> | | | † † | | 7 |
| Traffic Volume (veh/h) | 332 | 33 | 0 | 312 | 0 | 28 |
| Future Volume (Veh/h) | 332 | 33 | 0 | 312 | 0 | 28 |
| Sign Control | Free | | | Free | Stop | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 361 | 36 | 0 | 339 | 0 | 30 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | | | None | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | 134 | | | 53 | | |
| pX, platoon unblocked | | | | | 0.97 | |
| vC, conflicting volume | | | 397 | | 548 | 198 |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | | | 397 | | 482 | 198 |
| tC, single (s) | | | 4.2 | | 6.9 | 7.0 |
| tC, 2 stage (s) | | | | | | |
| tF (s) | | | 2.2 | | 3.5 | 3.3 |
| p0 queue free % | | | 100 | | 100 | 96 |
| cM capacity (veh/h) | | | 1137 | | 492 | 800 |
| Direction, Lane # | EB 1 | EB 2 | WB 1 | WB 2 | NB 1 | |
| Volume Total | 241 | 156 | 170 | 170 | 30 | |
| Volume Left | 0 | 0 | 0 | 0 | 0 | |
| Volume Right | 0 | 36 | 0 | 0 | 30 | |
| cSH | 1700 | 1700 | 1700 | 1700 | 800 | |
| Volume to Capacity | 0.14 | 0.09 | 0.10 | 0.10 | 0.04 | |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.9 | |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 9.7 | |
| Lane LOS | 0.0 | 0.0 | 0.0 | 0.0 | Α | |
| Approach Delay (s) | 0.0 | | 0.0 | | 9.7 | |
| Approach LOS | 0.0 | | 0.0 | | A | |
| Intersection Summary | | | | | | |
| | | | 0.4 | | | |
| Average Delay | ation | | 20.2% | IC | III ovol s | f Service |
| Intersection Capacity Utiliza | auull | | | IC | o revei (| i Service |
| Analysis Period (min) | | | 15 | | | |

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|---------------------------------|-----------|------------|-------|------|------------|----------|---------|-------|-------------|-------------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ř | ↑ ↑ | | ř | ∱ ∱ | | | 4 | 7 | | 4Th | |
| Traffic Volume (vph) | 83 | 209 | 85 | 34 | 192 | 85 | 94 | 218 | 39 | 49 | 153 | 61 |
| Future Volume (vph) | 83 | 209 | 85 | 34 | 192 | 85 | 94 | 218 | 39 | 49 | 153 | 61 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | | 1.00 | 1.00 | | 0.95 | |
| Frt | 1.00 | 0.96 | | 1.00 | 0.95 | | | 1.00 | 0.85 | | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.99 | 1.00 | | 0.99 | |
| Satd. Flow (prot) | 1738 | 3326 | | 1738 | 3317 | | | 1803 | 1555 | | 3325 | |
| Flt Permitted | 0.51 | 1.00 | | 0.56 | 1.00 | | | 0.79 | 1.00 | | 0.81 | |
| Satd. Flow (perm) | 931 | 3326 | | 1022 | 3317 | | | 1446 | 1555 | | 2733 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 90 | 227 | 92 | 37 | 209 | 92 | 102 | 237 | 42 | 53 | 166 | 66 |
| RTOR Reduction (vph) | 0 | 48 | 0 | 0 | 65 | 0 | 0 | 0 | 29 | 0 | 40 | 0 |
| Lane Group Flow (vph) | 90 | 271 | 0 | 37 | 236 | 0 | 0 | 339 | 13 | 0 | 245 | 0 |
| Turn Type | pm+pt | NA | | Perm | NA | | pm+pt | NA | Perm | Perm | NA | |
| Protected Phases | 5 | 2 | | | 6 | | 3 | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | 27.2 | 27.2 | | 17.1 | 17.1 | | | 18.2 | 18.2 | | 18.2 | |
| Effective Green, g (s) | 27.2 | 27.2 | | 17.1 | 17.1 | | | 18.2 | 18.2 | | 18.2 | |
| Actuated g/C Ratio | 0.47 | 0.47 | | 0.30 | 0.30 | | | 0.32 | 0.32 | | 0.32 | |
| Clearance Time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 555 | 1576 | | 304 | 988 | | | 458 | 493 | | 866 | |
| v/s Ratio Prot | 0.02 | c0.08 | | | c0.07 | | | | | | | |
| v/s Ratio Perm | 0.05 | | | 0.04 | | | | c0.23 | 0.01 | | 0.09 | |
| v/c Ratio | 0.16 | 0.17 | | 0.12 | 0.24 | | | 0.74 | 0.03 | | 0.28 | |
| Uniform Delay, d1 | 8.4 | 8.6 | | 14.7 | 15.2 | | | 17.5 | 13.5 | | 14.7 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 0.6 | 0.2 | | 0.8 | 0.6 | | | 6.3 | 0.0 | | 0.2 | |
| Delay (s) | 9.0 | 8.9 | | 15.5 | 15.8 | | | 23.8 | 13.5 | | 14.9 | |
| Level of Service | А | Α | | В | В | | | С | В | | В | |
| Approach Delay (s) | | 8.9 | | | 15.8 | | | 22.7 | | | 14.9 | |
| Approach LOS | | А | | | В | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 15.5 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capac | ity ratio | | 0.46 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 57.4 | S | um of lost | time (s) | | | 16.0 | | | |
| Intersection Capacity Utilizati | ion | | 56.1% | | CU Level o | | 9 | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-----------------------------------|---------|----------|-------|-------|------------|------------|---------|------|-------------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | ሻ | f) | | | 4 | 7 | | 4 | |
| Traffic Volume (vph) | 69 | 171 | 23 | 404 | 230 | 22 | 11 | 240 | 343 | 19 | 208 | 41 |
| Future Volume (vph) | 69 | 171 | 23 | 404 | 230 | 22 | 11 | 240 | 343 | 19 | 208 | 41 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Frt | | 0.99 | | 1.00 | 0.99 | | | 1.00 | 0.85 | | 0.98 | |
| Flt Protected | | 0.99 | | 0.95 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Satd. Flow (prot) | | 1785 | | 1738 | 1806 | | | 1826 | 1555 | | 1785 | |
| Flt Permitted | | 0.83 | | 0.54 | 1.00 | | | 0.98 | 1.00 | | 0.95 | |
| Satd. Flow (perm) | | 1506 | | 985 | 1806 | | | 1791 | 1555 | | 1711 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 75 | 186 | 25 | 439 | 250 | 24 | 12 | 261 | 373 | 21 | 226 | 45 |
| RTOR Reduction (vph) | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 287 | 0 | 12 | 0 |
| Lane Group Flow (vph) | 0 | 281 | 0 | 439 | 269 | 0 | 0 | 273 | 86 | 0 | 280 | 0 |
| Turn Type | Perm | NA | | pm+pt | NA | | Perm | NA | Perm | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | | 19.1 | | 32.1 | 32.1 | | | 13.3 | 13.3 | | 13.3 | |
| Effective Green, g (s) | | 19.1 | | 32.1 | 32.1 | | | 13.3 | 13.3 | | 13.3 | |
| Actuated g/C Ratio | | 0.33 | | 0.56 | 0.56 | | | 0.23 | 0.23 | | 0.23 | |
| Clearance Time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | | 501 | | 695 | 1009 | | | 414 | 360 | | 396 | |
| v/s Ratio Prot | | | | c0.12 | 0.15 | | | | | | | |
| v/s Ratio Perm | | c0.19 | | 0.23 | | | | 0.15 | 0.06 | | c0.16 | |
| v/c Ratio | | 0.56 | | 0.63 | 0.27 | | | 0.66 | 0.24 | | 0.71 | |
| Uniform Delay, d1 | | 15.7 | | 8.0 | 6.6 | | | 20.0 | 17.9 | | 20.3 | |
| Progression Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | | 4.5 | | 4.3 | 0.6 | | | 3.8 | 0.3 | | 5.7 | |
| Delay (s) | | 20.2 | | 12.3 | 7.2 | | | 23.8 | 18.3 | | 26.0 | |
| Level of Service | | С | | В | Α | | | С | В | | С | |
| Approach Delay (s) | | 20.2 | | | 10.3 | | | 20.6 | | | 26.0 | |
| Approach LOS | | С | | | В | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 17.6 | H | CM 2000 | Level of S | Service | | В | | | |
| HCM 2000 Volume to Capacity | y ratio | | 0.62 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 57.4 | S | um of lost | time (s) | | | 14.0 | | | |
| Intersection Capacity Utilization | n | | 81.0% | | U Level o | | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|---------------------------------|-----------|----------------|-------|------|------------|------------|---------|-------|-------------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ħ | (Î | | ¥ | 1> | | | 4 | | | 4 | |
| Traffic Volume (vph) | 40 | 329 | 35 | 19 | 307 | 18 | 20 | 35 | 16 | 14 | 21 | 18 |
| Future Volume (vph) | 40 | 329 | 35 | 19 | 307 | 18 | 20 | 35 | 16 | 14 | 21 | 18 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frt | 1.00 | 0.99 | | 1.00 | 0.99 | | | 0.97 | | | 0.95 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.99 | | | 0.99 | |
| Satd. Flow (prot) | 1789 | 1805 | | 1789 | 1867 | | | 1802 | | | 1696 | |
| Flt Permitted | 0.55 | 1.00 | | 0.53 | 1.00 | | | 0.88 | | | 0.89 | |
| Satd. Flow (perm) | 1034 | 1805 | | 995 | 1867 | | | 1614 | | | 1523 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 43 | 358 | 38 | 21 | 334 | 20 | 22 | 38 | 17 | 15 | 23 | 20 |
| RTOR Reduction (vph) | 0 | 5 | 0 | 0 | 3 | 0 | 0 | 15 | 0 | 0 | 18 | 0 |
| Lane Group Flow (vph) | 43 | 391 | 0 | 21 | 351 | 0 | 0 | 62 | 0 | 0 | 40 | 0 |
| Heavy Vehicles (%) | 2% | 5% | 4% | 2% | 2% | 2% | 2% | 2% | 2% | 2% | 5% | 12% |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 33.6 | 33.6 | | 33.6 | 33.6 | | | 5.9 | | | 5.9 | |
| Effective Green, g (s) | 33.6 | 33.6 | | 33.6 | 33.6 | | | 5.9 | | | 5.9 | |
| Actuated g/C Ratio | 0.65 | 0.65 | | 0.65 | 0.65 | | | 0.11 | | | 0.11 | |
| Clearance Time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 674 | 1177 | | 649 | 1218 | | | 184 | | | 174 | |
| v/s Ratio Prot | | c0.22 | | | 0.19 | | | | | | | |
| v/s Ratio Perm | 0.04 | | | 0.02 | | | | c0.04 | | | 0.03 | |
| v/c Ratio | 0.06 | 0.33 | | 0.03 | 0.29 | | | 0.34 | | | 0.23 | |
| Uniform Delay, d1 | 3.2 | 4.0 | | 3.2 | 3.8 | | | 21.0 | | | 20.7 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.2 | 0.8 | | 0.1 | 0.6 | | | 1.1 | | | 0.7 | |
| Delay (s) | 3.4 | 4.7 | | 3.3 | 4.4 | | | 22.1 | | | 21.4 | |
| Level of Service | Α | A | | A | A | | | C | | | C | |
| Approach Delay (s) | | 4.6 | | | 4.4 | | | 22.1 | | | 21.4 | |
| Approach LOS | | Α | | | А | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 7.0 | H | CM 2000 | Level of S | Service | | Α | | | |
| HCM 2000 Volume to Capac | ity ratio | | 0.33 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 51.5 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utilizati | ion | | 51.6% | IC | U Level o | of Service | | | Α | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| | - | • | • | ← | • | / |
|-------------------------------|-------------|------|-------|------------|-----------|-----------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ∱ 1> | | | † † | | 7 |
| Traffic Volume (veh/h) | 341 | 19 | 0 | 347 | 0 | 35 |
| Future Volume (Veh/h) | 341 | 19 | 0 | 347 | 0 | 35 |
| Sign Control | Free | | | Free | Stop | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 371 | 21 | 0 | 377 | 0 | 38 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | | | None | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | 134 | | | 53 | | |
| pX, platoon unblocked | | | | | 0.98 | |
| vC, conflicting volume | | | 392 | | 570 | 196 |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | | | 392 | | 516 | 196 |
| tC, single (s) | | | 4.2 | | 6.9 | 7.0 |
| tC, 2 stage (s) | | | | | | |
| tF (s) | | | 2.2 | | 3.5 | 3.3 |
| p0 queue free % | | | 100 | | 100 | 95 |
| cM capacity (veh/h) | | | 1142 | | 471 | 803 |
| Direction, Lane # | EB 1 | EB 2 | WB 1 | WB 2 | NB 1 | |
| Volume Total | 247 | 145 | 188 | 188 | 38 | |
| Volume Left | 0 | 0 | 0 | 0 | 0 | |
| Volume Right | 0 | 21 | 0 | 0 | 38 | |
| cSH | 1700 | 1700 | 1700 | 1700 | 803 | |
| Volume to Capacity | 0.15 | 0.09 | 0.11 | 0.11 | 0.05 | |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 | 0.0 | 1.1 | |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 9.7 | |
| Lane LOS | | | | | Α | |
| Approach Delay (s) | 0.0 | | 0.0 | | 9.7 | |
| Approach LOS | | | | | Α | |
| Intersection Summary | | | | | | |
| Average Delay | | | 0.5 | | | |
| Intersection Capacity Utiliza | ation | | 20.0% | IC | U Level c | f Service |
| Analysis Period (min) | | | 15 | | | |

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|-------------------------------|-------------|------------|-------|------|-------------|------------|---------|----------|------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ↑ ↑ | | ሻ | ∱ 1> | | | 4 | 7 | | 414 | |
| Traffic Volume (vph) | 80 | 236 | 79 | 55 | 220 | 67 | 61 | 214 | 38 | 63 | 229 | 62 |
| Future Volume (vph) | 80 | 236 | 79 | 55 | 220 | 67 | 61 | 214 | 38 | 63 | 229 | 62 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | | 1.00 | 1.00 | | 0.95 | |
| Frt | 1.00 | 0.96 | | 1.00 | 0.96 | | | 1.00 | 0.85 | | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.99 | 1.00 | | 0.99 | |
| Satd. Flow (prot) | 1738 | 3346 | | 1738 | 3354 | | | 1810 | 1555 | | 3356 | |
| Flt Permitted | 0.50 | 1.00 | | 0.55 | 1.00 | | | 0.81 | 1.00 | | 0.79 | |
| Satd. Flow (perm) | 921 | 3346 | | 998 | 3354 | | | 1487 | 1555 | | 2670 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 87 | 257 | 86 | 60 | 239 | 73 | 66 | 233 | 41 | 68 | 249 | 67 |
| RTOR Reduction (vph) | 0 | 43 | 0 | 0 | 41 | 0 | 0 | 0 | 29 | 0 | 26 | 0 |
| Lane Group Flow (vph) | 87 | 300 | 0 | 60 | 271 | 0 | 0 | 299 | 12 | 0 | 358 | 0 |
| Turn Type | pm+pt | NA | | Perm | NA | | pm+pt | NA | Perm | Perm | NA | |
| Protected Phases | 5 | 2 | | | 6 | | 3 | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | 27.2 | 27.2 | | 17.1 | 17.1 | | | 15.5 | 15.5 | | 15.5 | |
| Effective Green, g (s) | 27.2 | 27.2 | | 17.1 | 17.1 | | | 15.5 | 15.5 | | 15.5 | |
| Actuated g/C Ratio | 0.50 | 0.50 | | 0.31 | 0.31 | | | 0.28 | 0.28 | | 0.28 | |
| Clearance Time (s) | 2.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 578 | 1663 | | 311 | 1048 | | | 421 | 440 | | 756 | |
| v/s Ratio Prot | 0.02 | c0.09 | | | c0.08 | | | | | | | |
| v/s Ratio Perm | 0.05 | | | 0.06 | | | | c0.20 | 0.01 | | 0.13 | |
| v/c Ratio | 0.15 | 0.18 | | 0.19 | 0.26 | | | 0.71 | 0.03 | | 0.47 | |
| Uniform Delay, d1 | 7.3 | 7.6 | | 13.8 | 14.1 | | | 17.6 | 14.2 | | 16.2 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 0.6 | 0.2 | | 1.4 | 0.6 | | | 5.6 | 0.0 | | 0.5 | |
| Delay (s) | 7.9 | 7.8 | | 15.1 | 14.7 | | | 23.2 | 14.2 | | 16.7 | |
| Level of Service | А | Α | | В | В | | | С | В | | В | |
| Approach Delay (s) | | 7.8 | | | 14.7 | | | 22.1 | | | 16.7 | |
| Approach LOS | | Α | | | В | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 14.9 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capa | acity ratio | | 0.43 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 54.7 | S | um of lost | time (s) | | | 16.0 | | | |
| Intersection Capacity Utiliza | ation | | 57.2% | IC | CU Level | of Service | 9 | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-------------------------------|------------|----------|-------|-------|----------------|------------|---------|------|-------------|----------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | ň | (Î | | | 4 | 7 | | 4 | |
| Traffic Volume (vph) | 84 | 328 | 41 | 369 | 267 | 28 | 14 | 228 | 487 | 21 | 274 | 64 |
| Future Volume (vph) | 84 | 328 | 41 | 369 | 267 | 28 | 14 | 228 | 487 | 21 | 274 | 64 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Lane Util. Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Frt | | 0.99 | | 1.00 | 0.99 | | | 1.00 | 0.85 | | 0.98 | |
| Flt Protected | | 0.99 | | 0.95 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Satd. Flow (prot) | | 1791 | | 1738 | 1804 | | | 1824 | 1555 | | 1780 | |
| Flt Permitted | | 0.86 | | 0.39 | 1.00 | | | 0.96 | 1.00 | | 0.97 | |
| Satd. Flow (perm) | | 1560 | | 712 | 1804 | | | 1757 | 1555 | | 1723 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 91 | 357 | 45 | 401 | 290 | 30 | 15 | 248 | 529 | 23 | 298 | 70 |
| RTOR Reduction (vph) | 0 | 6 | 0 | 0 | 6 | 0 | 0 | 0 | 384 | 0 | 13 | 0 |
| Lane Group Flow (vph) | 0 | 487 | 0 | 401 | 314 | 0 | 0 | 263 | 145 | 0 | 378 | 0 |
| Turn Type | Perm | NA | | pm+pt | NA | | Perm | NA | Perm | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | | 22.0 | | 32.0 | 32.0 | | | 15.2 | 15.2 | | 15.2 | |
| Effective Green, g (s) | | 22.0 | | 32.0 | 32.0 | | | 15.2 | 15.2 | | 15.2 | |
| Actuated g/C Ratio | | 0.37 | | 0.54 | 0.54 | | | 0.26 | 0.26 | | 0.26 | |
| Clearance Time (s) | | 6.0 | | 2.0 | 6.0 | | | 6.0 | 6.0 | | 6.0 | |
| Vehicle Extension (s) | | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | | 579 | | 523 | 975 | | | 451 | 399 | | 442 | |
| v/s Ratio Prot | | | | c0.10 | 0.17 | | | | | | | |
| v/s Ratio Perm | | c0.31 | | 0.31 | | | | 0.15 | 0.09 | | c0.22 | |
| v/c Ratio | | 0.84 | | 0.77 | 0.32 | | | 0.58 | 0.36 | | 0.85 | |
| Uniform Delay, d1 | | 17.0 | | 9.7 | 7.6 | | | 19.2 | 18.0 | | 20.9 | |
| Progression Factor | | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | | 13.8 | | 10.3 | 0.9 | | | 1.9 | 0.6 | | 14.8 | |
| Delay (s) | | 30.8 | | 20.0 | 8.4 | | | 21.2 | 18.6 | | 35.8 | |
| Level of Service | | С | | С | Α | | | С | В | | D | |
| Approach Delay (s) | | 30.8 | | | 14.9 | | | 19.4 | | | 35.8 | |
| Approach LOS | | С | | | В | | | В | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 23.1 | Н | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.82 | | | | | | | | | |
| Actuated Cycle Length (s) | • | | 59.2 | S | um of lost | time (s) | | | 14.0 | | | |
| Intersection Capacity Utiliza | ition | | 95.8% | | CU Level o | | | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Analysis Period (min) c Critical Lane Group

| <u>e. ewen eneer a c</u> | 7011101 0 | | | | | | | | | | | |
|-------------------------------|------------|-------|-------|------|----------------|------------|---------|----------|------|------|------|------|
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| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ۲ | 4 | | ۲ | (Î | | | 4 | | | 4 | |
| Traffic Volume (vph) | 49 | 338 | 51 | 26 | 293 | 22 | 35 | 27 | 28 | 29 | 21 | 30 |
| Future Volume (vph) | 49 | 338 | 51 | 26 | 293 | 22 | 35 | 27 | 28 | 29 | 21 | 30 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frt | 1.00 | 0.98 | | 1.00 | 0.99 | | | 0.96 | | | 0.95 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.98 | | | 0.98 | |
| Satd. Flow (prot) | 1789 | 1796 | | 1789 | 1864 | | | 1770 | | | 1681 | |
| Flt Permitted | 0.56 | 1.00 | | 0.52 | 1.00 | | | 0.83 | | | 0.84 | |
| Satd. Flow (perm) | 1046 | 1796 | | 972 | 1864 | | | 1504 | | | 1438 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 53 | 367 | 55 | 28 | 318 | 24 | 38 | 29 | 30 | 32 | 23 | 33 |
| RTOR Reduction (vph) | 0 | 7 | 0 | 0 | 4 | 0 | 0 | 26 | 0 | 0 | 29 | 0 |
| Lane Group Flow (vph) | 53 | 415 | 0 | 28 | 338 | 0 | 0 | 71 | 0 | 0 | 59 | 0 |
| Heavy Vehicles (%) | 2% | 5% | 4% | 2% | 2% | 2% | 2% | 2% | 2% | 2% | 5% | 12% |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 32.9 | 32.9 | | 32.9 | 32.9 | | | 6.0 | | | 6.0 | |
| Effective Green, g (s) | 32.9 | 32.9 | | 32.9 | 32.9 | | | 6.0 | | | 6.0 | |
| Actuated g/C Ratio | 0.65 | 0.65 | | 0.65 | 0.65 | | | 0.12 | | | 0.12 | |
| Clearance Time (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | | 6.0 | | | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 676 | 1160 | | 628 | 1204 | | | 177 | | | 169 | |
| v/s Ratio Prot | | c0.23 | | | 0.18 | | | | | | | |
| v/s Ratio Perm | 0.05 | | | 0.03 | | | | c0.05 | | | 0.04 | |
| v/c Ratio | 0.08 | 0.36 | | 0.04 | 0.28 | | | 0.40 | | | 0.35 | |
| Uniform Delay, d1 | 3.4 | 4.1 | | 3.3 | 3.9 | | | 20.8 | | | 20.7 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.2 | 0.9 | | 0.1 | 0.6 | | | 1.5 | | | 1.2 | |
| Delay (s) | 3.6 | 5.0 | | 3.4 | 4.5 | | | 22.3 | | | 21.9 | |
| Level of Service | А | Α | | А | Α | | | С | | | С | |
| Approach Delay (s) | | 4.8 | | | 4.4 | | | 22.3 | | | 21.9 | |
| Approach LOS | | Α | | | A | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 7.8 | Н | CM 2000 | Level of | Service | | Α | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.36 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 50.9 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utiliza | tion | | 59.1% | IC | CU Level of | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-------------------------------|----------|------|-------|----------|-----------|-------------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † | | | <u>↑</u> | | 7 |
| Traffic Volume (veh/h) | 367 | 33 | 0 | 344 | 0 | 28 |
| Future Volume (Veh/h) | 367 | 33 | 0 | 344 | 0 | 28 |
| Sign Control | Free | | | Free | Stop | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 399 | 36 | 0 | 374 | 0 | 30 |
| Pedestrians | 0,, | 00 | | 071 | | 00 |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | | | None | | |
| Median storage veh) | None | | | NOTIC | | |
| Upstream signal (m) | 134 | | | 53 | | |
| pX, platoon unblocked | 137 | | | 33 | 0.96 | |
| vC, conflicting volume | | | 435 | | 604 | 218 |
| vC1, stage 1 conf vol | | | 433 | | 004 | 210 |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | | | 435 | | 513 | 218 |
| tC, single (s) | | | 4.2 | | 6.9 | 7.0 |
| tC, 2 stage (s) | | | 7.2 | | 0.7 | 7.0 |
| tF (s) | | | 2.2 | | 3.5 | 3.3 |
| p0 queue free % | | | 100 | | 100 | 96 |
| cM capacity (veh/h) | | | 1100 | | 466 | 778 |
| | | | | | | 770 |
| Direction, Lane # | EB 1 | EB 2 | WB 1 | WB 2 | NB 1 | |
| Volume Total | 266 | 169 | 187 | 187 | 30 | |
| Volume Left | 0 | 0 | 0 | 0 | 0 | |
| Volume Right | 0 | 36 | 0 | 0 | 30 | |
| cSH | 1700 | 1700 | 1700 | 1700 | 778 | |
| Volume to Capacity | 0.16 | 0.10 | 0.11 | 0.11 | 0.04 | |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.9 | |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 9.8 | |
| Lane LOS | | | | | Α | |
| Approach Delay (s) | 0.0 | | 0.0 | | 9.8 | |
| Approach LOS | | | | | Α | |
| Intersection Summary | | | | | | |
| Average Delay | | | 0.4 | | | |
| Intersection Capacity Utiliza | ation | | 21.2% | IC | U Level o | f Service |
| Analysis Period (min) | | | 15 | | | |

Appendix G: Construction Staging Plan

Legend



