

REVISED Hydrogeological Assessment 181 Burton Avenue Barrie, Ontario

Prepared for: Monolite Holdings Inc.

Prepared by: Azimuth Environmental Consulting, Inc.

August 2023

AEC 21-492



Environmental Assessments & Approvals

August 1st, 2023 AEC 21-492

Monolite Holdings Inc. 343 Sugar Maple Lane, Richmond Hill, ON L4C 4C3

Attn: Maria Rozentsvayg

Re: **REVISED** Hydrogeological Assessment

181 Burton Avenue, Barrie ON

Dear Maria:

Azimuth Environmental Consulting, Inc. (Azimuth) is pleased to provide our Revised Hydrogeological Assessment for the property located at 181 Burton Avenue within the City of Barrie, ON (the "Site"). This evaluation focused on the existing soil and ground water regime underlying the Site and the potential for the proposed development to impact the existing conditions. The report revisions include updating the dewatering assessment and inclusion of a water balance assessment.

Should you have any questions or wish to discuss the report in greater detail, please do not hesitate to contact the undersigned.

Yours truly,

AZIMUTH ENVIRONMENTAL CONSULTING, INC.

Colin Ross, B.Sc., P.Geo. Senior Hydrogeologist

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1.0 INTRODUCTION

Azimuth Environmental Consulting Inc. (Azimuth) has been retained by Monolite Holdings Inc. to conduct a Hydrogeological Assessment for the property located at 181 Burton Avenue within the City of Barrie, Ontario (the "Site")(Figure 1). The Site is approximately 1,995 square meters (m²) in size and is bound by Burton Avenue to the north, commercial properties to the east and west and vacant land to the north (Figure 2).

The proposed development is comprised of a four storey residential building (Appendix B). Access to the Site is from Burton Avenue, while all parking for the Site will be at grade north of the building.

The purpose of this assessment is to characterize the hydrogeological conditions at the Site and the potential for the proposed development to cause impact.

2.0 ENVIRONMENTAL SETTING

2.1 Soil

The soils at the Site are classified as Sargent Series gravelly sandy loam (Hoffman *et al*, 1962). This material has good drainage and is classified within hydrologic soil group "AB". Group A soils have low runoff potential and high infiltration rates even when thoroughly wet, and consist of deep, well to excessively drained sand or gravel. Group B soils have moderate infiltration rates when thoroughly wet and consist of moderately fine to moderately coarse textures.

2.2 Physiography

According to Chapman and Putnam (1984) the Site falls within the Simcoe Lowlands physiographic region. It lies on one of the numerous glacial shorelines that define the Lake Simcoe basin. These lowlands are considered to be the former Lake Algonquin shoreline features. The lowland soils are described as being composed of sands, silt and clay.

2.3 Topography and Drainage

The topographic relief at the Site is quite limited with elevations ranging between approximately 229 masl at the south and 232 masl at the north along Burton Avenue. The current Site drainage is expected to follow the local topographic dip to the north, although any surface runoff exiting the Site is expected to be captured within the local municipal stormwater system along Cumberland Street to the north. Run on to the Site is not expected from the south due to the presence of curb and gutters along Burton Avenue. The only surface water feature that is present in proximity to the Site is a small wetland



area immediately north of the Site (Figure 2) as identified in the Cambium, 2022 Environmental Impact Study (EIS). This feature is described as a small wetland pocket that is not connected to any mapped watercourses.

2.4 Bedrock Geology

The underlying bedrock geology has been described by the Ontario Geologic Survey (OGS) as being composed of interbedded bioclastic to very-fine grained limestone and grey-green calcareous shale of the Verulam Formation of the Simcoe Group (OGS, 2022). The Simcoe Group is Middle Ordovician in age. The entire overburden profile beneath the Site is estimated to be over 100 m in depth before encountering the bedrock contact based on local MECP well records for the area.

2.5 Quaternary Geology

According to Barnett *et al.* (1991), the surficial material at the Site consists of glaciofluvial ice-contact stratified deposits consisting of gravel and sand. The stratigraphy is dominated by sands and gravels inter-bedded with silts and clays. As a result, the overburden is characterized by a complex of layered, coarse-grained sediments with interbedded with fine-grained sediments that are not regionally extensive.

The Site soils as defined in the Site Geotechnical Assessment (WSP, 2021) and Phase II ESA (Envision, 2022) were that approximately 2 to 3 m of silty sand fill are present at the Site overlying native sand to silty sand. The native soils are consistent with what is reported in the OGS mapping. For reference, the borehole logs from the Geotechnical Assessment and Phase II ESA have been provided in Appendix D.

2.6 Well Records

The Ontario Ministry of Environment, Conservation, and Parks (MECP) Water Well Records were referenced for any recorded well information within the vicinity of the Site (300 m) (MECP, 2022). The area has been historically municipally serviced; however well records can be used to gain subsurface information which can provide insight into shallow geological formation within the area. The well records found in the vicinity of the Site that are pertinent to this assessment are summarized in Table 1 and are shown on Figure 3.



Table 1: MECP Water Well Database Summary (300 m radius from Site)

				Borehole	Ground
MECP Well				Depth	Elevation
Record No.	Drill Date	Status	Well Type	(mbgs)	(masl)
5700255	11-Oct-60	Unknown	Municipal Water Supply	86.6	227.4
5700265	22-Nov-62	Unknown	Municipal Water Supply	91.7	219.9
5709345	21-Nov-72	Unknown	Municipal Water Supply	87.2	227.0
5711799	28-Oct-74	Decommissioned	Municipal Water Supply	71.6	227.2
7264481 /					
A162243	25-Apr-16	Active	Observation Well	10.7	238.0
7278306 /					
A208627	22-Dec-16	Active	Observation Well	1.9	237.0
7278307 /					
A208628	22-Dec-16	Active	Observation Well	1.9	237.0
7045815 /					
A058556	26-Jun-07	Abandoned	Unknown	4.1	232.4
7045817 /					
A058557	26-Jun-07	Abandoned	Unknown	19.7	232.1
7337101	15-Jun-18	Unknown	Unknown	-	232.3
7310630	15-Mar-18	Unknown	Unknown	-	233.0

The surrounding wells in the MECP well record database were drilled for monitoring and municipal water supply. The wells were drilled to depths between 1.9 and 91.7 m. Not all actual well records were available online, but those that were available for download have been included in Appendix C. The soils identified in these records were primarily sand, which matches the geological literature outlined above, as well as the Site specific soils identified at the Site through the Site geotechnical drilling program.

3.0 SOURCE WATER PROTECTION

A review of the Source Water Protection Areas as identified on the MECP Source Protection Information Atlas website indicates the Site is partially located within a Wellhead Protection Area (WHPA-C). The Site is also located within a Significant Ground Water Recharge Area (SGRA), a Highly Vulnerable Aquifer Area (HVA), a Wellhead Protection Area (WHPA Q1/2) for quantity threat and an Issues Contributing Area (ICA) for sodium and chloride and is also considered an Intake Protection Zone (IPZ) 3.

4.0 MONITORING

4.1 Ground Water Level Monitoring

Two ground water monitoring wells were installed as part of the 2021 WSP geotechnical assessment with depths of 4.6 to 5.0 mbgs, while two additional monitoring wells were installed by Envision in April 2022 to depths of 6.1 mbgs as part of their Phase II ESA. For reference, borehole logs have been included in Appendix D. Water levels were measured as part of the geotechnical assessment in February 2021 and monthly by



Azimuth between March and June 2022 to establish seasonally high water table conditions, along with additional measurements in July 2023. The ground water levels at the Site have shown variation over time with the most elevated conditions observed in April, 2022 and the lowest in February, 2021. The high ground water condition is shown on Figure 4. Ground water flow direction is interpreted to be to the northeast, following a local topographic decline towards Lake Simcoe. The ground water level and elevation details have been included in Appendix D.

4.2 Hydraulic Conductivity Testing

In order to understand the hydraulic characteristics of the underlying overburden, a transient slug test can be performed within monitoring wells to determine the average hydraulic conductivity of the screened interval. A slug test involves the instantaneous injection or withdrawal of a volume or slug of water or solid cylinder of known volume. This is accomplished by adding or displacing a known volume to/from a well and measuring water level response time to return to equilibrium.

Hydraulic conductivity testing was completed at the Site by Azimuth staff within BH21-1 and BH21-4 on March 16th and April 14th, 2022. Water level measurements were recorded both manually and with a datalogger, which were programmed to record the pressure of water above the data logger every five seconds. Data was analyzed using the Hvorslev Method (1951) for unconfined aquifers, which assumes a homogeneous, isotropic medium in which soil and water are incompressible. Hydraulic testing results are summarized in Table 2, and within Appendix E.

Table 2: Hydraulic Testing Results

Monitoring Well	Screen Depth (mbgs)	Hydraulic Conductivity (m/s)	Soil Description	
BH21-1	3.1 - 4.6	2.3×10^{-6}	Sand	
BH21-4	3.5 - 5.0	1.5 x 10 ⁻⁶	Silty Sand	

Slug test data indicates that the hydraulic conductivity of the deposits is between 1.5×10^{-6} and 2.3×10^{-6} m/s. The measured hydraulic conductivity is within the published range for a sandy material (Freeze & Cherry, 1979).

4.3 Infiltration Testing

The current Infiltration Assessment focused on the proposed subsurface infiltration chamber, which is sized to capture up to the 28 mm precipitation event runoff from the entire rooftop area. The purpose of this assessment was to assess the existing soil beneath the proposed LID location, and determine a suitable infiltration rate for use in detailed design.



4.3.1 Methodology

A field program was conducted by Azimuth staff on July 20th, 2023 between the hours of 8:00 am and 12:00 pm during which the weather was 22°C and overcast. One test pit was advanced by an excavating contractor at the western side of the Site in the area of the proposed LID (Figure 2). The test pit base elevation was therefore determined based on the ground elevation and test pit depth.

The Infiltration Assessment was completed in accordance with Appendix C of the *Low Impact Development Stormwater Management Planning and Design Guide* (TRCA 7 CVC, 2010). The test pits were advanced to an elevation approximately 0.2 m above the base of the LID (230.26 masl). A hand auger was then used within the test pit to remove approximately 0.2 m of additional soil. The infiltration assessment was therefore completed at the base of the proposed LID. Information on the proposed LID design in included in Appendix B and contained within the Stormwater Management & Servicing Report (Pearson, 2023). The test pit was approximately about 1.5 m wide and 4 m long. An additional 0.5 m was excavated after the testing was complete to confirm the underlying material for each test pit.

The Guelph Permeameter Model 2800K1 (Soil Moisture Equipment Corp.) was used to measure the in-situ hydraulic conductivity as per the *Guelph Permeameter Operating Instructions* (Soil Moisture, 2012). Due to the dominance of granular material encountered, the single head method using the combined reservoir was utilized. Two tests were completed within each end at the base of the TP-1 to assess potential variability in the soils. Each test was within an independent augered hole. The value from each of the two tests for each location were averaged to determine a representative value for the soil type.

Table 3: Summary of Test Pit Location Details

Test Pit ID (masl) 1	Base of Test Pit Elevation (masl) ¹	Depth (mbgs) ²
TP-1 (231.5)	230.2	1.3

NOTES:

A soil sample was collected from the test pit in the area of GP-1 at the approximate LID base elevation of infiltration testing for laboratory grain size and T-Time analysis. The soil sample analysis was used to confirm the in-situ results. After the infiltration tests

¹ Ground surface elevation taken from site survey information and includes the depth of the augered holes

² Depth below surface level is the target depth of proposed LID system.



were completed, the test pits were advanced an additional 0.5 m to confirm the underlying material, and then backfilled with the original soil material.

4.3.2 Test Results

The material encountered within the test pits was composed of 1.1 m of fill in TP-1 underlain by native sand to a depth of >1.6 mbgs. Ground water was not encountered in TP-1. The complete test pit logs, grain size analysis and infiltration testing summary tables have been included in Appendix I.

The Guelph Permeameter generates a result as a hydraulic conductivity (K_{fs}) value. As per Table C1 from CVC & TRCA (2010), the K_{fs} values from the Guelph Permeameter and percolation rate (T-Time) values from the grain size analysis have been converted to an infiltration rate (1/T).

Based on the information provided in Table 4, the measured in-situ infiltration rate at the Site ranged between 99 and 93 mm/hr. These rates are consistent with values expected from a silty sand to sand material. The in-situ testing results and the estimate based on the grain size analysis appear to be lower than the measured rates, which could be a function of variability in silt content of the unit or limitations in relating grain size distribution to actual infiltration rates. Given the consistency between the two Guelph Permeameter values, it is felt that these values are most representative for use in establishing infiltration capacity of the Site.

Table 4: Results of Infiltration Assessment

		Guel	Estimated		
Test Pit ID	Soil Type at Depth ¹	Test # 1 Infiltration Rate ² (mm/hr)	Test # 2 Infiltration Rate ² (mm/hr)	Geometric Mean Infiltration Rate (mm/hr)	Infiltration Rate from Soil Sample ^{1,3} (mm/hr)
TP-1	Silty Sand	99	93	96	20

NOTES:

- ¹ As per GEI Letter Report dated July 31st, 2023 titled T-Time Analyses, Ref. No. 21-492
- Guelph Permeameter results are converted from K_{fs} to 1/T according to Table C1 from TRCA & CVC (2010)
- 3 Soil sample collection results are converted from T-Time to 1/T according to Table C1 from TRCA & CVC (2010)

4.3.3 Recommendations

As per TRCA & CVC (2010), the infiltration rate used to design infiltration LIDs must incorporate a safety correction factor that compensates for potential reductions in soil permeability due to compaction or smearing during construction, gradual accumulation of fine sediments over the lifespan of the LID, and an uncertainty in measured values when less permeable soil horizons exist. A safety correction factor of 2.5 was used along with



the geometric mean for infiltration rate as per TRCA & CVC (2010). Table 5 summarizes the recommended design infiltration rate for the location investigated:

Table 5: Summary of Design Infiltration Rate

Geometric Mean Infiltration Rate* (mm/hr)	Safety Correction Factor	Design Infiltration Rate (mm/hr)
96	2.5	39

^{* -} geometric mean of tested soil beneath the LID facility

After applying a correction factor of 2.5, the design infiltration rate for the LID area is 39 mm/hr. The results for the Site indicate that the infiltration rate for the material at the base of the LID is variable but feasible given the mean infiltration values.

5.0 WATER BALANCE

In order to determine the potential changes to the natural ground water recharge conditions, a pre- and post-development water balance assessment has been completed using the Thornthwaite and Mather method (1957). This method evaluates evapotranspiration based on precipitation and temperature. Residual soil saturation is a function of topography and soil type. Monthly data are tabulated from daily average temperature and precipitation, and the water budget is a continuous calculation over the period of record. To clarify, the method and the approach used by many individuals in examining infiltration resets annual conditions (moisture deficit, snow storage, etc) over the winter months because of the general lack of infiltration during the frost period. However, we maintain those records and carry them forward from month to month during the entire period of record.

Values were determined on a monthly basis, compiled from daily Environment Canada meteorological data station located in Barrie, Ontario between 1970 and 2021 (Barrie Climate Station – Station ID 6110557 / 6110556). The calculations are based on the average conditions during this period. The average precipitation was 907 millimeters (mm), rainfall was 654 mm, evapotranspiration was 479 mm, and the surplus was 428 mm per year.

5.1 Land Use

5.1.1 Pre-Development

The pre-development Site area was classified according to land use/vegetation type. Land within the pre-development area is provided in Table 6.



Table 6: Pre Development Area Classification

Land Use	Land Area (m²)
Forest	1,248
Bare Ground	750
TOTAL	1,998

Land within the pre-development scenario is considered 0% impervious. The pre-development areas are shown on Figure 2.

5.1.2 Post-Development

The land classification in the post-development scenario was classified based on the Site Plan (Appendix B / Figure 2). Land within the post-development Site is summarized in the below Table 7:

Table 7: Post Development Area Classification

Land Use	Land Area (m²)
Landscaped Grass	658
Rooftop	448
Paved Surface	892
TOTAL	1,998

(LID) – areas represent catchments 201 & 209 (including all subcatchments), which is being directed into LID infiltration gallery

Land within the post-development scenario is considered 67% impervious.

5.2 Infiltration

Infiltration is generated one of two ways: (1) directly from rainfall impact or snowmelt on pervious surfaces; and (2) indirectly when runoff from impervious surfaces is diverted into adjacent naturalized areas.

Infiltration factors for the Site were estimated based on the underlying soil, local topography, and ground cover as per Table 2 of the Ministry of Environment and Energy (MOEE) Hydrogeological Technical Information Requirements for Land Development Applications (1995).

The soil variable factor was determined by taking into account information obtained from the regional geologic mapping and the geotechnical program completed for the Site. This information suggests that the surficial material at the Site is primarily composed of silty sand to sand, however some areas with surficial silt to silt and clay was noted. The infiltration factors utilized in the water balance assessment are summarized in Table 8 below.



Table 8: Summary of Pervious Land Infiltration Factor

Scenario	Land Use	Infiltration	Assumption		
		Factor			
Pre-Development	Forest	0.70	Rolling land (0.2), silty sand to sand soil		
		0.70	(0.3), treed (0.2)		
	Landscaped /	0.60	Rolling land (0.2), silty sand to sand soil		
	Grassed	0.00	(0.3), grassed (0.1)		
Post-Development	Landscaped /	0.60	Rolling land (0.2), silt sand to sand soil		
	Grassed	0.00	(0.3), lawn (0.1)		

5.2.1 Pre-Development Infiltration

Pre-development direct infiltration was determined by multiplying the annual average surplus amount, the area of each land use, and the infiltration factor for each land use. The pre-development annual infiltration is therefore 545 m³/year (Appendix H).

5.2.2 Post-Development Infiltration

Post-development infiltration (without mitigation) was determined by multiplying the annual average surplus amount, the area of each land use, and the infiltration factor for each land use. The post-development annual direct infiltration is therefore 169 m³/year. There is therefore a decrease in infiltration of 376 m³/year from pre- to post-development without mitigation measures employed.

The post-development drainage plan includes low impact development (LID) to promote infiltration. An infiltration gallery will be included in the storm water design to collect runoff from the rooftop area. The details for this feature are outlined in the Pearson (2023) Storm Water Management & Servicing Report, which indicate a storage volume of 12.6 m³. Based on this storage volume and a rooftop capture area of 448 m², the LID is capable of capturing a 28 mm precipitation event. In order to correlate event based rainfall data, for which the LID is designed (i.e. 28 mm precipitation event), to annual averages, as is what is utilized in water balances, an event based assessment has been completed for the Barrie Climate station. Precipitation events over a 10 year period (2012-2021) were broken down by event size, such that total volumes for each of these events could be calculated for capture from hard surface area (road, rooftop). These totals were then related to the total volume over the same period to obtain a percentage. This percentage is then multiplied by the annual average precipitation value (907 mm) utilized in the overall water balance to obtain an annual average amount / depth for the various intervals. It was determined that an event depth of 28 mm represented an average annual precipitation total of 614 mm or 96% of the rainfall events over this period of record. It is noted that these represent cumulative amounts for all precipitation amounts less than the stated event size. In order to quantify the annual infiltration volumes for the



LID, the annual precipitation depth (event equivalent) discussed above is multiplied by the roof area, while an evaporation loss factor was also applied (10%). This results in a mitigated infiltration volume of 351 m³, creating an overall post-development annual infiltration volume of 520 m³, limiting the overall deficit from the pre-development condition to a loss of 25 m³, or 5%.

5.3 Water Balance Summary

Using the climate model data and calculations mentioned above, the water balance was completed for pre-development, post-development, and post-development with mitigation (Appendix H).

The pre-development infiltration volume is 545 m³/year. This assumes the Site is composed of treed and grassed areas. The post-development without mitigation infiltration volume is 169 m³/year, which is a deficit of 376 m³/year. This assumes the Site is composed of the above noted residential development. An additional 351 m³/year of infiltration can be obtained through LID capture (infiltration gallery). As a result of this mitigation measure, the post-development with mitigation volume is therefore 520 m³/year which represents a small decrease of 25 m³/year (-5%) from the predevelopment configuration. Given this limited post-development infiltration deficit, no off-setting payments are required by the LSRCA as per their Water Balance Offsetting Policy (2023) (<100 m³/year).

As all post development surface runoff will be directed into the existing stormwater infrastructure along Burton Avenue, there will be a reduction in surface water contributions of 424 m³/year to the wetland to the north of the Site, the maintenance of ground water infiltration through the ground water infiltration chambers and additional infiltration in the shallow soil profile through the permeable pavers will offset the surface runoff reductions such that there is not expected to be a meaningful reduction of water contributions to the adjacent feature.

6.0 DEWATERING ASSESSMENT

A review of the Site servicing details indicated that the storm sewer infrastructure and potable water connection is all above the high water table at the Site, while the sanitary servicing connections at Burton Avenue will potentially intrude into the water table at the Burton Avenue connection by 0.7 m such that limited dewatering may be required if service connections are installed during high water table period (March – May). As such, calculations were completed to assess potential dewatering volumes under these conditions. However, if construction is completed during the summer / fall seasonal low water table conditions, water table is expected to be below the servicing connection elevations, as per the February, 2021 measurements (Appendix D).



A review of these items indicated that the maximum depths for the sanitary connections at Burton Avenue was at 228.44 masl, which are all below the maximum water table elevation of 229.39 masl for the Site in this location (BH21-1).

The following details and assumptions are included in this assessment:

- Construction ground water lowering will target a depth of 0.5 m below the base of the inverts to ensure dry working conditions;
- Water table depths are at or below the most elevated level observed at the Site, which is in close proximity to Burden Ave; and
- The entire length of sanitary servicing will be done at once which is 10 m in length and the width is 3 m.

The actual drawdown will depend on construction timing. It is therefore recommended that excavation / construction is completed in the dry summer months to avoid the need for dewatering.

6.1 Approximate Dewatering Volumes

For trench dewatering, the steady state method from Powers *et al.* (2007) used for rectangular excavations, where the length / width ratio is >1.5:

$$Q = \{ [(\pi^* K)^* (H^2 - h^2)] / [ln(R_o/r_e)] + 2*[a*K*(H^2 - h^2)/(2R_o)] \}$$
(Ref: Powers *et al.* (2007)

The full dewatering assessment can be found in Appendix F. The dewatering details for the sanitary servicing connections are provided in Table 9 below.

Based on the information provided in Table 3, only very minimal ground water lowering will be required for the sanitary servicing. The dewatering volume is 2,500 L/day, while a 3x safety factor can then be applied which would make the volume 7,500 L/day. These values are based on worst case spring season ground water values. The dewatering volume is anticipated to not be required during dry summer months.

Any construction dewatering between 50,000 L/day and 400,000 L/day can be completed after registration under the Environmental Activity and Sector Registry (EASR). Any active construction dewatering above 400,000 L/day requires a Permit to Take Water (PTTW). As noted above, the magnitude of dewatering required will vary on the timing



of construction and less or no dewatering could be needed in the summer drought conditions. Based on the limited dewatering volumes, no permitting is required and any ground water encountered can likely be handled relatively informally, such as discharge and containment on site if required.

Table 9: Summary of Dewatering Conditions (Appendix F)

Variable	Sanitary Sewer Connection
Estimate of Equivalent Radius [r _e] (m)	4
Hydraulic Conductivity [K] (m/s)	2.3 x 10 ⁻⁶
Maximum Required Drawdown [H-h] (m)	1.2
Saturated Thickness Before Pumping [H] (m)	1.7
Depth of Water During Pumping [h] (m)	0.5
length of excavation [a] (m)	10
width of excavation [b] (m)	3
Radius of Influence [R] (m) ¹	10
Discharge [Q] (L/day)	2,500
Discharge [Q] (L/day) 3 X Safety Factor Applied	<u>7,500</u>

6.2 Impact Assessment

Based on the information provided in Table 9, the largest zone of influence is 10 m, while the overall decline in water levels is quite limited due to the shallow intrusion in the water table. As such, no off-site impacts are expected as a result of any Site dewatering.

Given the potential for dewatering has shown to be limited, the small volumes potentially handled would not necessitate a formal dewatering discharge plan. It is assumed that all potential discharge can either be handled on-site. Mitigation measures would likely just be a tank or enviro-bag prior to discharge off-site storm sewer (if required).

6.3 Water Quality

A water sample was collected from BH21-1 on May 27th, 2020 to determine the on-site ground water quality in preparation for potential dewatering activities, while water quality results are also available from the Phase II ESA completed by Envision. The Azimuth results are included in Appendix D and have been compared to the Provincial Water Quality Objectives (PWQO), while the lab report from the Envision results has been included un-edited. All parameters met the PWQO with the exception of total phosphorus and aluminum.

The aluminum exceedance (0.08 mg/L), which is only marginally above PWQO (0.075 mg/L) is not seen as a concern as is commonly elevated in ground water due to the fact it is a naturally abundant earth element. The total phosphorus concentrations is more significantly elevated, but is interpreted to be sourced to the elevated sediment load in the

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sample as evidenced by the elevated turbidity (1,180 NTU). The nutrient analysis was completed on water that was unfiltered, and therefore contained a high concentration of sediment particles. The increased phosphorus is therefore likely attributed to the excess nutrients that are bound to the sediment grains in suspension and dissolved within the acidified nutrients bottle. Sodium (150-1,000 mg/L) and chloride (800-1,320 mg/L) concentrations were noted to be elevated, which is likely associated with road salt application on Burton Avenue. The nitrate concentrations are also elevated (4.9 mg/L), which could be the result of leaky sewer infrastructure along Burton Avenue.

Finally, a suite of volatile organic compounds (VOCs) and Petroleum Hydrocarbons (PHCs) were analyzed for at the Site monitoring wells. The results indicated only a single trace detection of toluene at BH21-4 (0.48 ug/L), which given the lack of any other measurable organic parameter concentration would indicate that the results may be anomolous. This was confirmed with an additional sample collected on July 20th, 2023, which indicated no detection for toluene.

Overall, the water quality would not be detrimental if maintained on-site or discharged to the storm sewers as all parameters are noted to meet City of Barrie Storm Sewer Bylaw criteria if required.

7.0 SUMMARY AND CONCLUSIONS

Azimuth was retained by Monolite Holdings Inc. to conduct a Hydrogeological Assessment for the property located at 181 Burton Avenue, within the City of Barrie, Ontario. The Site is rectangular in shape and is approximately 1,995 m² in size and is accessed via Burton Avenue. The Site is bound by Burton Avenue to the north, commercial properties to the east and west and vacant land to the north. The Site is at an elevation of 232 masl along Burton Avenue sloping down to 229 masl at the north end of the Site which directs existing surface runoff towards a small isolated wetland area immediately north of the Site. The Site will be developed as a single multi unit residential building with at grade parking at the north end of the Site.

Boreholes logs from the Site show the subsurface is composed of approximately 3 m silty sand fill overlying a native sand or silty sand material. The inferred ground water flow direction is generally to the north following local topography towards Lake Simcoe. Ground water elevations at the Site were measured between 227.57 and 229.39 masl. Hydraulic conductivity testing was completed within the monitoring well BH21-1 & 21-4 at the Site by Azimuth staff. Slug test data indicates that the hydraulic conductivity of the deposits is $\sim 2x10^{-6}$ m/s.



The pre-development infiltration volume is 545 m³/year. This assumes the Site is composed of treed and grassed areas. The post-development without mitigation infiltration volume is 169 m³/year, which is a deficit of 376 m³/year. This assumes the Site is composed of the above noted residential development. An additional 351 m³/year of infiltration can be obtained through LID capture (infiltration gallery). As a result of this mitigation measure, the post-development with mitigation volume is therefore 520 m³/year which represents a small decrease of 25 m³/year (-5%) from the predevelopment configuration. Given this limited post-development infiltration deficit, no off-setting payments are required by the LSRCA as per their Water Balance Offsetting Policy (2023) (<100 m³/year).

As all post development surface runoff will be directed into the existing stormwater infrastructure along Burton Avenue, there will be a reduction in surface water contributions of 424 m³/year to the wetland to the north of the Site, the maintenance of ground water infiltration through the ground water infiltration chambers and additional infiltration in the shallow soil profile through the permeable pavers will offset the surface runoff reductions such that there is not expected to be a meaningful reduction of water contributions to the adjacent feature.

Based on the ground water elevations and details related outlined on the development plan, all foundations and infrastructure will be located above the water table with the exception of the sanitary sewer connections at Burton Avenue. However, the intrusion is considered limited (~0.7 m) and of limited length (~10 m). It is also noted that this intrusion is only present during spring high water table conditions such that if the connections are completed during the summer and fall low water table conditions, dewatering will not be required. Despite this, a dewatering assessment was completed to assess requirements if these connections were completed during the spring high water table conditions. The daily water taking volume estimate is quite limited at 2,500 L/day or 7,500 L/day with a 3x safety factor. As such, no permitting would be required for any dewatering and it is likely that any ground water could be dealt with relatively informally with a sump and discharge on-site. The largest zone of influence is 10 m from the dewatering zone such that all drawdown will be maintained within the Site boundaries or road alignment.

Azimuth completed in-situ percolation testing at the site in July 2023 targeting the proposed LID location. The assessment was focused on the existing soil beneath the previously proposed LID locations to determine suitable infiltration rate for use in detailed design. The design infiltration rates for the Site are 93 to 99 mm/hr. After applying a correction factor of 2.5, the design infiltration rates for the Site is 39 mm/hr.



The results for the Site indicate that the infiltration rate for the material at the base of the LID is considered moderate to high.

8.0 REFERENCES

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- Toronto and Region Conservation Authority (TRCA) and Credit Valley Conservation (CVC). 2010. Low Impact Development Stormwater Management Planning And Design Guide. Version 1.



APPENDICES

Appendix A: Figures **Appendix B:** Site Plan

Appendix C: MECP Well Records

Appendix D: Borehole Logs & Ground Water Elevations
Appendix E: Hydraulic Conductivity Testing Results

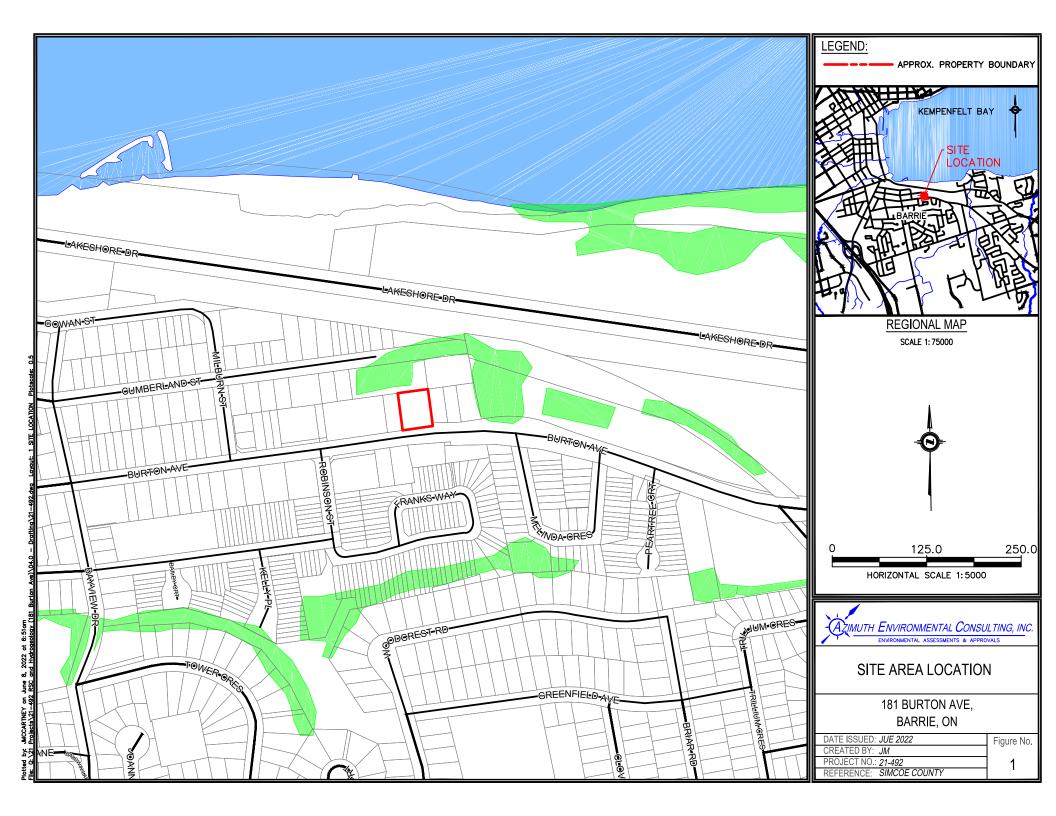
Appendix F: Dewatering Analysis
Appendix G: Water Quality Results
Appendix H: Water Balance Summary

Appendix I: Guelph Permeameter Testing Results



APPENDIX A

Figures





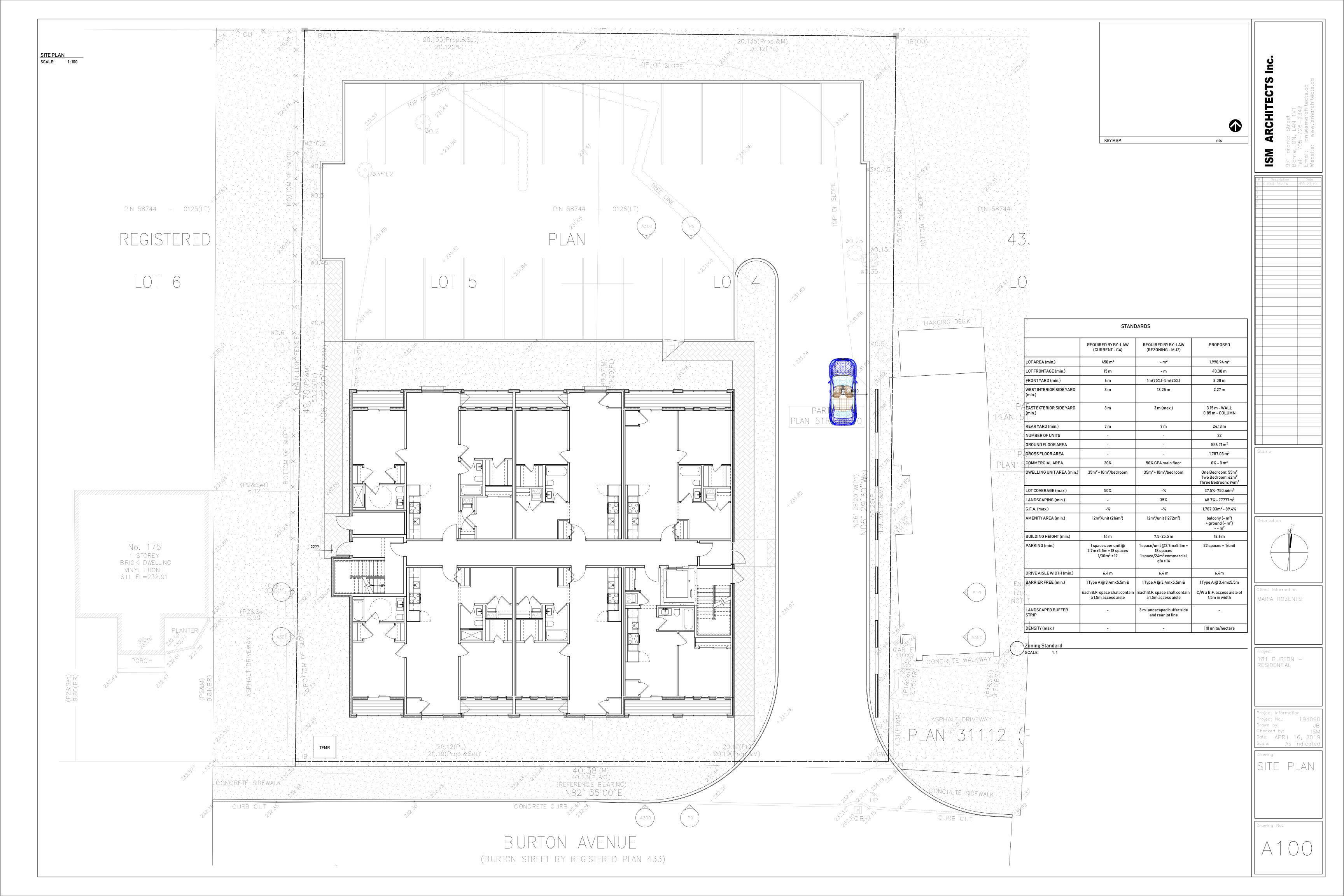


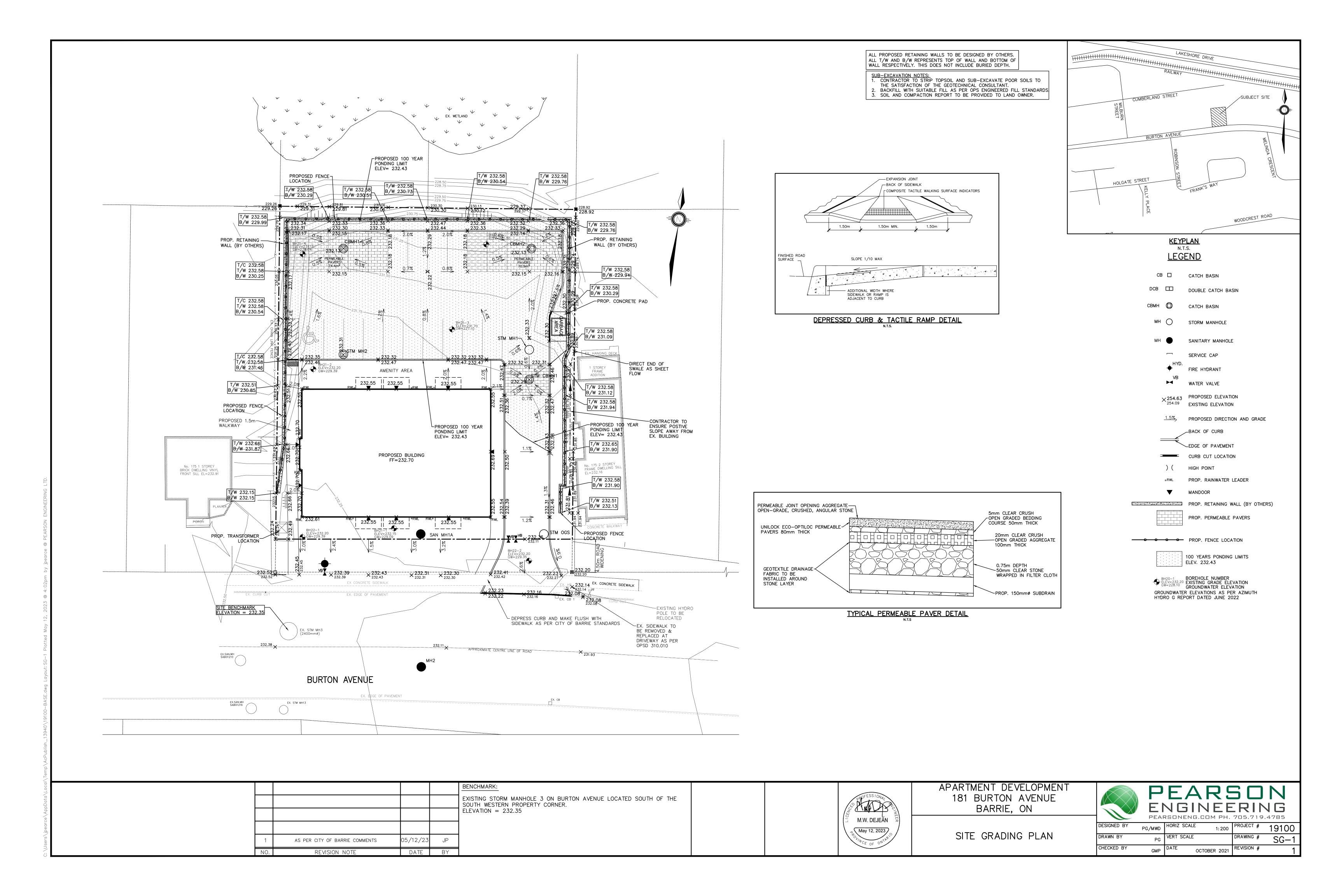


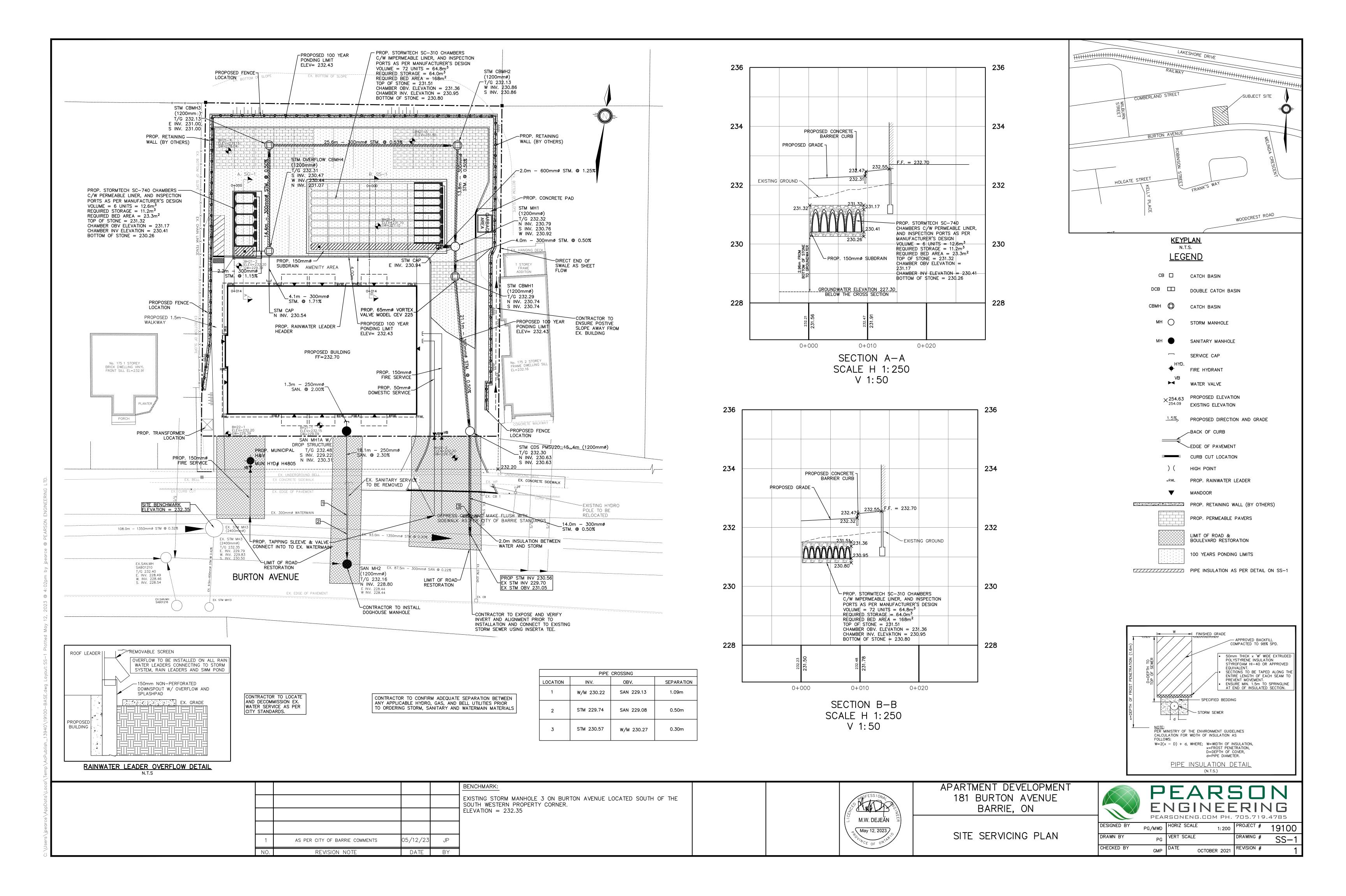


APPENDIX B

Development Plan









APPENDIX C

MECP Well Records

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Well Log 2/6	// *		Wate	r Record	
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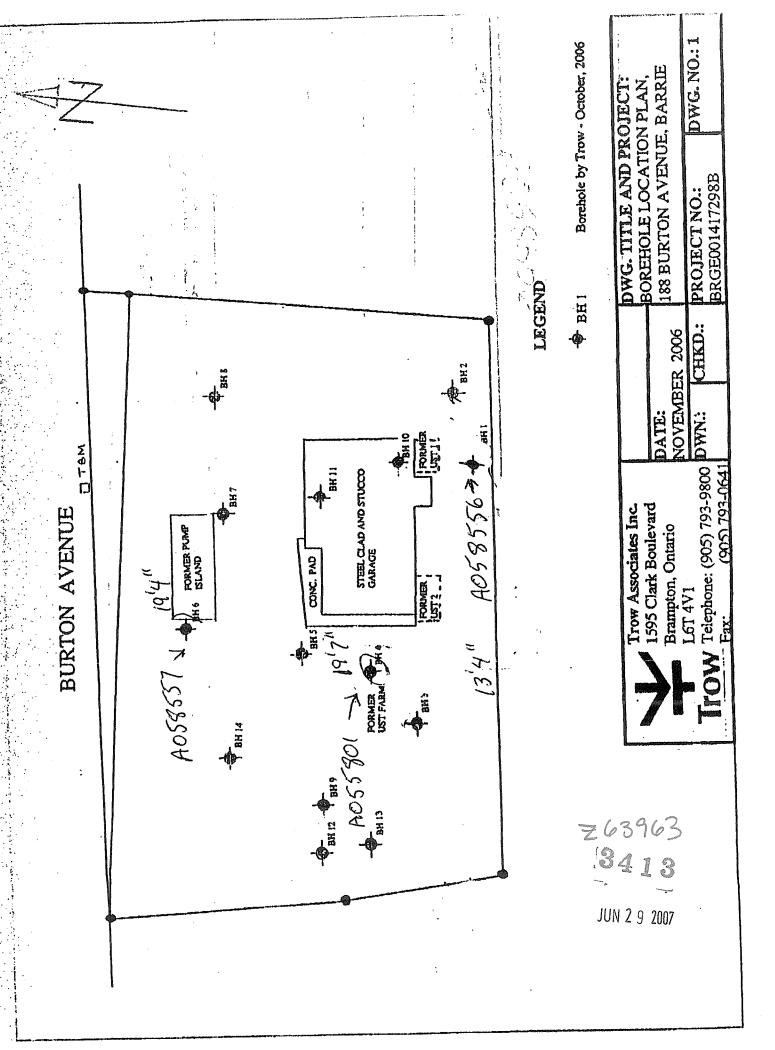
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Ministry of the Environment Well Tag No.

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Well Record

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Regulation 903 O A 058551 Page of Well Owner's Information First Name E-mail Address Last Name Well Constructed by Well Owner SOUTHVIEW AUTO CENTRE Mailing Address (Street Number/Name, RR) MD Municipality Province Telephone No. (inc. area code) N4N21511 7101517131712181216 BUDTON AVE BARRIE ONIT Part A Construction and/or Major Alteration of a Well Address of Well Location (Street Number/Name, RR) Concession Township 188 Subjon CITY OF BARRIE 3 TO 5 AVE City/Town/Village Postal Code Province SIM WE
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MOORE, JAMES

2007/06/27

Date Submitted (yyyy

Date Received (yyyy/mm/dd)

Remarks

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Bus.Telephone No. (inc. area code) Name of Well Technician (Last Name, First Name)

Signature of Technician

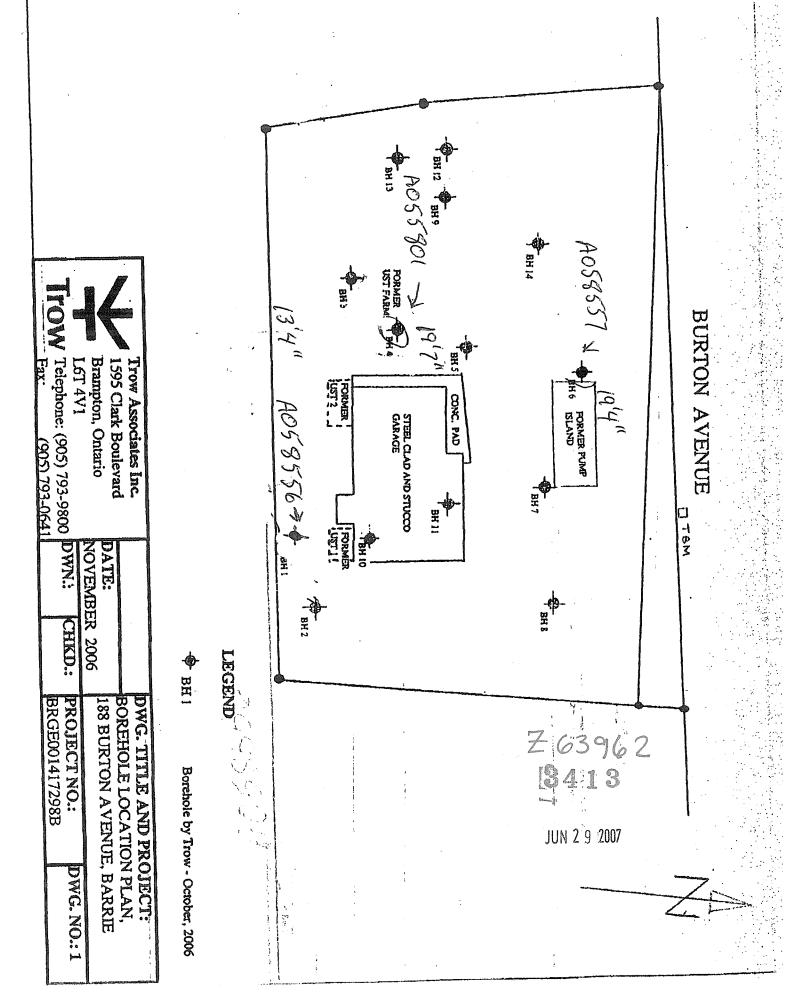
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er found at Depth Kind of Water: Fresh Untested	$\parallel \parallel T$
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(m/fi) Gas Other, specify Well Contractor and Well Technician Information ness Name of Well Contractor Well Contractor's Licence	CO NO. 15' of proportion
(m/fi) Gas Other, specify Well Contractor and Well Technician Information ness Name of Well Contractor Well Contractor's Licency ADDIA (Street Number/Name) Municipality	COmments O Comments O
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Well Contractor and Well Technician Information ness Name of Well Contractor Well Contractor Well Contractor's Licency ness Address (Street Number/Name) Municipality Ince Postal Code Business E-mail Address MOC 130 And ANSO 1	Comments Date Package Delivered Ministry Use Only
Well Contractor and Well Technician Information ness Name of Well Contractor No N	Comments Date Package Delivered Information package delivered Date Work Completed Date Work Completed
Well Contractor and Well Technician Information ness Name of Well Contractor Ness Address (Street Number/Name) Ince Postal Code Business E-mail Address Telephone No. (inc. area code) Name of Well Technician (Last Name, First Name)	Comments Date Package Delivered information package delivered vivi y y y m m D D Audit No. Z2 2 8 5 3 5

Ministry of the Environment and Climate Change

Well Tag No. (Place Sticker and/or Print Below)

Well Record

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General C			mon Material		Oth	er Materials		Gen	eral Description			Dep From	th (<i>m/ft</i>) To
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3.7_	6.1	J. 1.c	<u>a</u> 36/	<u> </u>						1		1	
							Pum	p intake set at (r	n/ft)	2		2	
	had at Car	etruction		W. Sangston, and 1888 and	10/20/11		Pum	ping rate (I/min /	GPM)	3		3	
Cable To	nod of Cor	Diamono	j ∏Pu	blic	Well Us			·		4		4	
Rotary (C	Conventional) Reverse)	☐ Jetting ☐ Driving	1 —	mestic estock	☐ Municipa	<u> </u>	Dura	tion of pumping hrs +	min	5		5	
Boring		Digging	☐ lmi	gation		& Air Conditioning	Final	water level end	of pumping (m/ft)	10		10	
Air percu	necify <u>Nual</u>	Robany		lustrial ner, <i>specify</i> _			If flow	ving give rate (Vr	nin / GPM)	15		15	
	1	struction R	T			Status of Well		ring give rate (in	Os 11.)	20		20	
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						Observation and/or Monitoring Hole	Well	production (I/min	(GPM)	50		50	
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envillanaesenineen		struction R				Abandoned, Insufficient Supply	1011101011	Yes No	Map of W	<u> </u>	ran a 4 at Address (1966)	7.000	
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UUU0E (2014/1	· · · <i>)</i>					Ministry's Copy					© Queer	s Printer for	Ontario, 2014

Ministry of the Environment

Well Tag No. (Place Sticker and/or Print Below)

Well Record

and Climate Change Tag#: A 208628 Regulation 903 Ontario Water Resources Act surements recorded in: 🔲 Metric 🔲 Imperial Well Owner's Information Last Name / Organization First Name E-mail Address ☐ Well Constructed Mailing Address (Street Number/Name) by Well Owner Corporation Municipality Postal Code Telephone No. (inc. area code) 01 L141N71419 Bourse Well Location Address of Well Location (Street Number/Name) Township Concession Lot County/District/Municipality City/Town/Village Postal Code Province Borne Municipal Plan and Sublot Number Ontario UTM Coordinates Zone , Easting Northing NAD | 8 | 3 | 1 | 7 | 6 | 0 | 5 | 1 | 7 | 2 | 4 | 9 | 1 | 3 | 8 | 5 | 4 Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form) General Colour Most Common Material Depth (*m/ft)* From | To General Description brown 1.5 Results of Well Yield Testing Annular Space Depth Set at (m/ft) Type of Sealant Used Volume Placed After test of well yield, water was: Draw Down Recovery (Material and Type) Time | Water Level | Time | Water Level (m^3/ft^2) Clear and sand free Other, specify (min) (m/ft) (min) (m/ft) Holeplya If pumping discontinued, give reason: Static Leve 1 1 Pump intake set at (m/ft) 2 2 3 3 Pumping rate (I/min / GPM) Method of Construction Well Use Cable Tool Diamond Commercial 4 4 Public ☐ Not used Duration of pumping Rotary (Conventional)
Rotary (Reverse) ☐ Jetting Domestic Dewatering ☐ Municipal hrs + 5 5 min Driving Livestock ☐ Test Hole Monitoring Boring Digging ☐ Irrigation Cooling & Air Conditioning Final water level end of pumping (m/ft): Air percussion 10 10 Industrial ☑ Other, specify 🔟 📶 Zotan Other, specify 15 15 If flowing give rate (Vmin / GPM) Construction Record - Casing Status of Well 20 20 Inside Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel) Wall Thickness Depth (m/ft) Water Supply Recommended pump depth (m/ft) Diameter (cm/in) Replacement Well 25 From То 25 (cm/in) Test Hole Recommended pump rate Recharge Well 30 30 0.635 (Vmin / GPM) 40,9 5.7 Dewatering Well 40 40 Observation and/or Well production (I/min / GPM) Monitorina Hole 50 50 ☐ Alteration Disinfected? (Construction) Yes No 60 Abandoned, Insufficient Supply Construction Record - Screen Map of Well Location Abandoned, Poor Outside Material (Plastic, Galvanized, Steel) Depth (m/ft) Water Quality Please provide a map below following instructions on the back Diamete (cm)(in) Slot No. Abandoned, other, To From specify Plastic 10 5.7 Other, specify Robinson Water Details Hole Diameter Water found at Depth Kind of Water: Fresh Untested Depth (m/ft) Diameter 1.5 - 6 (noth) Gas Other, specify From (cm/jn) Water found at Depth Kind of Water: Fresh Untested (m/ft) Gas Other, specify Water found at Depth Kind of Water: Fresh Untested (m/ft) Gas Other, specify Well Contractor and Well Technician Information Business Name of Well Contractor Well Contractor's Licence No. 7 | 3 BHI W BHZ Muniçipality Comments: Layout of Subdivision Proposed * Record Business E-mail Address BHZX Bus. Telephone No. (inc. area code) Name of Well Technician (Last Name, First Name) foe Well owner's information package delivered Ministry Use Only Date Package Delivered Audit No. Z251700 2016 NZ 23 md/or Contractor Date Submitted Date Work Completed Yes DEC 2 9 2016 2016/228 No

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Queen's Printer for Ontario, 2014



APPENDIX D

Borehole Logs & Ground Water Elevations



CLIENT: Monolite Holdings Inc.

Method: Solid Stem Auger

ENCL NO.: 1

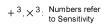
PROJECT LOCATION: Barrie, ON Diameter: 100 mm

DATUM: Geodetic Date: Jan-11-2021

BHLC	OCATION: See Figure 2		_	AMDI		Ι	Ι	SPT &	DYNA	MIC CO	NE PE	NETR/	ATION							
	SOIL PROFILE			AMPL	ES	H H				MIC CO		_		PLASTI LIMIT	c NAT	URAL STURE	LIQUID LIMIT	POCKET PEN. (Cu) (KPa)	-w⊤	REMARKS AND
(m)		STRATA PLOT			SI c	GROUND WATER CONDITIONS	z	_		10 60 RENGT		0 1	00	W _P	CON	N N	WL	ET PEI (KPa)	L UNIT	GRAIN SIZE
ELEV DEPTH	DESCRIPTION	TAP	NUMBER		BLOWS 0.3 m	ON OFFICE	EVATION	O U	NCONF	INED	+	FIELD V & Sensiti	ANE	 		0		POCK (Cu)	TURA (kN	DISTRIBUTION (%)
0000	Charles of Confess	STRA	S ME	TYPE	ž	SROI	ELEV			RIAXIAL 10 60	. ×	LAB V	ANE 00		TER CO		T (%) 30		A	GR SA SI CL
232.2	Ground Surface TOPSOIL	1/1/2			=						, ,	<u> </u>					1			GR SA SI CL
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229.8	SAND	F -						1												
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CLIENT: Monolite Holdings Inc.

Method: Solid Stem Auger

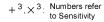
ENCL NO.: 2

PROJECT LOCATION: Barrie, ON Diameter: 100 mm

DATUM: Geodetic Date: Jan-11-2021

BH LO	OCATION: See Figure 2		_					SPT 8	DYNA	MIC CO	NF P	FNFTR	ATION	1					_	
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		IRA]	NUMBER	TYPE	<u>=</u>	30U	EV.	● Q	UICK 1	RIAXIA	L ×	LAB V	'ANE		TER C		NT (%)	2	NAT	(%)
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7.0																		1		
8817-00 88	 Upon completion of drilling the borehole was open with water 																			
AX 201-09	measured at 4.9 meters below ground surface.																			
01-128 M	ground candoc.																	1		
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	NDWATED ELEVATIONS					<u>GRAPH</u>	. 3	<u>.</u> 3.	Numbe	ers refer		8 =3%	6	. =						

GRAPH NOTES





CLIENT: Monolite Holdings Inc.

Method: Solid Stem Auger

ENCL NO.: 3

PROJECT LOCATION: Barrie, ON Diameter: 100 mm

DATUM: Geodetic Date: Jan-11-2021

BHLC	OCATION: See Figure 2		٦,	- A N 4 D I				SPT 8	DYNA	MIC CC	NE PE	NETR/	ATION								
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-	trace gravel, moist, very loose	\bowtie																			
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3.0	SILTY SAND Greenish grey, trace gravel, moist,		_	00	44			1													
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227.3	SILTY SAND	1 1.1																			
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6.6	End of Borehole																				
BH OGS OF	- Upon completion of drilling the borehole was open to 5.5 mBGS																				
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CLIENT: Monolite Holdings Inc.

Method: Solid Stem Auger

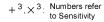
ENCL NO.: 4

PROJECT LOCATION: Barrie, ON Diameter: 100 mm

DATUM: Geodetic Date: Jan-11-2021

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(m)		LOT			थ्र	GROUND WATER CONDITIONS	z	L.	2			50 		10		W _P	COI	NTENT W	, LII	VL E	KPa)	N. €	GRAIN SIZE
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		TRA.	NUMBER	TYPE	M -	ROL OND	LEV.	•	+ QL	JICK T	RIAXIA	(L)	X L	AB V	ANE				ENT (%) [_	N A	(70)
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[- Brownish grey, wet	١.				:·目:		ŀ		1													
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CLIENT: Monolite Holdings Inc.

Method: Solid Stem Auger

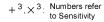
ENCL NO.: 5

PROJECT LOCATION: Barrie, ON Diameter: 100 mm

DATUM: Geodetic Date: Jan-11-2021

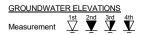
BH LC	DCATION: See Figure 2		_					SPT 8	DYNA	MIC CO	NF PF	NETRA	ATION							
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(m)		TO.			<u></u> ω	GROUND WATER CONDITIONS	7			40 60		30 1		LIMIT W _P	CON	ITENT W	LIMIT W _i	T PEN (Pa)	uNIT سُ)	AND GRAIN SIZE
ELEV DEPTH	DESCRIPTION	BLOWS 0.3 m	V QN JOE	ELEVATION	SHE/	AR ST NCONI	RENGT INED	ΓΗ (kF +	Pa) FIELD∨	ANE	i-		o	<u> </u>	SCKE SC SC SC SC SC SC SC SC SC SC SC SC SC	URAL (kN/i	DISTRIBUTION			
		STRATA PLOT	NUMBER	TYPE	M	ROU	EV#	● Q	UICK T	RIAXIAL	. ×	LAB V	ANE		TER CO		NT (%)	ā	NAT	(%)
	Ground Surface — TOPSOIL	\(\frac{1}{2}\).	ž		Z	ਹ ਹ	П	-	20 4	40 60	3 (30 1	00	1	0 2	20	30			GR SA SI CL
238.9	park brown silty sand, some gravel,																			
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[noist SILT AND SAND		ľ	00				ŀ۱												
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226.4	First (Birth)	: :	<u> </u>					_												
5.0	End of Borehole																			
700 BH 07	 Upon completion of drilling the borehole was open and dry. 																			
201-0951	porenoie was open and dry.																			
T-120 MWX																				
DCPT PLC																				
LOGSBIT																				
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	IDVA/ATED ELEVATIONS					<u>GRAPH</u>	. 3		Numbe	rs refer		8=3%		at Failu						







PROJECT: Phase Two Environmental Site Assessment REF. NO.: 22-0127 CLIENT: Monolite Holdings Inc. Method: Geo Probe ENCL NO.: ΚH PROJECT LOCATION: 181 Burton Avenue, Barrie, Ontario ORIGINATED BY Diameter: FL DATUM: Geodetic Date: Apr/08/2022 to Apr/08/2022 **COMPILED BY** CHECKED BY JA. BH LOCATION: N 4914009.96 E 605206.01 SOIL PROFILE SAMPLES Soil Head Space Vapors PLASTIC NATURAL LIQUIC MOISTURE LIMIT CONTENT LIMIT REMARKS GROUND WATER CONDITIONS PID CGD AND NATURAL UNIT (kN/m³) (m) STRATA PLOT GRAIN SIZE (ppm) (ppm) BLOWS 0.3 m ELEVATION ELEV DEPTH DISTRIBUTION DESCRIPTION NUMBER (%) WATER CONTENT (%) TYPE 10 20 30 10 20 30 20 GR SA SI CL 232.2 Ground Surface Rising Up Casing TOPSOIL: 100mm FILL: silty sand, trace gravel, trace clay, trace organics, dark brown, moist. 1A S PAHs silty sand to sandy silt at 0.8m 1B S 231 PHCs & BTEX Holeplug 2A S M&ORPs 230 SILTY SAND: trace clay, brown to grey, wet. 2B S W. L. 229.5 m Apr 11, 2022 229 ЗА S PHCs & BTEX grey below 3.8m 3B S 228 Screen S VOCs 227 4B S ²226.1 END OF BOREHOLE: 1) 50mm diameter monitoring well was installed upon completion, screened at 3.05-6.10m. 2) Water Level Readings: Water Level(mbgl): Date: April 11, 2022 2.73



GRAPH NOTES $+3, \times^3$: Numbers refer to Sensitivity

O $^{8=3\%}$ Strain at Failure

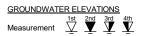


PROJECT: Phase Two Environmental Site Assessment REF. NO.: 22-0127 CLIENT: Monolite Holdings Inc. Method: Geo Probe ENCL NO.: ΚH PROJECT LOCATION: 181 Burton Avenue, Barrie, Ontario ORIGINATED BY Diameter: FL DATUM: Geodetic Date: Apr/08/2022 to Apr/08/2022 **COMPILED BY** CHECKED BY JA. BH LOCATION: N 4914013.89 E 605235.91 SOIL PROFILE SAMPLES Soil Head Space Vapors PLASTIC NATURAL LIQUIC MOISTURE LIMIT CONTENT LIMIT REMARKS GROUND WATER CONDITIONS PID CGD AND NATURAL UNIT (kN/m³) (m) STRATA PLOT GRAIN SIZE (ppm) (ppm) BLOWS 0.3 m ELEV DEPTH DISTRIBUTION DESCRIPTION NUMBER (%) WATER CONTENT (%) TYPE 10 20 30 10 20 30 20 GR SA SI CL 231.9 Ground Surface TOPSOIL: 100mm Rising Up Casing FILL: silty sand, trace gravel, trace clay, trace organics, dark brown, moist. 1A S PAHs 231 1B S M&ORPs -Holeplug 2A S 230 PHCs & BTEX SILTY SAND: trace clay, grey, wet. 2B S W. L. 229.3 m Apr 11, 2022 Sandı ЗА S PHCs & BTEX 228 3B S Screen 227 S VOCs 4B S 226 END OF BOREHOLE: 1) 50mm diameter monitoring well was installed upon completion, screened at 3.05-6.10m. 2) Water Level Readings: Water Level(mbgl): Date: April 11, 2022 2.73





PROJECT: Phase Two Environmental Site Assessment REF. NO.: 22-0127 Method: Geo Probe CLIENT: Monolite Holdings Inc. ENCL NO.: ΚH PROJECT LOCATION: 181 Burton Avenue, Barrie, Ontario ORIGINATED BY Diameter: FL DATUM: Geodetic Date: Apr/08/2022 to Apr/08/2022 **COMPILED BY** BH LOCATION: N 4914031.41 E 605220.08 CHECKED BY JA. SOIL PROFILE SAMPLES Soil Head Space Vapors PLASTIC NATURAL LIQUID MOISTURE LIMIT CONTENT REMARKS GROUND WATER CONDITIONS PID CGD AND NATURAL UNIT ((kN/m³) STRATA PLOT (m) GRAIN SIZE (ppm) (ppm) BLOWS 0.3 m ELEV DEPTH DISTRIBUTION DESCRIPTION NUMBER (%) WATER CONTENT (%) TYPE 10 20 30 40 10 20 30 40 20 30 GR SA SI CL 232.5 Ground Surface TOPSOIL: 100mm FILL: silty sand, trace gravel, trace clay, trace organics, dark brown, moist. 1A S PAHs 232 PHCs&BTEX 1B S M&ORPs 231 contains wood pieces at 1.5m 2A S FILL: sand, trace gravel, trace silt, trace clay, brown, wet. 230 2B S **2**29.5 SILTY SAND: trace clay, grey, wet. ЗА S 229 S 3B 228 END OF BOREHOLE:



GRAPH + 3





PROJECT: Phase Two Environmental Site Assessment REF. NO.: 22-0127 Method: Geo Probe CLIENT: Monolite Holdings Inc. ENCL NO.: ΚH PROJECT LOCATION: 181 Burton Avenue, Barrie, Ontario ORIGINATED BY Diameter: FL DATUM: Geodetic Date: Apr/08/2022 to Apr/08/2022 **COMPILED BY** BH LOCATION: N 4914047.67 E 605222.53 CHECKED BY JA. SOIL PROFILE SAMPLES Soil Head Space Vapors PLASTIC NATURAL LIQUID MOISTURE LIMIT CONTENT REMARKS GROUND WATER CONDITIONS PID CGD AND NATURAL UNIT (m) STRATA PLOT GRAIN SIZE (ppm) (ppm) BLOWS 0.3 m ELEVATION ELEV DEPTH DISTRIBUTION DESCRIPTION NUMBER (%) WATER CONTENT (%) TYPE 10 20 30 40 10 20 30 20 GR SA SI CL 232.3 Ground Surface TOPSOIL: 100mm FILL: silty sand, trace gravel, trace 232 clay, trace organics, dark brown, moist. 1A S PAHs 1B S PHCs&BTEX 231 2A S M&ORPs 230 2B S 229 S ЗА 228.5 SILTY SAND: trace gravel, trace clay, grey, wet. S 3B 228 227.7 END OF BOREHOLE:



GRAPH NOTES



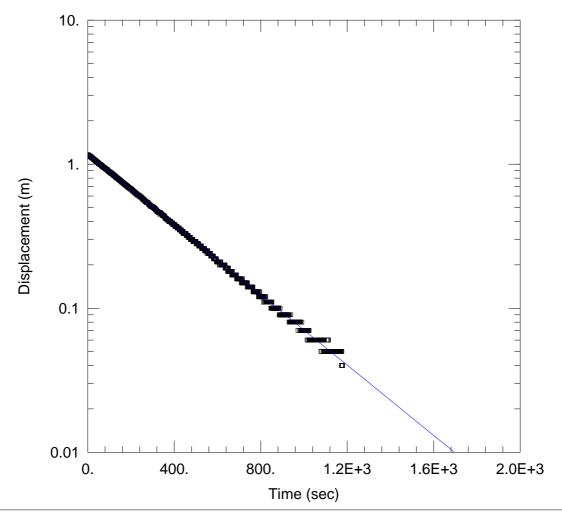
Monitoring Well Details & Ground Water Levels

Monitoring	Ground Elevation	Stickup	Reference Elevation	Total Depth		Gi	ound Water	· Level (mbg	js)			Gro	und Water E	levation (m	asl)	
Well	(masl)	(m)	(masl)	(mbgs)	10-Feb-21	16-Mar-22	28-Apr-22	12-May-22	06-Jun-22	20-Jul-23	10-Feb-21	16-Mar-22	28-Apr-22	12-May-22	06-Jun-22	20-Jul-23
BH21-1	232.20	0.80	233.00	4.60	4.08	3.14	3.06	3.12	3.25	3.13	228.12	229.06	229.14	229.08	228.95	229.07
BH21-4	231.60	0.81	232.41	5.00	4.03	3.09	3.06	3.10	3.22	3.15	227.57	228.51	228.54	228.50	228.38	228.45
BH22-1	232.2	0.95	233.15	6.13			2.81	2.87	3.01	2.84			229.39	229.33	229.19	229.36
BH22-2	231.9	1.07	232.97	5.86			2.85	2.88	2.97	2.83			229.05	229.02	228.93	229.07



APPENDIX E

Hydraulic Conductivity Testing Results



WELL TEST ANALYSIS

Data Set: M:\...\BH21-1 Slug Test.aqt

Date: 05/18/22 Time: 15:37:09

PROJECT INFORMATION

Company: Azimuth Environmental

Project: 21-492

Location: 181 Burton Street

Test Well: BH21-1

Test Date: May 12th 2022

AQUIFER DATA

Anisotropy Ratio (Kz/Kr): 1. Saturated Thickness: 1.58 m

WELL DATA (BH 21-1)

Initial Displacement: 1.16 m

Static Water Column Height: 1.58 m Total Well Penetration Depth: 1.58 m

Casing Radius: 0.0254 m

Screen Length: 1.52 m Wellbore Radius: 0.1 m

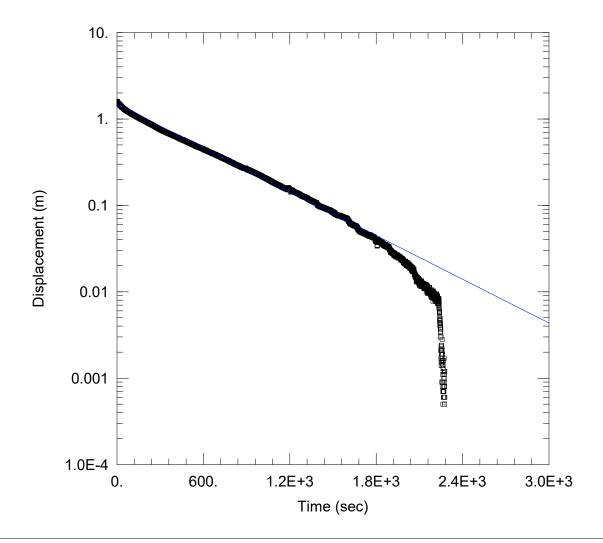
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 2.036E-6 m/sec

y0 = 1.17 m



181 BURTON

Data Set: M:\...\BH21-4 Slug Test.aqt

Date: 04/13/22 Time: 16:30:57

PROJECT INFORMATION

Company: Azimuth Environmental

Project: 21-492 Test Well: BH21-4 Test Date: Mar 16, 2022

AQUIFER DATA

Saturated Thickness: 1.91 m Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (BH21-4)

Initial Displacement: 1.6 m

Total Well Penetration Depth: 1.91 m

Casing Radius: 0.0254 m

Static Water Column Height: 1.91 m

Screen Length: 1.5 m Wellbore Radius: 0.075 m

SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 1.543E-6 m/sec

y0 = 1.484 m



APPENDIX F

Dewatering Analysis

Туре	ID	Length (m)	Width (m)	Effecitve Radius ¹ (m)	Hydraulic Conductivity (m/s)	Hydraulic Conductivity (m/day)	Initial Depth of Water (static head) prior to dewatering (m)		Depth of Water in the well while pumping (m)	h²	H-h (m)	H ² -h ²	Radius of Influence ² (m)	Discharge Into Ends ³ (m ³ /day)	Plane Discharge ⁴ (m³/day)	Total Discharge (m³/day)	Total Discharge (L/day)	Total Discharge x 1.5 Safety Factor (L/day)
		а	b	re	k	k	Н		h				Ro	Q	Q	Q	Q	Q
Servicing	Servicing Connection	10	3	4	2.30E-06	1.99E-01	1.70	3	0.5	0.3	3.0	3	10	2	0.5	2.5	2,500	7,500
Total Dewatering																	2,500	7,500

 $^{^{1}}$ r_{e} = (a+b) $/\pi$ - assuming a/b >1.5, or re = \sqrt{ab}/π (Powers et. al., 2007)

² Ro = r_e + 3000 * (H-h)* Vk - Sichardts Formula, (Cashman and Preene, 2001) ³ $Q = [(\pi^* K)^* (H^2 - h^2)] / [ln(R_o/r)]$ (Powers et al., 2007)

⁴ $Q = 2*[a*K*(H^2-h^2)/(2R_o)]$ (Powers et al., 2007) * H & h are relative to base of active ground water levels



APPENDIX G

Water Quality Results

Summary of Water Quality Data

				City of		BH21-1
			O, Reg. 153/04	City of Barrie Storm	Provincial Water Quality	Sampled on: 2022-03-16
			Table 2 Criteria	Sewer By- law	Objectives (1994)	Sampled by: SY
						Analyzed by:
Parameter	Symbol	Units			Objective	Caduceon
Saturation pH			-		-	6.51
pH (lab)			-	6.0-9.5	6.5-8.5	7.8
Langelier Saturation Index			-		-	1.29
Alkalinity (4.2) (as Calcium Carbonate)		mg/L	-		-	519
Bicarbonate	HCO ₃	mg/L	-		-	519
Carbonate	CO ₃ -2	mg/L	-		-	< 5
Hydroxide		0/	-		-	< 5
Conductivity		μS/cm	-		-	4980
Fluoride Chloride	F ⁻	mg/L	700		-	< 0.1
	CI ⁻ NO ₃ -N	mg/L	790		-	1320
Nitrate (as Nitrogen) Nitrite (as Nitrogen)	NO ₂ -N	mg/L	-		-	4.9 < 0.1
Bromide		mg/L	-			
Sulphate	Br ⁻ SO ₄ -2	mg/L mg/L	-		-	< 0.4 48
Calcium	Ca Ca	mg/L	-		-	197
Magnesium	Mg	mg/L	-		-	15.7
Sodium	Na	mg/L	490		-	825
Potassium	K	mg/L	-		-	3.1
Total Ammonia (as Nitrogen)	NH ₃ -N	mg/L	_		_	0.07
Phosphate (ortho)	PO ₄ -3	mg/L	_		_	0.019
Phosphorus	P	mg/L	_		0.02	0.95
Reactive Silica	Si	mg/L	_		-	8.58
Dissolved Organic Carbon	DOC	mg/L	-		-	2.1
Colour			-		-	3
Turbidity			-		-	1180
Aluminum	Al	mg/L	-		0.075	0.08
Arsenic	As	mg/L	0.025		0.1	< 0.0005
Barium	Ва	mg/L	1		-	0.268
Boron	В	mg/L	5		0.2	0.06
Cadmium	Cd	mg/L	0.0027	0.001	0.0005	< 0.000059
Chromium	Cr	mg/L	0.05	0.08	0.0089	0.002
Copper	Cu	mg/L	0.087	0.01	0.005	< 0.002
Iron	Fe	mg/L	-		0.3	< 0.005
Lead	Pb	mg/L	0.01	0.05	0.005	0.00027
Manganese	Mn	mg/L	-		-	0.001
Molybdenum	Мо	mg/L	0.07		0.04	< 0.01
Nickel	Ni	mg/L	0.1	0.05	0.025	< 0.01
Selenium	Se	mg/L	0.01		0.1	0.004
Silver	Ag	mg/L	0.0015		0.0001	< 0.0002
Strontium	Sr	mg/L	-		-	2.06
Thallium	TI	mg/L	0.002		0.0003	0.00005
Tin	Sn	mg/L	-		-	< 0.05
Titanium	Ti	mg/L	-		-	< 0.005
Uranium	U	mg/L	0.02		0.005	0.00065
Vanadium	V	mg/L	0.0062		0.006	< 0.0007
Zinc	Zn	mg/L	1.1		0.02	< 0.005
Total Dissolved Solids	TDS	mg/L	-		-	2745
Hardness (as Calcium Carbonate)		mg/L	-		-	557
% Difference / Ion Balanace			-		-	2.02

Bold and Highlighted indicates PWQO Exceedance

Bold and Italics indicates O.Reg. 153/04 Table 2 exceedance

Bold and Underlined indicates City of Barrie Storm Sewer Bylaw Exceedance



Report Date: 2022/11/29

EnVision Consultants Ltd. Client Project #: 22-0127.120 Site Location: 181 BURTON AVE

Sampler Initials: KH

O.REG 153 METALS & INORGANICS PKG (WTR)

Bureau Veritas ID			SIO598			SIO598			SIO599		
Sampling Date			2022/04/12			2022/04/12			2022/04/12		
Sampling Date			11:20			11:20			11:40		
COC Number			873637-01-01			873637-01-01			873637-01-01		
	UNITS	Criteria	BH20-1	RDL	QC Batch	BH20-1 Lab-Dup	RDL	QC Batch	BH20-4	RDL	QC Batch
Inorganics											
WAD Cyanide (Free)	ug/L	66	<1	1	7938174	<1	1	7938174	<1	1	7938174
Dissolved Chloride (Cl-)	mg/L	790	1400	15	7939326				180	2.0	7939326
Metals	•	•					•	•			•
Chromium (VI)	ug/L	25	1.0	0.50	7935665				<0.50	0.50	7935665
Mercury (Hg)	ug/L	0.29	<0.10	0.10	7937804				<0.10	0.10	7937804
Dissolved Antimony (Sb)	ug/L	6.0	<0.50	0.50	7940296				<0.50	0.50	7940296
Dissolved Arsenic (As)	ug/L	25	<1.0	1.0	7940296				<1.0	1.0	7940296
Dissolved Barium (Ba)	ug/L	1000	340	2.0	7940296				110	2.0	7940296
Dissolved Beryllium (Be)	ug/L	4.0	<0.40	0.40	7940296				<0.40	0.40	7940296
Dissolved Boron (B)	ug/L	5000	61	10	7940296				36	10	7940296
Dissolved Cadmium (Cd)	ug/L	2.7	<0.090	0.090	7940296				<0.090	0.090	7940296
Dissolved Chromium (Cr)	ug/L	50	<5.0	5.0	7940296				<5.0	5.0	7940296
Dissolved Cobalt (Co)	ug/L	3.8	<0.50	0.50	7940296				0.64	0.50	7940296
Dissolved Copper (Cu)	ug/L	87	2.0	0.90	7940296				1.7	0.90	7940296
Dissolved Lead (Pb)	ug/L	10	<0.50	0.50	7940296				<0.50	0.50	7940296
Dissolved Molybdenum (Mo)	ug/L	70	<0.50	0.50	7940296				<0.50	0.50	7940296
Dissolved Nickel (Ni)	ug/L	100	<1.0	1.0	7940296				1.4	1.0	7940296
Dissolved Selenium (Se)	ug/L	10	<2.0	2.0	7940296				<2.0	2.0	7940296
Dissolved Silver (Ag)	ug/L	1.5	<0.090	0.090	7940296				<0.090	0.090	7940296
Dissolved Sodium (Na)	ug/L	490000	1000000	500	7940296				150000	100	7940296
Dissolved Thallium (TI)	ug/L	2.0	<0.050	0.050	7940296				<0.050	0.050	7940296
Dissolved Uranium (U)	ug/L	20	0.67	0.10	7940296				0.65	0.10	7940296
Dissolved Vanadium (V)	ug/L	6.2	<0.50	0.50	7940296				1.4	0.50	7940296
Dissolved Zinc (Zn)	ug/L	1100	<5.0	5.0	7940296				<5.0	5.0	7940296

No Fill Grey Black

No Exceedance

Exceeds 1 criteria policy/level Exceeds both criteria/levels

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

Lab-Dup = Laboratory Initiated Duplicate

Criteria: Ontario Reg. 153/04 (Amended April 15, 2011)

Table 2: Full Depth Generic Site Condition Standards in a Potable Ground Water Condition



Sampler Initials: KH

O.REG 153 METALS & INORGANICS PKG (WTR)

Bureau Veritas ID			SIO600		SIO601		
Sampling Date			2022/04/12		2022/04/12		
Jamping Date			11:00		10:30		
COC Number			873637-01-01		873637-01-01		
	UNITS	Criteria	BH22-1	RDL	BH22-2	RDL	QC Batch
Inorganics							
WAD Cyanide (Free)	ug/L	66	1	1	<1	1	7938174
Dissolved Chloride (Cl-)	mg/L	790	800	7.0	1200	10	7939326
Metals	•						
Chromium (VI)	ug/L	25	<0.50	0.50	<0.50	0.50	7935665
Mercury (Hg)	ug/L	0.29	<0.10	0.10	<0.10	0.10	7937804
Dissolved Antimony (Sb)	ug/L	6.0	<0.50	0.50	<0.50	0.50	7940296
Dissolved Arsenic (As)	ug/L	25	<1.0	1.0	<1.0	1.0	7940296
Dissolved Barium (Ba)	ug/L	1000	200	2.0	270	2.0	7940296
Dissolved Beryllium (Be)	ug/L	4.0	<0.40	0.40	<0.40	0.40	7940296
Dissolved Boron (B)	ug/L	5000	52	10	58	10	7940296
Dissolved Cadmium (Cd)	ug/L	2.7	<0.090	0.090	<0.090	0.090	7940296
Dissolved Chromium (Cr)	ug/L	50	<5.0	5.0	<5.0	5.0	7940296
Dissolved Cobalt (Co)	ug/L	3.8	<0.50	0.50	<0.50	0.50	7940296
Dissolved Copper (Cu)	ug/L	87	1.7	0.90	1.3	0.90	7940296
Dissolved Lead (Pb)	ug/L	10	<0.50	0.50	<0.50	0.50	7940296
Dissolved Molybdenum (Mo)	ug/L	70	0.94	0.50	1.0	0.50	7940296
Dissolved Nickel (Ni)	ug/L	100	<1.0	1.0	<1.0	1.0	7940296
Dissolved Selenium (Se)	ug/L	10	<2.0	2.0	<2.0	2.0	7940296
Dissolved Silver (Ag)	ug/L	1.5	<0.090	0.090	<0.090	0.090	7940296
Dissolved Sodium (Na)	ug/L	490000	570000	100	740000	500	7940296
Dissolved Thallium (TI)	ug/L	2.0	<0.050	0.050	<0.050	0.050	7940296
Dissolved Uranium (U)	ug/L	20	1.2	0.10	0.53	0.10	7940296
Dissolved Vanadium (V)	ug/L	6.2	1.0	0.50	0.50	0.50	7940296
Dissolved Zinc (Zn)	ug/L	1100	15	5.0	<5.0	5.0	7940296

No Fill

No Exceedance

Grey Black

Exceeds 1 criteria policy/level

Exceeds both criteria/levels

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

Criteria: Ontario Reg. 153/04 (Amended April 15, 2011)

Table 2: Full Depth Generic Site Condition Standards in a Potable Ground Water Condition



Sampler Initials: KH

O.REG 153 VOCS BY HS & F1-F4 (WATER)

Bureau Veritas ID			SIO598	SIO599	SIO600	SIO601	SIO602		
Committee Date			2022/04/12	2022/04/12	2022/04/12	2022/04/12	2022/04/12		
Sampling Date			11:20	11:40	11:00	10:30	10:30		
COC Number			873637-01-01	873637-01-01	873637-01-01	873637-01-01	873637-01-01		
	UNITS	Criteria	BH20-1	BH20-4	BH22-1	BH22-2	GW22-1	RDL	QC Batch
Calculated Parameters									
1,3-Dichloropropene (cis+trans)	ug/L	0.5	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7936373
Volatile Organics									
Acetone (2-Propanone)	ug/L	2700	<10	<10	<10	<10	<10	10	7938140
Benzene	ug/L	5.0	<0.17	<0.17	<0.17	<0.17	<0.17	0.17	7938140
Bromodichloromethane	ug/L	16.0	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7938140
Bromoform	ug/L	25.0	<1.0	<1.0	<1.0	<1.0	<1.0	1.0	7938140
Bromomethane	ug/L	0.89	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7938140
Carbon Tetrachloride	ug/L	0.79	<0.20	<0.20	<0.20	<0.20	<0.20	0.20	7938140
Chlorobenzene	ug/L	30	<0.20	<0.20	<0.20	<0.20	<0.20	0.20	7938140
Chloroform	ug/L	2.4	<0.20	<0.20	<0.20	<0.20	<0.20	0.20	7938140
Dibromochloromethane	ug/L	25.0	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7938140
1,2-Dichlorobenzene	ug/L	3.0	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7938140
1,3-Dichlorobenzene	ug/L	59	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7938140
1,4-Dichlorobenzene	ug/L	1.0	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7938140
Dichlorodifluoromethane (FREON 12)	ug/L	590	<1.0	<1.0	<1.0	<1.0	<1.0	1.0	7938140
1,1-Dichloroethane	ug/L	5	<0.20	<0.20	<0.20	<0.20	<0.20	0.20	7938140
1,2-Dichloroethane	ug/L	1.6	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7938140
1,1-Dichloroethylene	ug/L	1.6	<0.20	<0.20	<0.20	<0.20	<0.20	0.20	7938140
cis-1,2-Dichloroethylene	ug/L	1.6	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7938140
trans-1,2-Dichloroethylene	ug/L	1.6	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7938140
1,2-Dichloropropane	ug/L	5.0	<0.20	<0.20	<0.20	<0.20	<0.20	0.20	7938140
cis-1,3-Dichloropropene	ug/L	0.5	<0.30	<0.30	<0.30	<0.30	<0.30	0.30	7938140
trans-1,3-Dichloropropene	ug/L	0.5	<0.40	<0.40	<0.40	<0.40	<0.40	0.40	7938140
Ethylbenzene	ug/L	2.4	<0.20	<0.20	<0.20	<0.20	<0.20	0.20	7938140
Ethylene Dibromide	ug/L	0.2	<0.20	<0.20	<0.20	<0.20	<0.20	0.20	7938140
Hexane	ug/L	51	<1.0	<1.0	<1.0	<1.0	<1.0	1.0	7938140
Methylene Chloride(Dichloromethane)	ug/L	50	<2.0	<2.0	<2.0	<2.0	<2.0	2.0	7938140
Methyl Ethyl Ketone (2-Butanone)	ug/L	1800	<10	<10	<10	<10	<10	10	7938140

No Fill Grey Black

No Exceedance

Exceeds 1 criteria policy/level Exceeds both criteria/levels

RDL = Reportable Detection Limit QC Batch = Quality Control Batch

Criteria: Ontario Reg. 153/04 (Amended April 15, 2011)

Table 2: Full Depth Generic Site Condition Standards in a Potable Ground Water Condition



Sampler Initials: KH

O.REG 153 VOCS BY HS & F1-F4 (WATER)

Bureau Veritas ID			SIO598	SIO599	SIO600	SIO601	SIO602		
Sampling Date			2022/04/12	2022/04/12	2022/04/12	2022/04/12	2022/04/12		
Sampling Date			11:20	11:40	11:00	10:30	10:30		
COC Number			873637-01-01	873637-01-01	873637-01-01	873637-01-01	873637-01-01		
	UNITS	Criteria	BH20-1	BH20-4	BH22-1	BH22-2	GW22-1	RDL	QC Batch
Methyl Isobutyl Ketone	ug/L	640	<5.0	<5.0	<5.0	<5.0	<5.0	5.0	7938140
Methyl t-butyl ether (MTBE)	ug/L	15	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7938140
Styrene	ug/L	5.4	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7938140
1,1,1,2-Tetrachloroethane	ug/L	1.1	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7938140
1,1,2,2-Tetrachloroethane	ug/L	1.0	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7938140
Tetrachloroethylene	ug/L	1.6	<0.20	<0.20	<0.20	<0.20	<0.20	0.20	7938140
Toluene	ug/L	24	<0.20	0.48	<0.20	<0.20	<0.20	0.20	7938140
1,1,1-Trichloroethane	ug/L	200	<0.20	<0.20	<0.20	<0.20	<0.20	0.20	7938140
1,1,2-Trichloroethane	ug/L	4.7	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7938140
Trichloroethylene	ug/L	1.6	<0.20	<0.20	<0.20	<0.20	<0.20	0.20	7938140
Trichlorofluoromethane (FREON 11)	ug/L	150	<0.50	<0.50	<0.50	<0.50	<0.50	0.50	7938140
Vinyl Chloride	ug/L	0.5	<0.20	<0.20	<0.20	<0.20	<0.20	0.20	7938140
p+m-Xylene	ug/L	-	<0.20	<0.20	<0.20	<0.20	<0.20	0.20	7938140
o-Xylene	ug/L	-	<0.20	<0.20	<0.20	<0.20	<0.20	0.20	7938140
Total Xylenes	ug/L	300	<0.20	<0.20	<0.20	<0.20	<0.20	0.20	7938140
F1 (C6-C10)	ug/L	750	<25	<25	<25	<25	<25	25	7938140
F1 (C6-C10) - BTEX	ug/L	750	<25	<25	<25	<25	<25	25	7938140
F2-F4 Hydrocarbons	•	,			•			•	
F2 (C10-C16 Hydrocarbons)	ug/L	150	<100	<100	<100	<100	<100	100	7941387
F3 (C16-C34 Hydrocarbons)	ug/L	500	<200	<200	<200	<200	<200	200	7941387
F4 (C34-C50 Hydrocarbons)	ug/L	500	<200	<200	<200	<200	<200	200	7941387
Reached Baseline at C50	ug/L	-	Yes	Yes	Yes	Yes	Yes		7941387
Surrogate Recovery (%)									
o-Terphenyl	%	-	99	99	100	99	98		7941387
4-Bromofluorobenzene	%	-	87	88	87	88	88		7938140
D4-1,2-Dichloroethane	%	-	106	106	107	105	106		7938140
D8-Toluene	%	-	91	92	92	92	91		7938140

No Fill
Grey
Black

No Exceedance

Exceeds 1 criteria policy/level Exceeds both criteria/levels

RDL = Reportable Detection Limit
QC Batch = Quality Control Batch

Criteria: Ontario Reg. 153/04 (Amended April 15, 2011)

Table 2: Full Depth Generic Site Condition Standards in a Potable Ground Water Condition



Sampler Initials: KH

O.REG 153 VOCS BY HS (WATER)

Bureau Veritas ID			SIO603		
Sampling Date			2022/04/12		
COC Number			873637-01-01		
	UNITS	Criteria	TRIP BLANK	RDL	QC Batch
Calculated Parameters					
1,3-Dichloropropene (cis+trans)	ug/L	0.5	<0.50	0.50	7936373
Volatile Organics					
Acetone (2-Propanone)	ug/L	2700	<10	10	7938148
Benzene	ug/L	5.0	<0.20	0.20	7938148
Bromodichloromethane	ug/L	16.0	<0.50	0.50	7938148
Bromoform	ug/L	25.0	<1.0	1.0	7938148
Bromomethane	ug/L	0.89	<0.50	0.50	7938148
Carbon Tetrachloride	ug/L	0.79	<0.19	0.19	7938148
Chlorobenzene	ug/L	30	<0.20	0.20	7938148
Chloroform	ug/L	2.4	<0.20	0.20	7938148
Dibromochloromethane	ug/L	25.0	<0.50	0.50	7938148
1,2-Dichlorobenzene	ug/L	3.0	<0.40	0.40	7938148
1,3-Dichlorobenzene	ug/L	59	<0.40	0.40	7938148
1,4-Dichlorobenzene	ug/L	1.0	<0.40	0.40	7938148
Dichlorodifluoromethane (FREON 12)	ug/L	590	<1.0	1.0	7938148
1,1-Dichloroethane	ug/L	5	<0.20	0.20	7938148
1,2-Dichloroethane	ug/L	1.6	<0.49	0.49	7938148
1,1-Dichloroethylene	ug/L	1.6	<0.20	0.20	7938148
cis-1,2-Dichloroethylene	ug/L	1.6	<0.50	0.50	7938148
trans-1,2-Dichloroethylene	ug/L	1.6	<0.50	0.50	7938148
1,2-Dichloropropane	ug/L	5.0	<0.20	0.20	7938148
cis-1,3-Dichloropropene	ug/L	0.5	<0.30	0.30	7938148
trans-1,3-Dichloropropene	ug/L	0.5	<0.40	0.40	7938148
Ethylbenzene	ug/L	2.4	<0.20	0.20	7938148
Ethylene Dibromide	ug/L	0.2	<0.19	0.19	7938148
Hexane	ug/L	51	<1.0	1.0	7938148
Methylene Chloride(Dichloromethane)	ug/L	50	<2.0	2.0	7938148
Methyl Ethyl Ketone (2-Butanone)	ug/L	1800	<10	10	7938148

No Fill Grey

Black

No Exceedance

Exceeds 1 criteria policy/level

Exceeds both criteria/levels

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

Criteria: Ontario Reg. 153/04 (Amended April 15, 2011)

Table 2: Full Depth Generic Site Condition Standards in a Potable Ground Water Condition



Sampler Initials: KH

O.REG 153 VOCS BY HS (WATER)

Bureau Veritas ID			SIO603		
Sampling Date			2022/04/12		
COC Number			873637-01-01		
	UNITS	Criteria	TRIP BLANK	RDL	QC Batch
Methyl Isobutyl Ketone	ug/L	640	<5.0	5.0	7938148
Methyl t-butyl ether (MTBE)	ug/L	15	<0.50	0.50	7938148
Styrene	ug/L	5.4	<0.40	0.40	7938148
1,1,1,2-Tetrachloroethane	ug/L	1.1	<0.50	0.50	7938148
1,1,2,2-Tetrachloroethane	ug/L	1.0	<0.40	0.40	7938148
Tetrachloroethylene	ug/L	1.6	<0.20	0.20	7938148
Toluene	ug/L	24	<0.20	0.20	7938148
1,1,1-Trichloroethane	ug/L	200	<0.20	0.20	7938148
1,1,2-Trichloroethane	ug/L	4.7	<0.40	0.40	7938148
Trichloroethylene	ug/L	1.6	<0.20	0.20	7938148
Trichlorofluoromethane (FREON 11)	ug/L	150	<0.50	0.50	7938148
Vinyl Chloride	ug/L	0.5	<0.20	0.20	7938148
p+m-Xylene	ug/L	-	<0.20	0.20	7938148
o-Xylene	ug/L	-	<0.20	0.20	7938148
Total Xylenes	ug/L	300	<0.20	0.20	7938148
Surrogate Recovery (%)					
4-Bromofluorobenzene	%	-	90		7938148
D4-1,2-Dichloroethane	%	-	112		7938148
D8-Toluene	%	-	93		7938148

No Fill Grey

No Exceedance

Exceeds 1 criteria policy/level

Black Exceeds both criteria/levels

RDL = Reportable Detection Limit QC Batch = Quality Control Batch

Criteria: Ontario Reg. 153/04 (Amended April 15, 2011)

Table 2: Full Depth Generic Site Condition Standards in a Potable Ground Water Condition



REPORT NO: 23-018389

COC #: -

Report To:
Azimuth Environmental

642 Welham Rd Barrie, ON L4N9A1 **CADUCEON Environmental Laboratories**

112 Commerce Park Dr Unit L

Barrie, ON L4N 8W8 Tel: 705-252-5743

Attention: Alan Turner

DATE SUBMITTED: 20-Jul-23 CUSTOMER PROJECT: 21-492
DATE REPORTED: 28-Jul-23 P.O. NUMBER:
SAMPLE MATRIX: Ground Water WATERWORKS NO:

R153 Tbl. 2 - PGW

	Client ID:		MW 21-4	R153 Table 2 - Potable Ground
	Sample ID:		23-018389-1	
	Date Collected:		20-Jul-23	Maximum Concentration
Parameter	Units	R.L.		
Benzene	μg/L	0.5	<0.5	5
Ethylbenzene	μg/L	0.5	<0.5	2.4
Toluene	μg/L	0.5	<0.5	24
Xylene, m,p-	μg/L	1	<1	
Xylene, m,p,o-	μg/L	1.1	<1.1	300
Xylene, o-	μg/L	0.5	<0.5	

R.L. = Reporting Limit

The analytical results reported herein refer to the samples as received. Reproduction of this analytical report in full or in part is prohibited without prior written consent from Caduceon Environmental Laboratories.



APPENDIX H

Water Balance Summary

Table A: Pre-Development

Table A: Pre-Developmen			
Catchment Designation	Landscaped Grass	Forest	Total
Area (m²)	1,248	750	1,998
Pervious Area (m ²)	1,248	750	1,998
Impervious Area (m²)	0	0	0
Infiltration Factors	<u>'</u>	L	
Topography Infiltration Factor	0.2	0.2	
Soil Infiltration Factor	0.3	0.3	
Land Cover Infiltration Factor	0.1	0.2	
Infiltration Factor	0.6	0.7	
Run-Off Coefficient	0.4	0.3	
Run-Off From Impervious Surfaces	0.8	0.8	
Inputs (Per Unit Area)		T	
Precipitation (mm/yr)	907	907	907
Rainfall (mm/yr)	654	654	654
Run-On (mm/yr)	0	0	0
Other Inputs (mm/yr)	907	907	907
Total Inputs (mm/yr) Outputs (Per Unit Area)	907	907	907
Precipitation Surplus (mm/yr)	428	428	428
Net Surplus (mm/yr)	428	428	428
Evapotranspiration (mm/yr)	479	479	479
Infiltration (mm/yr)	257	300	273
Surplus Infiltration (mm/yr)	0	0	0
Total Infiltration (mm/yr)	257	300	273
Run-Off Pervious Areas (mm/yr)	171	128	155
Run-Off Impervious Areas (mm/yr)	0	0	0
Total Run-Off (mm/yr)	171	128	155
Total Outputs (mm/yr)	907	907	907
Difference (Inputs - Outputs)	0	0	0
Inputs (Volumes)		1	
Precipitation (m³/yr)	1,132	680	1,812
Run-On (m³/yr)	0	0	0
Other Inputs (m ³ /yr)	0	0	0
Total Inputs (m ³ /yr)	1,132	680	1,812
Outputs (Volumes)			
Precipitation Surplus (m³/yr)	534	321	855
Net Surplus (m³/yr)	534	321	855
Evapotranspiration (m³/yr)	598	359	957
Infiltration (m³/yr)	320	225	545
Surplus Infiltration (m³/yr)	0	0	0
Total Infiltration (m³/yr)	320	225	545
Run-Off Pervious Areas (m³/yr)	214	96	310
Run-Off Impervious Areas (m³/yr)	0	0	0
Total Run-Off (m³/yr)	214	96	310
Total Outputs (m³/yr)	1,132	680	1,812
Difference (Inputs - Outputs)	0	0	0

Table B: Post-Development (no mit)

Table B: Post-Developme	it (110 mit)			
Catchment Designation	Landscaped Grass	Paved Surface	Building	Total
Area (m²)	658	892	448	1,998
Pervious Area (m ²)	658	0	0	658
Impervious Area (m²)	0	892	448	1,340
Infiltration Factors		<u> </u>	<u> </u>	,
Topography Infiltration Factor	0.2	0	0	
Soil Infiltration Factor	0.3	0	0	
Land Cover Infiltration Factor	0.1	0	0	
Infiltration Factor	0.6	0	0	
Run-Off Coefficient	0.4	1	1	
Run-Off From Impervious Surfaces	0.8	0.8	0.8	
Inputs (Per Unit Area)	007			
Precipitation (mm/yr)	907	907	907	907
Rainfall (mm/yr) Run-On (mm/yr)	654 0	654 0	654 0	654 0
Other Inputs (mm/yr)	0	0	0	0
Total Inputs (mm/yr)	907	907	907	907
Outputs (Per Unit Area)	301	307	307	901
Precipitation Surplus (mm/yr)	428	726	726	628
Net Surplus (mm/yr)	428	726	726	628
Evapotranspiration (mm/yr)	479	181	181	279
Infiltration (mm/yr)	257	0	0	85
Surplus Infiltration (mm/yr)	0	0	0	0
Total Infiltration (mm/yr)	257	0	0	85
Run-Off Pervious Areas (mm/yr)	171	0	0	56
Run-Off Impervious Areas (mm/yr)	0	726	726	487
Total Run-Off (mm/yr)	171	726	726	543
Total Outputs (mm/yr)	907	907	907	907
Difference (Inputs - Outputs)	0	0	0	0
Inputs (Volumes)			1 1	
Precipitation (m³/yr)	597	809	406	1,812
Run-On (m³/yr)	0	0	0	0
Other Inputs (m³/yr)	0	0	0	0
Total Inputs (m³/yr)	597	809	406	1,812
Outputs (Volumes)				
Precipitation Surplus (m³/yr)	282	647	325	1,254
Net Surplus (m³/yr)	282	647	325	1,254
Evapotranspiration (m³/yr)	315	162	81	558
Infiltration (m³/yr)	169	0	0	169
Surplus Infiltration (m³/yr)	0	0	0	0
Total Infiltration (m³/yr)	169	0	0	169
Run-Off Pervious Areas (m³/yr)	113	0	0	113
Run-Off Impervious Areas (m³/yr)	0	647	325	972
Total Run-Off (m³/yr)	113	647	325	1,085
Total Outputs (m³/yr)	597	809	406	1,812
Difference (Inputs - Outputs)	0	0	0	0

Table C: Post-Development (with mitigation)

Table C: Post-Developme	int (with mitigation	<u>')</u>		
Catchment Designation	Landscaped Grass	Paved Surface	Building	Total
Area (m ²)	658	892	448	1,998
Pervious Area (m ²)	658	0	0	658
Impervious Area (m²)	0	892	448	1,340
Infiltration Factors			<u> </u>	,
Topography Infiltration Factor	0.2	0	0	
Soil Infiltration Factor	0.3	0	0	
Land Cover Infiltration Factor	0.1	0	0	
Infiltration Factor	0.6	0	0	
Run-Off Coefficient	0.4	1	1	
Run-Off From Impervious Surfaces	0.8	0.8	0.8	
Inputs (Per Unit Area)	1 1			
Precipitation (mm/yr)	907	907	907	907
Rainfall (mm/yr) Run-On (mm/yr)	654 0	654 0	654 0	654 0
Other Inputs (mm/yr)	0	0	0	0
Total Inputs (mm/yr)	907	907	907	907
Outputs (Per Unit Area)	301	301	307	301
Precipitation Surplus (mm/yr)	428	726	726	628
Net Surplus (mm/yr)	428	726	726	628
Evapotranspiration (mm/yr)	479	181	181	279
Infiltration (mm/yr)	257	0	0	85
Surplus Infiltration (mm/yr)	0	0	784	176
Total Infiltration (mm/yr)	257	0	784	260
Run-Off Pervious Areas (mm/yr)	171	0	0	56
Run-Off Impervious Areas (mm/yr)	0	726	-58	311
Total Run-Off (mm/yr)	171	726	-58	367
Total Outputs (mm/yr)	907	907	907	907
Difference (Inputs - Outputs)	0	0	0	00
Inputs (Volumes)	1			
Precipitation (m³/yr)	597	809	406	1,812
Run-On (m ³ /yr)	0	0	0	0
Other Inputs (m³/yr)	0	0	0	0
Total Inputs (m ³ /yr)	597	809	406	1,812
Outputs (Volumes)				
Precipitation Surplus (m³/yr)	282	647	325	1,254
Net Surplus (m³/yr)	282	647	325	1,254
Evapotranspiration (m³/yr)	315	162	81	558
Infiltration (m³/yr)	169	0	0	169
Surplus Infiltration (m³/yr)	0	0	351	351
Total Infiltration (m³/yr)	169	0	351 351	520
` ','				
Run-Off Pervious Areas (m³/yr)	113	0	0	113
Run-Off Impervious Areas (m³/yr)	0	647	-26	621
Total Run-Off (m³/yr)	113	647	-26	734
Total Outputs (m ³ /yr)	597	809	406	1,812
Difference (Inputs - Outputs)	0	0	0	0

Table D: Water Balance Summary Table

Tubio B. Water Balance Callinary	Site							
Characteristic	Pre- Post- Change (Pre to Post) Development		Post-Development with Mitigation	Change (Pre to Post with Mitigation)				
Inputs (Volume)								
Precipitation (m ³ /yr)	1,812	1,812	0	0%	1,812	0	0%	
Run-On (m³/yr)	0	0	0	NA	0	0	NA	
Other Inputs (m ³ /yr)	0	0	0	NA	0	0	NA	
Total Inputs (m ³ /yr)	1,812	1,812	0	0%	1,812	0	0%	
			Outputs (Vo	lume)				
Precipitation Surplus (m ³ /yr)	855	1,254	399	47%	1,254	399	47%	
Net Surplus (m3/yr)	855	1,254	399	47%	1,254	399	47%	
Evapotranspiration (m³/yr)	957	558	-399	-42%	558	-399	-42%	
Infiltration (m ³ /yr)	545	169	-376	-69%	169	-376	-69%	
Rooftop Infiltration (m ³ /yr)	0	0	0	NA	351	351	NA	
Total Infiltration (m ³ /yr)	545	169	-376	-69%	520	-25	-5%	
Run-Off Pervious Areas (m³/yr)	310	113	-197	-64%	113	-197	-64%	
Run-Off Impervious Areas (m³/yr)	0	972	972	NA	621	621	NA	
Total Run-Off (m ³ /yr)	310	1,085	775	250%	734	424	137%	
Total Outputs (m ³ /yr)	1,812	1,812	0	0%	1,812	0	0%	



APPENDIX I

Guelph Permeameter Testing Results

Guelph Pereameter Infiltration Test Results

Investigator:	A Turner & J. Millington
Date:	20-Jul-23
Location:	181 Burton Ave. Barrie, ON
TP ID:	TP-1
Depth of Hole:	20 cm auger hole
Radius:	3 cm
Reserviors used during test:	Combined
(Combined or Inner)	
Reservior constant used:	35.22
Ground Surface Elevation:	231.5 masl

Water Level in Well: 10 cm

Time	Δt	Water level in	Δh	Rate of Change
t	(min)	Reservoir	(cm)	$\Delta h/\Delta t$
(min)		h (cm)	, ,	(cm/ min)
0		2.0		
0.25	0.25	2.7	0.7	2.80
0.5	0.25	3.5	0.8	3.20
0.75	0.25	4.4	0.9	3.60
1	0.25	5.1	0.7	2.80
1.5	0.5	6.5	1.4	2.80
2	0.5	7.9	1.4	2.80
2.5	0.5	9.1	1.2	2.40
3	0.5	10.2	1.1	2.20
3.5	0.5	11.5	1.3	2.60
4	0.5	12.6	1.1	2.20
4.5	0.5	13.7	1.1	2.20
5	0.5	14.7	1.0	2.00
	Ste	ady rate for 3 co	onsecutive readings $(\mathbf{R_1})$:	2.80

Water Level in Well: 10 cm

Time	Δt	Water level in	Δh	Rate of Change
t	(min)	Reservoir	(cm)	$\Delta h/\Delta t$
(min)		h (cm)		(cm/min)
0		0		
0.25	0.25	1.5	1.5	6.00
0.5	0.25	1.8	0.3	1.20
0.75	0.25	2.2	0.4	1.60
1	0.25	2.5	0.3	1.20
1.5	0.5	3.7	1.2	2.40
2	0.5	4.8	1.1	2.20
2.5	0.5	6.1	1.3	2.60
3	0.5	7.5	1.4	2.80
3.5	0.5	8.8	1.3	2.60
4	0.5	9.9	1.1	2.20
4.5	0.5	11.1	1.2	2.40
5	0.5	12	0.9	1.80
5.5	0.5	13	1.0	2.00
6	0.5	14	1.0	2.00
6.5	0.5	15.3	1.3	2.60
7	0.5	16.5	1.2	2.40
7.5	0.5	17.5	1.0	2.00
8	0.5	19	1.5	3.00
8.5	0.5	20.2	1.2	2.40
9	0.5	21.2	1.0	2.00
9.5	0.5	22.3	1.1	2.20
10	0.5	23.4	1.1	2.20
10.5	0.5	24.5	1.1	2.20
	Ste	ady rate for 3 co	onsecutive readings (R ₂):	2.20

SOLMOISTURE

SOLIMOISTURE Guelph Permeameter Calculations

Input

Support: ali@soilmoisture.com

 $\phi_m = \frac{1.17E-02}{(cm^2/min)}$

Result

Reservoir Type (enter "1" for Combined and "2" for Inner reservoir):

Enter water Head Height ("H" in cm):

Enter the Borehole Radius ("a" in cm):

3

Enter the soil texture-structure category (enter one of the below numbers):

- 1. Compacted, Structure-less, clayey or silty materials such as landfill caps and liners, lacustrine or marine sediments, etc.
- 2. Solls which are both fine textured (clayey or silty) and unstructured; may also include some fine sands.
- Most structured soils from clays through loams; also includes unstructured medium and fine sands. The category most frequently applicable for agricultural soils.
- 4. Coarse and gravely sands; may also include some highly structured soils with large and/or numerous cracks, macropors, etc

		Steady State Rate of Water Level Change ("R" in cm/min):	2.8000	
Res Type	35.22			
Н	10			
а	3	α*=	0.12	(cm ⁻¹)
H/a	3.333			
a*	0.12	€ =	1.287543	
C0.01	1.218	Q =	1.6436	
C0.04	1.29			
C0.12	1.288	$K_{fs} =$	1.78E-03	cm/sec
C0.36	1.288	<i>'-</i>	1.07E-01	cm/min
С	1.288		1.78E-05	m/sec
R	2.800		4.21E-02	inch/min
Q	1.644		7.01E-04	inch/sec
pi	3.142			
		Φ,,,, =	1.48E-02	(cm²/min)

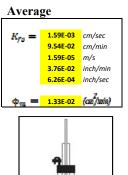
Head #2 Reservoir Type (enter "1" for Combined and "2" for Inner reservoir): Enter water Head Height ("H" in cm): Enter the Borehole Radius ("a" in cm): 3 Enter the soil texture-structure category (enter one of the below numbers): 3

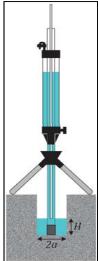
- 1. Compacted, Structure-less, clayey or silty materials such as landfill caps and liners, lacustrine or marine sediments, etc.
- Soils which are both fine textured (clayey or silty) and unstructured; may also include some fine sands.

pi 3.1415

- Most structured solls from clays through loams; also includes unstructured medium and fine sands. The category most frequently applicable for agricultural soils.
- 4. Coarse and gravely sands; may also include some highly structured soils with large and/or numerous cracks, macropors, et

	ils with large and/or numerous cracks, macropors, etc	tured so	struc
2.2000	Steady State Rate of Water Level Change ("R" in cm/min): 2.200		
		35.22	Res Type
		10	Н
0.12 (cm ⁻¹)	$\alpha^* = 0.12$	3	а
		3.333333	H/a
287543	C = 1.28756	0.12	a*
.2914	Q = 1.2914	1.21841	C0.01
		1.290234	C0.04
40E-03 cm/sec	$K_{fs} = 1.40E-0$	1.287543	C0.12
40E-02 cm/min	8.40E-0	1.287543	C0.36
40E-05 m/ses	1.40E-0	1.287543	С
31E-02 inch/min	3.31E-0	2.200	R
51E-04 inch/sec	5.51E-0	1.2914	Q







TEST PIT LOG 1

Environmental Assessments & Approvals

Project Name/ Project Client	Guelph Permeameter Testing - Hydrogeological Assessment Monolite Holdings Inc.	Project Address	181 Burton Avenue, Barrie, Ontario	Date	July 20, 2023
Test Pit Number	1	Contractor	Mark St. John	Elevation	231.50 masl
Equipment	Rubber Track Mini-Excavator	Test Pit Size	1.2x4.0 m	Datum	17T E 605210 N 4914039
Temperature	22 °C	Weather	Sunny, partly cloudy	Sample Type	Soil

De	pth			Sai	nples		
From (m)	To (m)	Soil description	N	No.	Depth (mbgs)	Screening Parameters	Remarks / Chemical Analysis
0.00	0.22	TOPSOIL: Dark brown to black, sand, trace to some silt, some gravel, organics, moist					
0.22	1.10	FILL: Dark brown to black, sand, trace to some silt, some gravel to gravelly, organics, moist					
1.10	1.60	SAND: Compact to dense, brown, sand, trace to some silt, trace to some gravel, moist		1	1.3		Submitted for T-Time and grain size analysis
							Guelph Permeameter Test #1 completed at north side of test pit, Test #2 completed at south side of test pit. Both tests completed at 1.3 m depth
		Test Pit Terminated at1.6 m					
	Comments		W	Water Conditions in Test Pit			
	No water seepage No sidewall sloughing				mpletion mpletion		
					J	OB No.	21-492

JOB No.	21-492
TEST PIT No.	1
FIELD STAFF	Alan Turner



July 31, 2023

Azimuth Environmental Consulting Inc. 642 Welham Road
Barrie, Ontario
L4N 9A1

Attn: Alan Turner

RE: Job No. 21-492

Determination of Estimated T-Time

Dear Mr. Turner

GEI Consultants (GEI) was provided with one (1) soil sample on July 20, 2023 to complete a grain size analysis to determine the percolation rate of the tested soil (T-Time analysis).

The delivered sample was identified as shown below.

TP1 GS1, 1.3 m

A grain size distribution curve was developed by testing the above referenced soil sample in accordance with ASTM Standard Test Methods for Particle-Size Distribution D6913 (Gradation) of Soils Using Sieve Analysis and ASTM D7928 (Gradation) of Fine-Grained Soils using the Sedimentation (Hydrometer) Analysis. The result of the laboratory test and graphical representation of the grain size analysis is enclosed.

Determination of percolation rate is based on the "Ministry of Municipal Affairs and Housing (MMAH) Supplementary Guidelines SB-6, Percolation Time and Soil Descriptions, September 14, 2012". Based on this document, a summary of the result and the estimated percolation rate of the soil is as follows:

Client Ref.	GEI Lab No.	Soil Description (MIT)	USCS Soil Classification	Estimated Percolation Rate or "T-Time" (mins/cm)	Estimated Infiltration Rate (mm/hr)
TP1 GS1, 1.3 m	5932	SILTY SAND, Some Clay, Trace Gravel	S.M.	30 mins/cm	20 mm/hour



It is noted that the typical range for an S.M. classified soil is typically on the order 8 to 20 mins/cm. Due to the extremely well graded nature of the soil samples, and that soils such as these (glacial tills) are typically hard or very dense, it is recommended that 30 mins/cm be used for instead for TP1 GS1, 1.3 m as a more realistic and conservative estimate.

It is noted that percolation time not only varies based on the grain size distribution but is also influenced by other soil characteristics such as the density of the soil, the structure of the soil, the percentage/mineralogy of clay, the plasticity of the soil, the organic content of the soil, and the groundwater table level which are not expressly calculated as part of a grain size analysis.

No field investigation was conducted by GEI in conjunction with the above testing and did not witness the depth or location in which these samples were obtained. GEI is providing the percolation rates as factual information, to be used in design by a qualified professional with due regard to the limitations as indicated above.

We trust this information is sufficient for your present purposes. Should you have any questions concerning the above, or can be of any further assistance, please do not hesitate to contact the undersigned.

Yours truly,

GEI Consultants

Donna Davidson-Gorry Laboratory Testing Services Practice Lead

(705) 718-6604

ddavidsongorry@geiconsultants.com

Andrew Jones

Materials Testing and Inspection Practice Lead

(705) 220-0060

ajones@geiconsultants.com

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Enclosures (1)

Grain Size Analysis (T-Time)



ENCLOSURE 1

Grain Size Analysis (T-Time)

