

**HYDROGEOLOGICAL INVESTIGATION REPORT
PROPOSED RESIDENTIAL DEVELOPMENT
79 COLLIER STREET, BARRIE, ONTARIO**

Prepared for:

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1.0. INTRODUCTION AND BACKGROUND

Sirati & Partners Consultants Ltd. (SIRATI) was retained by Vitmont Holdings (Barrie) Inc. c/o Marydel Homes (“the Client”) to conduct a Hydrogeological Investigation at the property identified as 79 Collier Street, Barrie, Ontario (the Property or the Site). The location of the Property is shown in Figure 1-1.

We understand that prior to December 2019, the municipal address for the Site was 36 Mulcaster Street, Barrie, Ontario. According to a City of Barrie memo dated December 11, 2019, the municipal address 79 Collier Street was assigned to the Site.

We also understand that the Site is an L-shaped property with an approximate area of 1,600 m² (0.16 hectares) located at the southwest corner of the intersection of Mulcaster Street and Collier Street in Downtown Barrie. It is bounded by Collier Street to the north, by Mulcaster Street to the east, by a retaining wall and a laneway to the south, followed by multiple commercial buildings, and by commercial property to the west. To the southeast of the Site is an armory building currently in operation as the Grey & Simcoe Foresters Regimental Museum.

It is understood that the Client intends to develop the Property with a fifteen-storey apartment complex with added commercial spaces.

The hydrogeological study was undertaken to ascertain the soil and groundwater conditions of the Site, assess any impacts on the surrounding natural environment due to the proposed development and provide recommendations or mitigative measures.

2.0. SCOPE OF WORK

This hydrogeological investigation assessment was carried out with the following tasks:

- **Review of available background information:** a review of available geological and hydrogeological information for the site and surrounding areas and the investigation reports completed for the Site was conducted to provide background information to allow for characterization of the Site’s soil and groundwater conditions.
- **Detailed site inspection:** an inspection of the Site was completed to review existing site conditions including identification of any hydrogeological features such as significant areas of potential groundwater recharge or areas of groundwater discharge.
- **Measurement of groundwater levels:** groundwater levels were measured in the existing monitoring wells to establish and/or confirm the general groundwater flow condition.

- **Water Balance (Preliminary):** a preliminary water balance study was completed for the proposed development using the Thornthwaite approach and the climatic data obtained from Environment Canada.
- **Dewatering Assessment:** an assessment of the short-term and long-term dewatering was conducted for the construction of the proposed residential building with one level of underground parking. The assessment also evaluated the need for Permit to Take Water (PTTW) or Environmental Activity and Sector Registry (EASR) registration.
- **Report Preparation:** a hydrogeological report was prepared presenting the results, findings, and recommendations of this investigation.

It should be noted that a Phase Two Environmental Site Assessment (ESA) was concurrently conducted by SIRATI at the Site. In addition, environmental site assessments and geotechnical investigations were completed previously at the Site by other consultants.

The data or information obtained in the current and former investigations has been incorporated into this hydrogeological investigation report.

3.0. PAST INVESTIGATIONS

- 1) V.A. Wood Associates Ltd. (V.A. Wood) completed a geotechnical assessment at the Site in 2016. A report entitled “*Geotechnical Investigation, Proposed Condominium, 36 Mulcaster Street, Barrie, Ontario,*” dated April 2016 was prepared for Edgecon Inc. by V.A. Wood. (Ref. No. 6862-16-02). The extracted data including borehole locations and borehole logs are presented in Appendix A1.

During geotechnical investigation, a total of six (6) boreholes (with no monitoring well installation) were completed across the Site. The boreholes were advanced to the depths ranging from 3.5 m below ground surface (mbgs) to 15.7 mbgs. The boreholes encountered a pavement 300 mm to 400 mm thick, followed by 1 m to 3.7 m of loose to compact gravelly sand fill, then generally competent native deposits of sand, gravelly sand till. The groundwater table is considered to be at least 5.5 mbgs. Soil samples taken from fill materials were submitted for analysis of polyaromatic hydrocarbons (PAHs), petroleum hydrocarbons (PHCs), and metals. The analytical results were summarized in a letter report “*Ref. No. 6862-16-02, Soil Analytical Testing, 36 Mulcaster Street, Barrie, Ontario,*” dated April 8, 2016. The test results show that some of the samples have concentrations of PAHs, some metals, sodium adsorption ratio (SAR) and electrical conductivity (EC) exceeding the Ministry of Environment, Conservation and

Parks (MECP) Site Condition Standards (SCS).

- 2) PGL Environmental Consultants (PGL) conducted a Phase II ESA at the Site in 2019, which was based on the findings of a Phase I ESA completed in February 2015 by Spice Environmental Inc. (Spice). A report entitled *“Phase II Environmental Site Assessment, 36 Mulcaster Street, Barrie, Ontario,”* dated June 2019 was prepared for Grant Thornton Limited by PGL. The extracted data including the borehole locations and borehole logs are presented in Appendix A2.

The Spice’s Phase I ESA identified onsite risks of environmental contamination due to the importation of up to 2,500 m³ fill of unknown quality and the remains of a drill shed which was destroyed by fire in 1885.

The 2019 Phase II ESA findings are described below:

- Six (6) boreholes (BH101 to BH104 and BH201 and BH202) were advanced at the Site, to the depths ranging from 6.1 mbgs to 13.7 mbgs. Five (5) boreholes were completed as monitoring wells (identified as BH101M, BH102M, BH103M, BH201M and BH201M). However, monitoring wells BH101M, BH102M, BH103M were found to be dry.
- Fill material was present at depths ranging from 2 mbgs to 5mbgs in the boreholes across the Site. Staining and extraneous materials such as bricks, debris, and charcoal were observed in the fill.
- Soil samples were collected and analyzed for petroleum hydrocarbons Fractions 1 to 4 (PHC F1-F4), benzene, toluene, ethylbenzene and xylenes (BTEX), polycyclic aromatic hydrocarbons (PAHs) and metals.
- Groundwater was encountered at roughly 8.7 mbgs. Two (2) groundwater samples were collected and tested for PAHs and metals.
- Soil and groundwater results were compared to Ontario Regulation 153/04 Table 2 Site Condition Standards (SCS) for industrial/commercial/community land use and a coarse-textured soil. They were also compared against the Table 2 residential/parkland/institutional SCS in the event the Site is redeveloped for residential purposes.
- Impacts of PAHs and metals were identified in the fill material on the west side of the Site. The groundwater results met the applicable Table 2 SCS for both industrial/commercial/community and residential/parkland/ institutional land uses.
- The 2019 Phase II ESA recommended that impacted fill be addressed through remediation and/or a Risk Assessment during redevelopment of the Site.

It should be noted that the previous Phase II ESA was carried out for due diligence purpose for prior to divestment of the Site. A Phase One ESA, followed by a Phase Two ESA was recently conducted by SIRATI in support of the proposed development. The preliminary results indicate that exceedances of the MECP Table 2 Standards were found in some soil and groundwater samples for one or more parameters including PAHs, metals, PHCs and VOCs.

4.0. LAND USE

The Site is located at the southwest corner of the intersection of Mulcaster Street and Collier Street, in a built up mixed residential and commercial area, in Barrie.

The Site is relatively flat with a gentle slope from north to south. To the southeast corner of the Site is an existing heritage structure currently in operation as the Grey & Simcoe Foresters Regimental Museum.

5.0. SITE DEVELOPMENT PLAN

The Property covering an area of about 0.40 acres (0.16 ha) was proposed to be developed as a step-like structure consisting of a 15-storey bulging in the north, a 14-storey structure in the center and a 13-storey building in the south, with a total of 127 residential units and equal number of parking spaces. Parking is being provided at one level underground parking and three (3) levels of above ground parking. Commercial spaces are being provided in the eastern half of the Site.

The site development plan with the outlay of the building is shown in Figure 5-1.

Figure 5-2 shows the building sectional plan provided by the Client, which indicates the finished floor (FF) grade elevation at 234.38 m above mean sea level (mAMSL).

6.0. ENVIRONMENTAL FEATURES

To assess environmental features, the databases maintained by the Ministry of Natural Resources and Forestry (MNRF), the Ministry of Environment, Conservation and Parks (MECP), and the Lake Simcoe and the Region Conservation Authority (LSRCA) were reviewed.

Based on the data reviewed, the Site is situated within the Barrie Creeks subwatershed, as shown on Figure 6-1, under the jurisdiction of the Lake Simcoe and Couchiching Black Source Protection Area. No creeks or waterbodies are present at the Site.

As per MNRF Natural Heritage System database, the Site is not located in any significant natural areas or areas of natural and scientific interests (ANSIs) (Figure 6-2).

As shown on the MECP Sourcewater Protection Atlas map (Figure 6-3), the Site is located within a drinking water vulnerable area (wellhead protection area, WHPA-B, and Issue Contributing Area).

The Site is not located in any LSRCA regulation areas, as shown in Figure 6-4.

7.0. PHYSICAL SETTING

7.1 Topography and Drainage

The Site is located within the Barrie subwatershed of the Lake Simcoe watershed area. As shown in Figure 6-1, the Barrie subwatershed consists of Barrie Creeks, Lovers Creek and Hewitt's Creek. The Site falls within the Barrie Creeks subwatershed. Barrie Creeks subwatershed is roughly 37.5 km² in area and includes six (6) major creeks and all these creeks drain separately into Kempenfelt Bay of the Lake Simcoe.

Figure 7-1 presents the topography survey map prepared by C.A. MacDonald Surveying Inc., dated June 9, 2015. It indicates that the Site slopes generally to the south, with the elevations ranging from approximately 234.6 mAMSL in the north/northeast to about 230.4 mAMSL at the southwest corner. The nearest water body is Kempenfelt Bay of the Lake Simcoe, with the nearest point located about 160 m southeast of the Site.

7.2 Physiography

According to Chapman and Putnam (1984), three (3) physiographic regions are found within the subwatershed: the Simcoe Uplands, the Simcoe Lowlands, and the Peterborough Drumlin Field. As shown in Figure 7-2, the Site is located in the Sand Plain area in the Simcoe Lowlands physiographic region. The region is described as having lower elevations, with flat-floored valley features that generally correspond to current river systems (Sharpe *et al.*, 1999). The lowlands were flooded by glacial Lake Algonquin, and as a result, are floored by sand, silt and clay (Chapman and Putnam, 1984).

7.3 Overburden Geology

The surficial geology at the Site, was described as foreshore-basinal deposits consisting mainly of sand and silt with varying amounts of gravel, with high infiltration rates (Figure 7-3). In general, the thickness ranges from approximately 83 m to 191 m.

The Paleozoic bedrock topography appears to strongly influence the overlying Quaternary sediment thickness and distribution. The thicker Quaternary sediments occur in bedrock topographical lows (i.e. within bedrock valleys), while the thinnest areas of Quaternary deposits occur along the shoreline of Kempenfelt Bay.

7.4 Bedrock Geology

The bedrock can be characterized as being from the Paleozoic Era, consisting primarily of limestone of the Middle Ordovician Simcoe Group (Figure 7-4). The Simcoe Group consists of four formations that dip gently towards the southwest: Gull River Formation, Bobcaygeon Formation, Verulam Formation and the Lindsay Formation from oldest to youngest. However, only the Verulam and Lindsay Formations are found within these subwatersheds.

Verulam Formation occurs along the shoreline of Kempenfelt Bay and expands west of the City of Barrie and ranges in thickness from 32 m to 65 m and consists of fossiliferous limestone with inter-beds of calcareous shale.

8.0. HYDROGEOLOGY

Water well records on file with the Ministry of the Environment, Conservation and Parks (MECP) serve as a database for this hydrogeological assessment. The well locations were provided from the MECP interactive water well record database. According to the well records, there appears to be 79 wells within a 500 m radius around the property. The locations of the recorded water wells are shown in Figure 8-1.

Five (5) water wells (#5700235 for municipal, #5700236 and #5700262 for industrial, #5718640 for cooling/AC and #5719264 for public) were found for water supply use, and the others were recorded as test holes, observation wells, abandoned wells or with no detailed information.

Based on the details in the well records, a thick layer of overburden materials seems to be present in the study area. Bedrock was not encountered at the maximum explored depth of about 98 mbgs in a test hole identified as #5700288. The groundwater levels recorded in water supply wells and deep test holes ranged from 3 m above ground surface (artesian flowing water) to about 8.4 mbgs.

9.0. BOREHOLE DRILLING AND MONITORING WELL INSTALLATION

Concurrently with the Phase Two ESA, a total of five (5) boreholes (BH1 to BH5) were advanced at the Site, of which two (2) monitoring wells identified as BH/MW2 and BH/MW3 were completed with installation of monitoring wells.

As mentioned earlier, five (5) monitoring wells were installed at the Site in the previous investigations. However, during the site visit, only two (2) monitoring wells (BH201M and BH202M) were found existing at the Site.

Figure 9-1 depicts the locations of boreholes and monitoring wells completed by SIRATI, along with the monitoring wells completed previously by other consultant. The observed soil stratigraphy and the details of monitoring well construction are presented in Borehole Logs included in Appendix A1, A2 and A3.

9.1 Soil Stratigraphy

The soil stratigraphy as revealed from the advanced boreholes by SIRATI, generally consisted of topsoil/asphalt overlying the fill materials, underlain by cohesionless soils, predominantly composed of sand. No bedrock was encountered at the maximum explored depth of 15.7 mbgs (by V.A.Wood).

Following is the generalized stratigraphy at the Site, as depicted in the boreholes.

Topsoil

A layer of topsoil with a maximum thickness of 0.15 m was found at the surface of borehole number 1.

Asphalt

A layer of asphalt was found at the surface of all the boreholes, except MW1, with a maximum thickness of about 0.1 m.

Fill

Fill material consisting of sand, some stone, trace silt, clay with pieces of brick was found to a maximum depth of 2.3 mbgs at BH2.

Sand

A layer of sand with trace gravel with some silt was encountered from about 2.3 mbgs to the explored depth of 13.7 mbgs. This layer was moist to wet, white to dark grey in color.

The cross-section profiles A-A' and B-B' as shown in Figures 9-2 and 9-3, respectively, present the general soil stratigraphy of the Site. As can be seen from the cross-section, a layer of sand deposits exists below the fill materials across the entire Site.

A representative soil sample taken from BH/MW2 was selected for grain size analysis. The result is provided in Appendix B, which indicated the tested soil as silty fine sand.

9.2 Groundwater Levels

Groundwater levels were measured on July 16, and July 27, 2020 in two (2) new monitoring wells (BH/MW2 and BH/MW3) installed by SIRATI and two (2) existing monitoring wells (BH201M and BH202M) previously installed by PGL. The recorded groundwater levels are presented in Table 9-1 below.

Table 9-1: Well Construction Details and Measured Groundwater Levels

Monitoring Well	Ground Elevation (mAMSL)	Well Depth (mbgs)	Screen Depth (mbgs)	Screened Soil Type	June 3, 2019		July 16, 2020		July 27, 2020	
					Depth to Ground water (mbgs)	Ground water Elevation (mAMSL)	Depth to Ground water (mbgs)	Ground water Elevation (mAMSL)	Depth to Ground water (mbgs)	Ground water Elevation (mAMSL)
BH/MW 2	231.75	10.70	7.7 ~ 10.7	Sand	-	-	9.48	222.27	9.51	222.24
BH/MW 3	232.10	12.20	9.2 ~ 12.2	Sand	-	-	9.88	222.22	9.82	222.28
BH201M	230.80	13.70	10.7 ~ 13.7	Sand	8.7	222.10	8.80	222.00	8.87	221.93
BH202M	231.05	13.70	10.7 ~ 13.7	Sand	8.7	222.35	8.81	222.24	8.89	222.16

Notes: mAMSL - metres above mean sea level; mbgs - metres below ground surface

As presented above, the latest measured groundwater levels ranged in depth from 8.87 mbgs to 9.82 mbgs, and the elevations ranged from 221.93 mAMSL to 222.28 mAMSL, with an average groundwater elevation of 222.15 mAMSL.

9.3 Groundwater Flow Direction and Hydraulic Gradients

Based on the groundwater elevation data obtained from the latest monitoring event, a site-specific groundwater elevation contour map was prepared to present the inferred the groundwater flow direction. As shown in Figure 9-4, the groundwater flow direction was inferred to be southwards, generally following the local surface drainage.

The hydraulic gradient is a gradient or slope between two or more hydraulic head measurements over the length of the flow path. The hydraulic gradients help determine the groundwater flux or discharge. Groundwater will flow down the hydraulic gradient. Based on the groundwater elevation data for the shallow monitoring wells, horizontal hydraulic gradient was calculated to be approximately 0.004 m/m (Table 9-2).

Table 9-2: Horizontal Hydraulic Gradients – 79 Collier Street, Barrie, Ontario

Monitoring Well	Groundwater Elevation (mAMSL)		Distance Between Monitors (m)	Gradient (m/m)
BH/MW2 to BH/MW3	222.24	222.28	27	0.001
BH/MW2 to BH202M	222.24	222.16	16	0.005
BH/MW3 to BH202M	222.28	222.16	20	0.006
			Average	0.004

9.4 Estimated Hydraulic Conductivity

The native soils present at the Site are predominantly sandy soils. Based on the result of grain size analysis of one representative soil sample, the hydraulic conductivity was estimated using empirical Hazen equation, and was estimated to be 4.3×10^{-6} m/s.

It should be noted that the theoretical hydraulic conductivity (K-value) of the sandy soils may range from 1.0×10^{-5} m/s to 1.0×10^{-6} m/s.

10.0. CONSTRUCTION DEWATERING REQUIREMENTS

Construction dewatering is intended to lower the groundwater levels in the excavation area in order to ensure a dry working condition.

The requirements for construction dewatering generally depend on the site's soil and groundwater conditions including soil type, soil permeability or hydraulic conductivity, local groundwater levels, and the design of the proposed development such as the foundation and/or basement elevation, as well as the size of proposed structure, etc.

10.1 Proposed Development and Anticipated Excavation

As mentioned earlier, the Property covering an area of about 1,660 m² (0.16 hectares) was proposed to be developed into a 15-storey residential apartment building with part of commercial use, accommodate 127 dwelling units. The proposed building will consist of one level underground parking and three (3) levels of above ground parking. Commercial spaces are being provided in the eastern half of the building.

Based building sectional plan (Figure 5-2) made available by the Client, the finished main floor elevation is at 234.38 mAMSL, the underground level elevation is at 231.38 mAMSL and the lower loading level elevation, which appears to be similar to footing elevation, is at 227.68 mAMSL,

For construction of the footing/foundation and loading level, the excavation may extend to the elevation of 227. 23 mAMSL (227.68 minus 0.45 m below the loading level or footing for the placement of granular materials and construction of concrete slab).

Based on the soil stratigraphy revealed at the Site, the excavation will cut through the fill material and into the sandy soil.

10.2 Dewatering Requirements

As discussed, the excavation may extend to the elevation of 227. 23 mAMSL. Based on the groundwater monitoring completed at the monitoring wells (MW2, MW3, BH201M and BH202M), the measured

groundwater elevations ranged from 221.93 mAMSL to 222.28 mAMSL, which are well below the final excavation elevation of 227.23 mAMSL for the footing as well as lower loading level. Therefore, groundwater control will not be required for the proposed development either for temporary construction dewatering or for long-term drainage discharge. Therefore, PTTW or EASR registration are not required.

11.0. ASSESSMENT OF POTENTIAL IMPACTS

As discussed, there is no construction dewatering, either short-term or long-term due to the prevailing deep-water table conditions. The potential impacts due to the Site development were assessed as follows.

11.1 Natural Features

As discussed, no natural features including a wetland, a pond or a creek are located on the Site. The nearest water body is located at about 160 m southeast of the Site and therefore, there should be no impact on the local natural features, due to the site development.

11.2 Water Supply Wells near the Site

Given that no dewatering will be required for completion of the proposed development, impacts on the local water wells (private or public) will not be anticipated to be associated with the dewatering activity, although the Site is located within the Barrie Water Supply Wells # 11, 12 and 14 combined wellhead protection area.

11.3 Considerations on Drinking Water Vulnerability

Based on the MECP Source Protection Information Atlas, the Site is located within the Lakes Simcoe and Couchiching/Blake River Source Protection Area (Figure 6-3), and vulnerable areas are identified to be associated with at the site development.

It is understood that the following South Georgian Bay Lake Simcoe Source Protection Plan policies apply to the proposed development: RLU-1, DNAPL-1, Salt (ICA)-2, LUP-2.

11.3.1 Well Head Protection Area

The proposed development lies within the 2- year Time of Travel (TOT) capture zone, i.e. Well Head Protection Area, WHPA-B (Figure 6-3), which is related to the Barrie Water Supply Wells #11, 12 and 14. Time of travel is important because it is an indication of how quickly a contaminant can move from a WHPA into a municipal well.

Use and/or storage of chemicals on Site may result in contamination in soil and/or groundwater due to inadvertent release on the Property, and potentially would result in contamination in the source of groundwater for the municipal wells.

Policies: RLU-1, DNAPL-1, and Salt(ICA)-2 should be considered to be applied during the design and construction of the proposed development, which restrict storage and handling of road salt, snow, fuels, dense nonaqueous phase liquid (DNAPL) and/or organic solvent on Site.

11.3.2 Issue Contributing Area – Chloride and Sodium

The Site is located in an issue contributing area for chloride and sodium, associated with water supply Well# 11, 12 and 14. As such, the Site is susceptible to contamination in soil and groundwater due to chloride and sodium. Therefore, storage and/or application of de-icing salt material would pose a potential impact at the Site, because chloride and sodium are typical components of de-icing salt.

Policies: RLU-1 and Salt (ICA)-2 should be considered to be applied during the design and construction of the proposed development.

11.3.3 Significant Groundwater Recharge Area

The Site is located in a Significant Groundwater Recharge Area with a vulnerable score of 6. Significant Groundwater Recharge Areas are areas on the landscape that are characterized by porous soils, such as sand or gravel, which allows water to seep easily into the ground and flow to an aquifer. A recharge area is considered significant when it helps maintain the water level in an aquifer that supplies a community or private residence with drinking water.

Given that the Site is located in an urbanized area, the Site and its neighbouring properties would be relying on the City's water supply. The proposed development may reduce the pervious area at the Site, which result in decreased infiltration into subsurface or decrease in groundwater recharge.

However, considering that the municipal water wells are usually constructed in deep aquifers and no dewatering is required, the impact on the groundwater recharge may not be considered.

11.3.4 Highly Vulnerable Aquifer

The Site is located in a Highly Vulnerable Aquifer area with a vulnerable score of 6. An aquifer is an area underground that is highly saturated with water – enough water that it can be withdrawn for human use. A Highly Vulnerable Aquifer is one that is particularly susceptible to contamination because of its location near the ground's surface or where the types of materials in the ground around it are highly permeable.

Based on the site condition, the shallow groundwater at the Site is susceptible to contamination. Considerations should be taken into as in Section 11.3.1 and 11.3.2.

11.3.5 Wellhead Protection Area – Q (Water Quantity)

The Site is identified to be an area of a Wellhead Protection Area – Q (Water Quantity), with low stress level. Any WHPA-Q areas where significant or moderate drinking water stress has been identified is an area where significant drinking water quantity threat activities can occur. Within these areas, future activities which take water without returning it to the same source or which reduce recharge to the aquifer are significant water quantity threats.

As discussed, no dewatering is required for the proposed development. Therefore, no concerns on Wellhead Protection Area – Q (Water Quantity) would be considered due to the proposed development.

12.0. WATER BALANCE

A preliminary water balance for the Site was calculated for both pre-development and post-development conditions in order to assess the change in overall rate of infiltration.

12.1 Site Condition

The Site is currently occupied by a parking lot, a landscaped area with trees and a private drive lane. There are no creeks, ponds or wetlands located on the Subject Property.

It is understood that a residential development has been proposed consisting of construction of a 15-storey residential building with one (1) level of underground level and 3-levels of above ground parking.

Based on the design information, the development area at the Site can be generally categorized into three (3) types as paved area, roof area, and landscape area as shown in Figures 12-1 and 12-2. A summary of the surface areas of the development is listed in Table 12-1.

Table 12-1: Pre-and Post-Development Site Conditions

Type of Land Coverage	Pre-Development Area (m ²)	Post- Development Area (m ²)
Paved Area	1260	558
Building Roof Area	0	1102
Landscape/Vegetated Area	400	0
Total (m²)	1660	1660

12.2 Site Level Water Balance

Based on the Thornthwaite and Mather methodology (1957), the water balance is an accounting of water in the hydrologic cycle. Precipitation (P) falls as rain and snow. It can run off towards lakes and streams (R), infiltrate to the groundwater table (I), or evaporate from ground or evapotranspiration by vegetation (ET). When long-term average values of P, R, I, and ET are used, there is minimal or no net change to groundwater storage (ΔS).

The annual water budget can be expressed as:

$$P = ET + R + I + \Delta S$$

Where:

P = Precipitation (mm/year)

ET = Evapotranspiration (mm/year)

R = Run-off (mm/year)

I = Infiltration (mm/year)

ΔS = Change in groundwater storage (taken as zero) (mm/year)

12.3 Climatic Data

The climatic data including monthly average temperature and precipitation were obtained from Environment Canada, for Shanty Bay weather station (Climate Identifier: 6117684) located at about 4 km distance from the Site.

The data were available between the years 1973 to 2006 i.e. 33 years. Temporal variations of mean annual temperature and precipitation are shown in Figures 12-3 and 12-4.

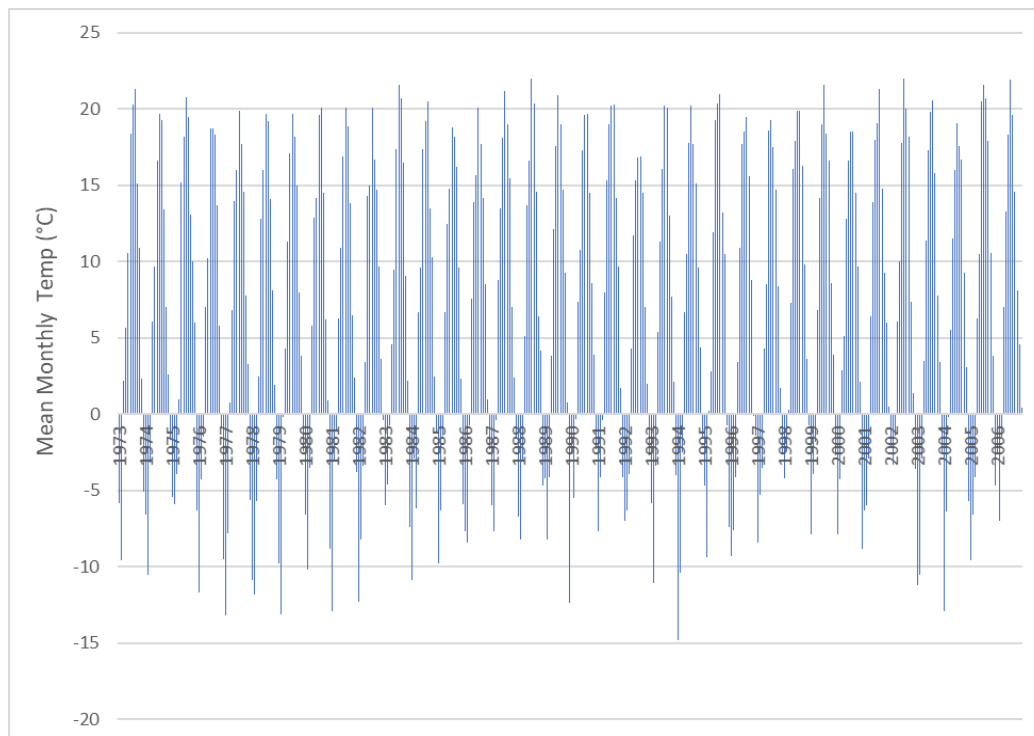


Figure 12-3: Mean Annual Temperature at the Site

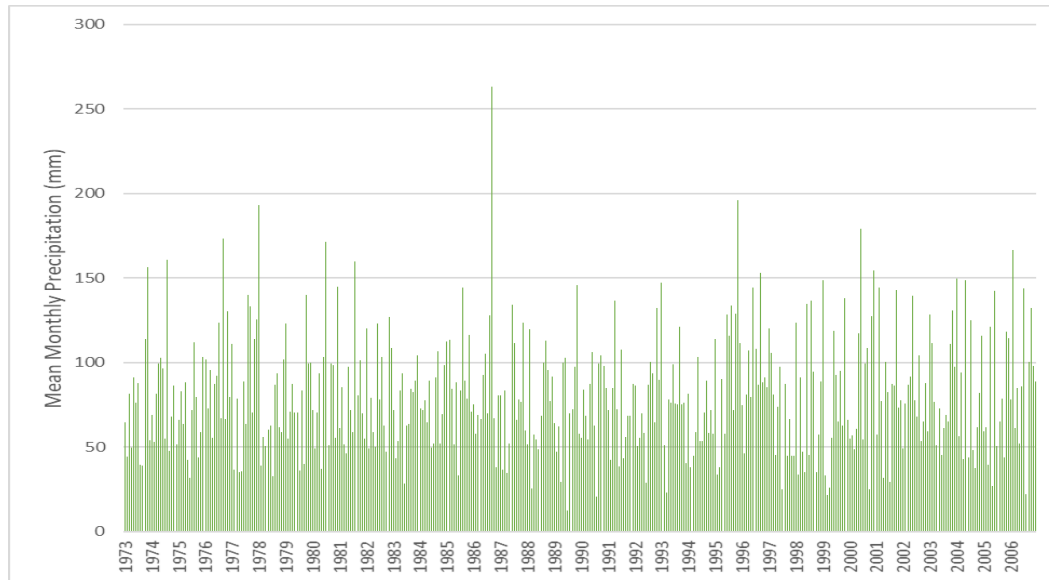


Figure 12-4: Mean Annual Precipitation at the Site

Average monthly variations of both temperature and precipitation were calculated for the period from 1973 to 2006 (33 years) and is presented below in Figure 12-5. The highest average temperature was recorded in the month of August, while the highest precipitation was in the month of November.

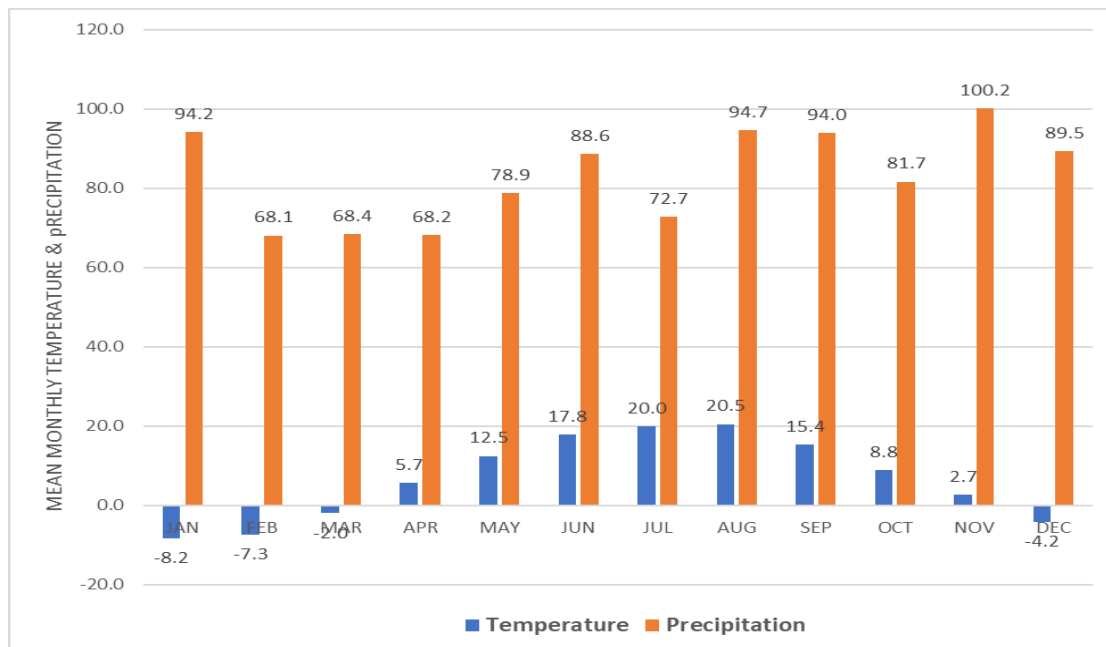


Figure 12-5: Mean Monthly Average Temperature and Precipitation at the Site

Based on the data for the precipitation and temperature, actual evapotranspiration was estimated to be about 531 mm/annum using the USGS Thornthwaite Monthly Water Balance software (Appendix E), and the average annual precipitation was recorded to be 999 mm/annum.

12.4 Infiltration and Runoff

As mentioned above, the actual evapotranspiration was estimated to be 531 mm/annum. Given the average annual precipitation of 999 mm/annum, there is a water surplus of 468 (=999-531) mm/annum occurring at the Site, which can either infiltrate into subsurface or go as run-off.

The rate of infiltration at a site is expected to vary, based on a number of factors to be considered in any infiltration model. To partition the available water surpluses into infiltration and surface run-off, the Ministry of Environment, Conservation and Parks (MECP) infiltration factor was used. The MECP Storm Water Management Planning and Design Manual (2003) methodology for calculating total infiltration based on topography, soil type and land cover was used, and a corresponding run-off component was calculated for the soil moisture storage conditions.

The calculation of infiltration and runoff in the stages of pre-development and post-development is provided in Appendix D, and are presented in Tables 12-2 to 12-5, below.

Table 12-2: Annual Pre-Development Water Balance

Land Use		Area (m ²)	Precipitation (m ³)	Evapotranspiration (m ³)	Infiltration (m ³)	Run-off (m ³)
Impervious Areas	Paved Area	1260	1259	126	0	1133
	Roof Area	0	0	0	0	0
Pervious Areas	Landscape Area	400	400	212	140	47
		1,660	1,658	338	140	1,180
Assuming no infiltration occurring in paved and roof areas, and 10% of precipitation to be evaporated from paved and roof areas.						

Table 12-3: Annual Post-Development Water Balance

Land Use		Area (m ²)	Precipitation (m ³)	Evapotranspiration (m ³)	Infiltration (m ³)	Run-off (m ³)
Impervious Areas	Paved Area	558	557	56	0	502
	Roof Area	1102	1,101	110	0	991
Pervious Areas	Landscape Area	0	0	0	0	0
		1,660	1,658	166	0	1,493
Assuming no infiltration occurring in paved and roof areas, 10% of precipitation to be evaporated from paved and general roof areas.						

Table 12-4: Comparison of Pre- and Post Development Water Balance Components

	Precipitation (m³)	Evapotranspiration (m³)	Infiltration (m³)	Run-off (m³)
Pre-Development	1,658	338	140	1,180
Post-Development	1,658	166	0	1,493
Change in Volume		-172	-140	313
Change in %			-100	27

Table 12-5: Requirement for Infiltration of Roof Run-off

Volume of Pre-Development Infiltration (m ³ /annum)	140
Volume of Post-Development Infiltration (m ³ /annum)	0
Deficit from Pre to Post Development Infiltration (m ³ /annum)	140
Percentage of Roof Runoff required to match the pre-development infiltration (%)	14

12.5 Summary of Water Balance Calculation

Based on the above calculations, a summary of water balance could be provided as below:

- 1) There is a net increase in run-off at the Site of about 313 m³/annum, from 1,180 m³/annum to 1,493 m³/annum. This increase is a result of the development of the Site with more impervious areas such as roof and paved areas, and reduction in pervious areas.
- 2) Without implementation of mitigation measures, there is a net deficit of about 140 m³ /annum (or 100% decrease) in the post-development infiltration on a yearly basis.
- 3) There is a volume of 991 m³/annum collected from the general roof area, which can be used for the enhanced infiltration for the purpose of implementing the Low Impact Development (LID) measures, if applicable. Based on the estimation, diversion of 14% of the general roof water for infiltration would maintain a balanced infiltration after the development.

12.6 Discussions on LID Measures

It is known that low impact development (LID) practices have received increasing attention as these strategies attempt to capture the runoff and mimic the natural hydrologic cycle.

The City of Barrie has introduced an Infiltration LID Screening Process to guide the selection and implementation of LID measures.

In general, there are two primary categories of LIDs. The first promotes the infiltration of stormwater close to the source. These infiltration type LIDs are preferred when hydrogeological and physical

conditions are optimal and allow for their emplacement. The second captures and slowly releases the water to the surface water system through the process of storage and filtration. Storage and filtration type LIDs are to be considered when conditions do not permit infiltration LIDs to be implemented. As it is discussed, the Site is located in an area categorized as WHPA-B and Issue Contributing Area – Chloride and Sodium. According to the LID Screening Process, water source from the paved area (driveway and/or walkway) is not permitted for use of infiltration, based LID practices. In other words, the LID measures such as permeable pavers or other open infiltration facility may not be allowed.

Given the proposed design, there is little or no space available for the implementation of LID measures. However, as SIRATI is not providing any design of LID facilities, it would be beneficial to consult with design engineers for the LID design recommendations.

13.0. CONCLUSIONS AND RECOMMENDATIONS

This report was prepared by SIRATI in support of a proposed mix-use residential/commercial development at the Site located at 79 Collier Street, Barrie, Ontario. Based on the hydrogeological investigation conducted on the Property, the following conclusions and recommendations are presented:

- The Site is located within the Barrie Creeks subwatershed of Simcoe Watershed within the Lakes Simcoe and Couchiching/Black River Source Protection Area. No creeks or waterbodies are present at the Site.
- Topographically, the Site slopes generally to the south, with the elevations ranging from approximately 234.6 mAMSL in the north/northeast to about 230.4 mAMSL at the southwest corner. The nearest water body is Kempenfelt Bay of Lake Simcoe, which is located about 160 m southeast of the Site.
- The Site is located in the Sand Plain area in the Simcoe Lowlands physiographic region, covered by foreshore-basinal deposits consisting mainly of sand and silt with varying amounts of gravel and underlain by the bedrock of the Middle Ordovician Simcoe Group consisting primarily of limestone.
- The soil stratigraphy revealed at the Site generally consisted of topsoil or asphalt pavement structure overlying the fill materials, underlain by cohesionless soils consisting predominantly of sand. No bedrock was encountered on the Site to the maximum explored depth of 15.7 mbgs.
- Groundwater levels measured recently in the monitoring wells ranged in depth from 8.87 mbgs to 9.82 mbgs, and the elevations ranged from 221.93 mAMSL to 222.28 mAMSL. The groundwater flow was inferred to be to the southwestwards.
- Based on the soil and groundwater conditions and the proposed development design, short-term construction dewatering and long-term sub-drain discharge are not expected at the Site. Therefore, PTTW or EASR registration are not required
- No significant impact due to the proposed development would be anticipated with regards to the natural environmental features or water wells near the development Site.
- However, the proposed development lies within the 2- year Time of Travel (TOT) capture zone (WHPA-B) of Barrie Water Supply Well #s 11, 12 and 14 with moderate intrinsic vulnerability score between 6 and 8, and hence, the Lake Simcoe Source Protection Plan policies are applicable to the Site.
- As per City of Barrie Risk Management Plan within the wellhead protection areas, the road salt application best management practices should be adhered to in order to reduce any impacts to the local groundwater supply.

- As the subject property is within the Wellhead Protection Area B, WHPA-Q1, and HVA area, it is recommended to conduct and submit a Source Water Impact Assessment and Mitigation Plan (SWIAMP).
- Water balance assessment indicated a net deficit of 140 m³ /annum (or 100% decrease) in the post-development infiltration (changed from 140 m³/annum to zero), due to the fact that landscape areas were not proposed in the post-development scenario. This The deficit of 140 m³ / annum is considered insignificant.
- As per City of Barrie's LID guideline, infiltration based LID practices (such as permeable pavers) is not permitted. Given the proposed design, there is little or no space available for the implementation of LID measures.

14.0. SELECTED BIBLIOGRAPHY

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CITY OF BARRIE, Infiltration Low Impact Development Screening Process (undated)

15.0. LIMITATIONS AND USE OF THE REPORT

This report was produced for the sole use of Vitmont Holdings (Barrie) Inc. (the Client), for the property located at 79 Collier Street, in the City of Barrie, Ontario and may not be relied upon by any other person or entity without the written authorization of Sirati & Partners Consultants Ltd. (SIRATI). The conclusions presented in this report are professional opinions based on the historical and current records search, visual observations and limited information provided by persons knowledgeable about past and current activities on this site. As such, SIRATI cannot be held responsible for environmental conditions at the Property that was not apparent from the available information. No investigation method can completely eliminate the possibility of obtaining partially imprecise or incomplete information; it can only reduce the possibility to an acceptable level.

Professional judgement was exercised in gathering and analyzing data and formulation of recommendations using current industry guidelines and standards. Similar to all professional persons rendering advice, SIRATI cannot act as absolute insurer of the conclusion we have reached. No additional warranty or representation, expressed or implied, is included or intended in this report other than stated herein the report.

The assessment should not be considered a comprehensive audit that eliminates all risks of encountering environmental problems. The information presented herein this report is primarily based on information collected during the hydrogeological study based on the condition of the Property at the time of site inspection/drilling followed by a review of historical data, as appended to this report.

In assessing the environmental setting of the Property, SIRATI has solely relied upon information supplied by others in good faith and has therefore assumed that the information supplied is factual and accurate. We accept no responsibility for any inaccurate information, misrepresentation or for any deficiency of the information supplied by any third party.

The scope of services performed in the execution of this investigation may not be appropriate to satisfy third parties. SIRATI accepts no responsibility for damages if any, suffered by any third party as a result of decisions made or action taken based on this report. Any use, copying or distribution of the report in whole or in part is not permitted without the express written permission of SIRATI and use of findings, conclusions and recommendations represented in this report, is at the sole risk of third parties.

In the event that during future work new information regarding the environmental condition of the Property is encountered, or in the event that the outstanding responses from the regulatory agencies indicate outstanding issues on file with respect to the Property, SIRATI should be notified in order that we may re-evaluate the findings of this assessment and provide amendments, as required.

16.0. SIGNATURES

Should you have any questions regarding the information presented or limitation set in this report, please do not hesitate to contact our office.

Yours truly,

Sirati and Partners Consultants Ltd.



Sudhakar Kurli, M.Sc., P. Geo.
Hydrogeologist/Project Manager



Bujing Guan, M. A.Sc., P. Geo.
Senior Hydrogeologist/Environmental Specialist

FIGURES



North:

Legend:

Property Boundary

Project Title:

Hydrogeological Investigation

Site Location:

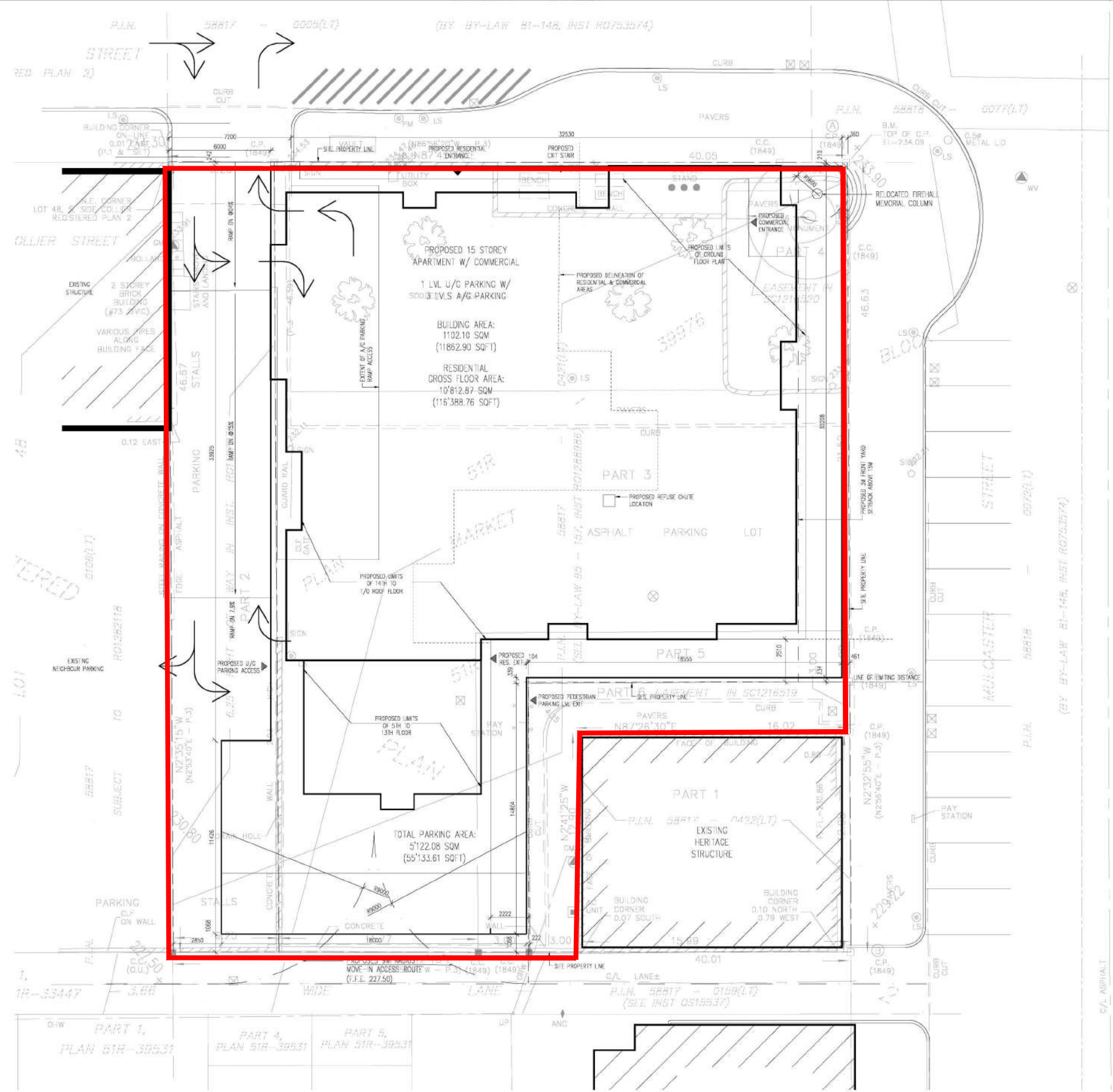
79 Collier Street, Barrie, ON

Figure Title:

Site Location Plan

Scale:	Project Number:
As Shown	SP20-666-30

Date:	Figure Number:
September 2020	1-1



1 SITE PLAN
SCALE 1:125

North:



Legend:

Property Boundary

PROJECT NAME: BAYSIDE APARTMENTS		
PROJECT ADDRESS: 79 COLLIER STREET, BARRIE, ONTARIO		
DATE: MAY 05, 2020	JOB NO.	SHEET NO.
DRAWN BY: NT	00-000	A1.1
SCALE: 1:125		

Project Title:

Hydrogeological Investigation

Site Location:

79 Collier Street, Barrie, ON

Figure Title:

Site Development Plan

Scale: As Shown	Project Number: SP20-666-30
Date: September 2020	Figure Number: 5-1

North:

Legend:

DRAWING TITLE

BUILDING SECTION

PROJECT NAME

BAYSIDE APARTMENT

79 COLLIER ST. BARRIE, ON

MARYDEL

DATE

MAY 11, 2020

PROJECT #

SHEET #

A4.1

DRAWN BY

Author

PROJECT #

SCALE

1 : 150

Project Title:
Hydrogeological Investigation

Site Location:
79 Collier Street, Barrie, ON

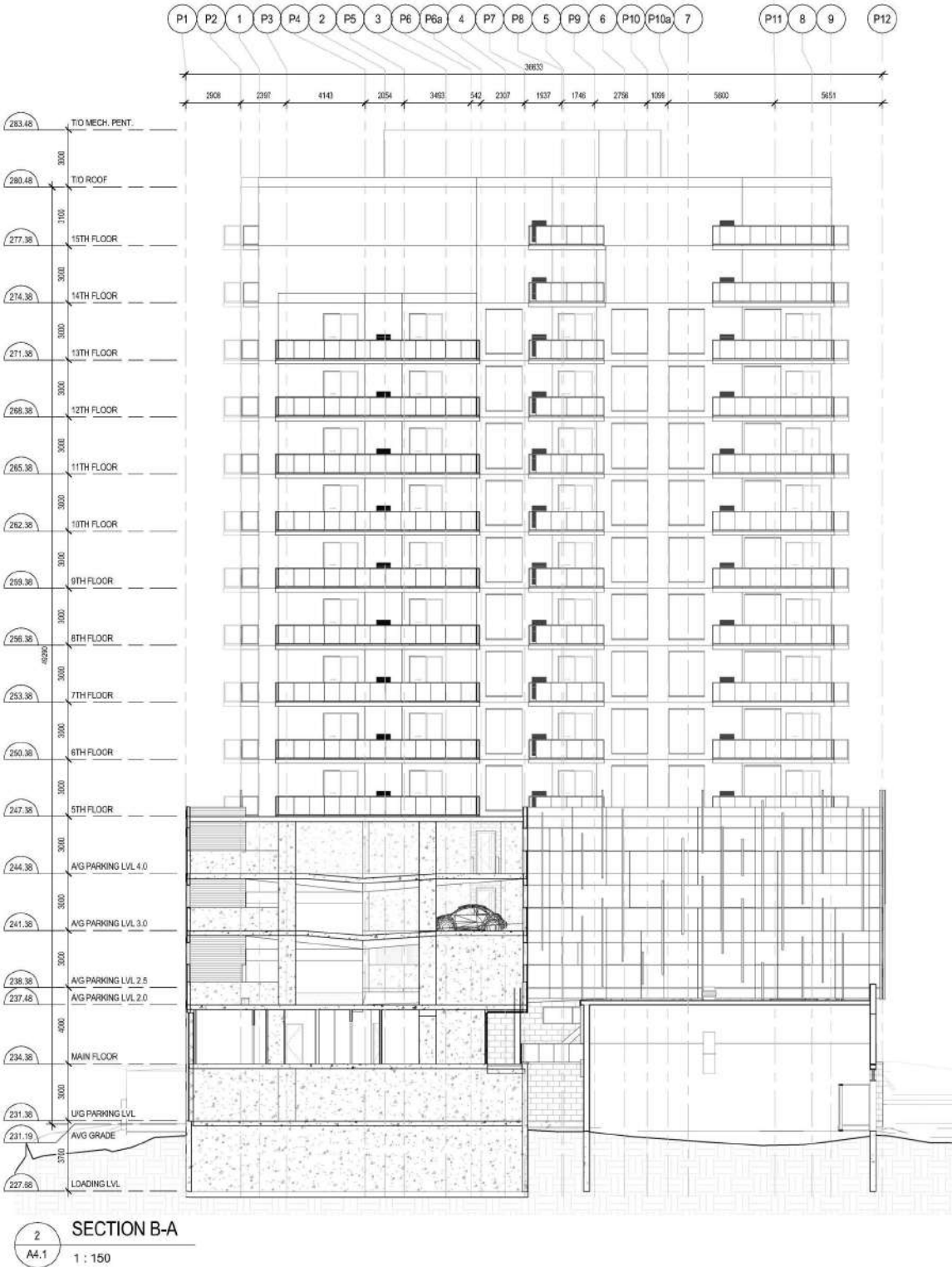
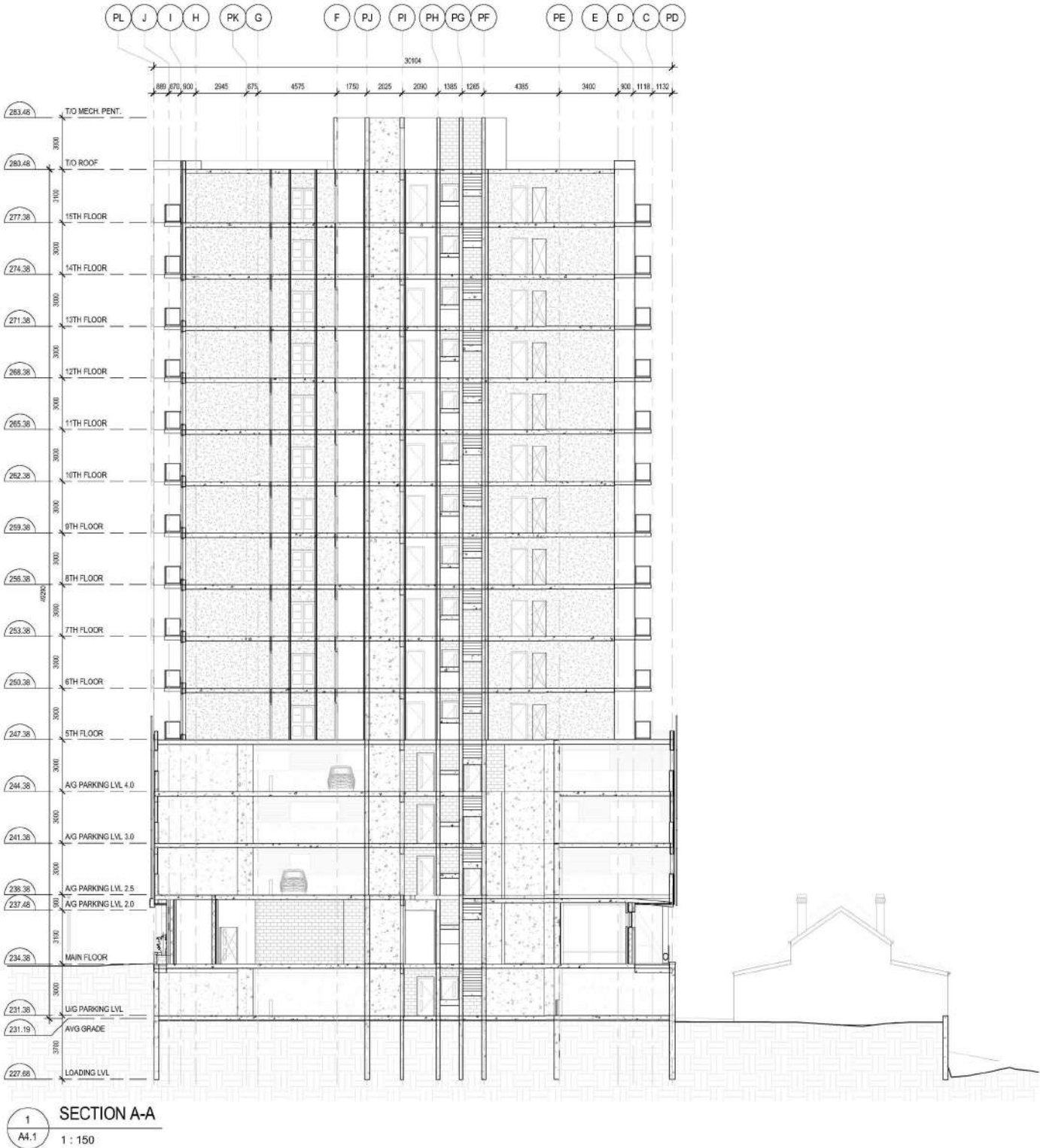
Figure Title:
Building Sectional Map

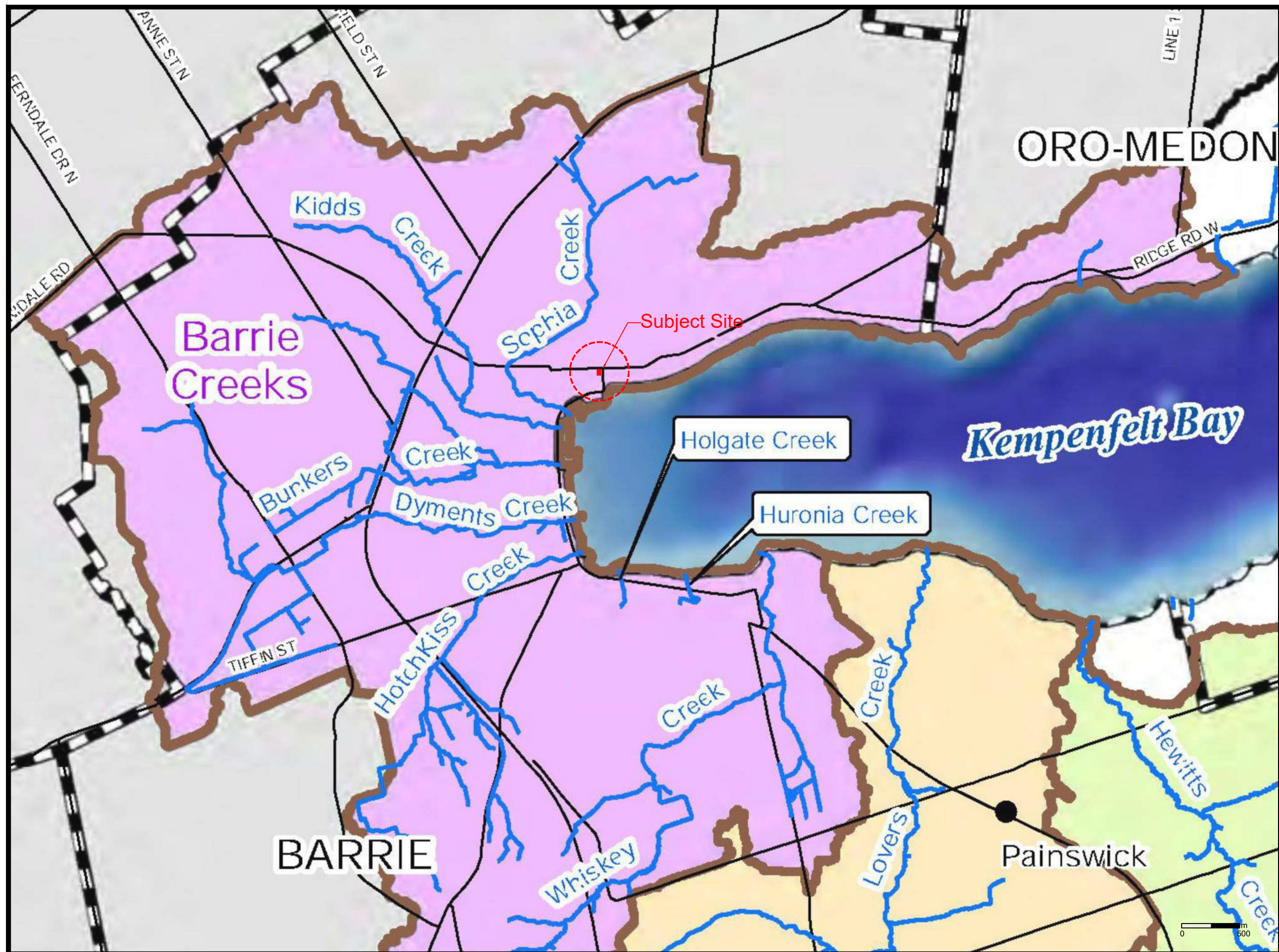
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As Shown

Project Number:
SP20-666-30

Date:
September 2020

Figure Number:
5-2





SIRATI & PARTNERS
Geotechnical Hydrogeological & Environmental Solutions
12700- Keele Street
King City, ON. L7B 1H5
Phone# 905 833 1582, Fax# 905 833 5360

North:

Legend:

Subject Site

Approximately 500 m from the Site

Legend

Road

Municipal Boundary

Watercourse

Barrie Creeks

Hewitts Creeks

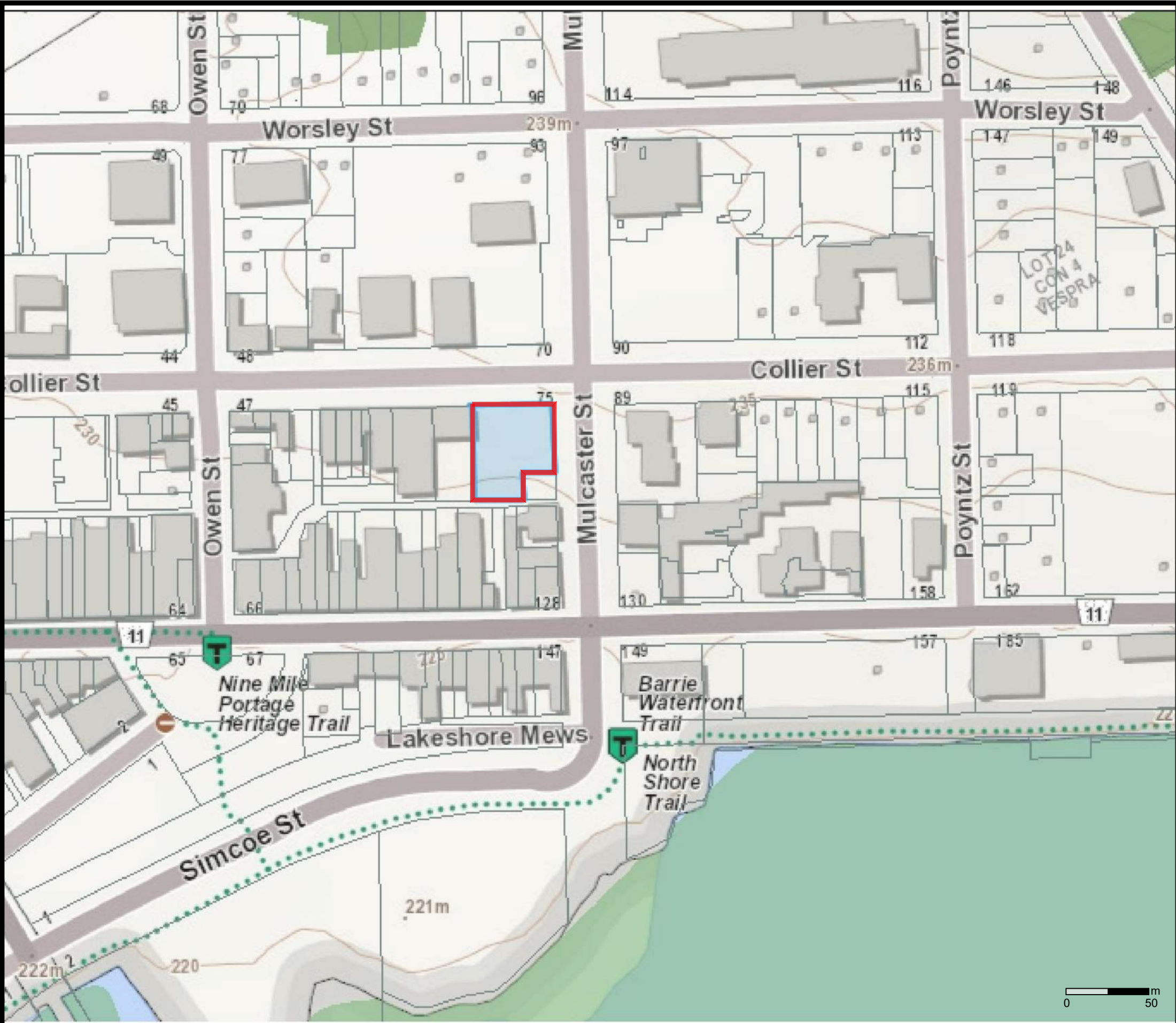
Lovers Creeks

Project Title:
Hydrogeological Investigation

Site Location:
79 Collier Street, Barrie, ON

Figure Title:
Barries Creeks Watershed Map

Scale: As Shown	Project Number: SP20-666-30
Date: September 2020	Figure Number: 6-1



Legend

Assessment Parcel

Woodland

Conservation Reserve

Provincial Park

Natural Heritage System

Ecoregion

Wetland

Provincially Significant Wetland Evaluated

Non - Provincially Significant Wetland Evaluated

Unevaluated Wetland

Area of Natural Heritage & Scientific Interest (ANSI)

Provincially Significant Life Science ANSI

Provincially Significant Earth Science ANSI

Greenbelt Plan

Boundary

Greenbelt External Connections

Land Use Designations

Protected Countryside

Greenbelt Towns and Villages

Greenbelt Hamlets

Urban River Valley

Greenbelt Specialty Crop Area

Niagara Escarpment Plan (NEP)

Boundary

Parks and Open Space System

Land Use Designations

Escarpment Natural Area

Escarpment Protection Area

Escarpment Rural Area

Mineral Resource Extraction Area

Escarpment Recreation Area

Urban Area

Minor Urban Centre

Oak Ridges Moraine Conservation Plan (ORM)

Boundary

Land Use Designations

Natural Core Area

Natural Linkage Area

Countryside Area

Rural Settlement

Palgrave Estates Residential Community

Settlement Area

SIRATI & PARTNERS

Geotechnical Hydrogeological & Environmental Solutions

12700- Keele Street

King City, ON. L7B 1H5

Phone# 905 833 1582, Fax# 905 833 5360

North:

Legend:

Property Boundary

Project Title:

Hydrogeological Investigation

Site Location:

79 Collier Street, Barrie, ON

Figure Title:

Key Hydrological and Natural Heritage Features Map

Scale:

As Shown

Project Number:

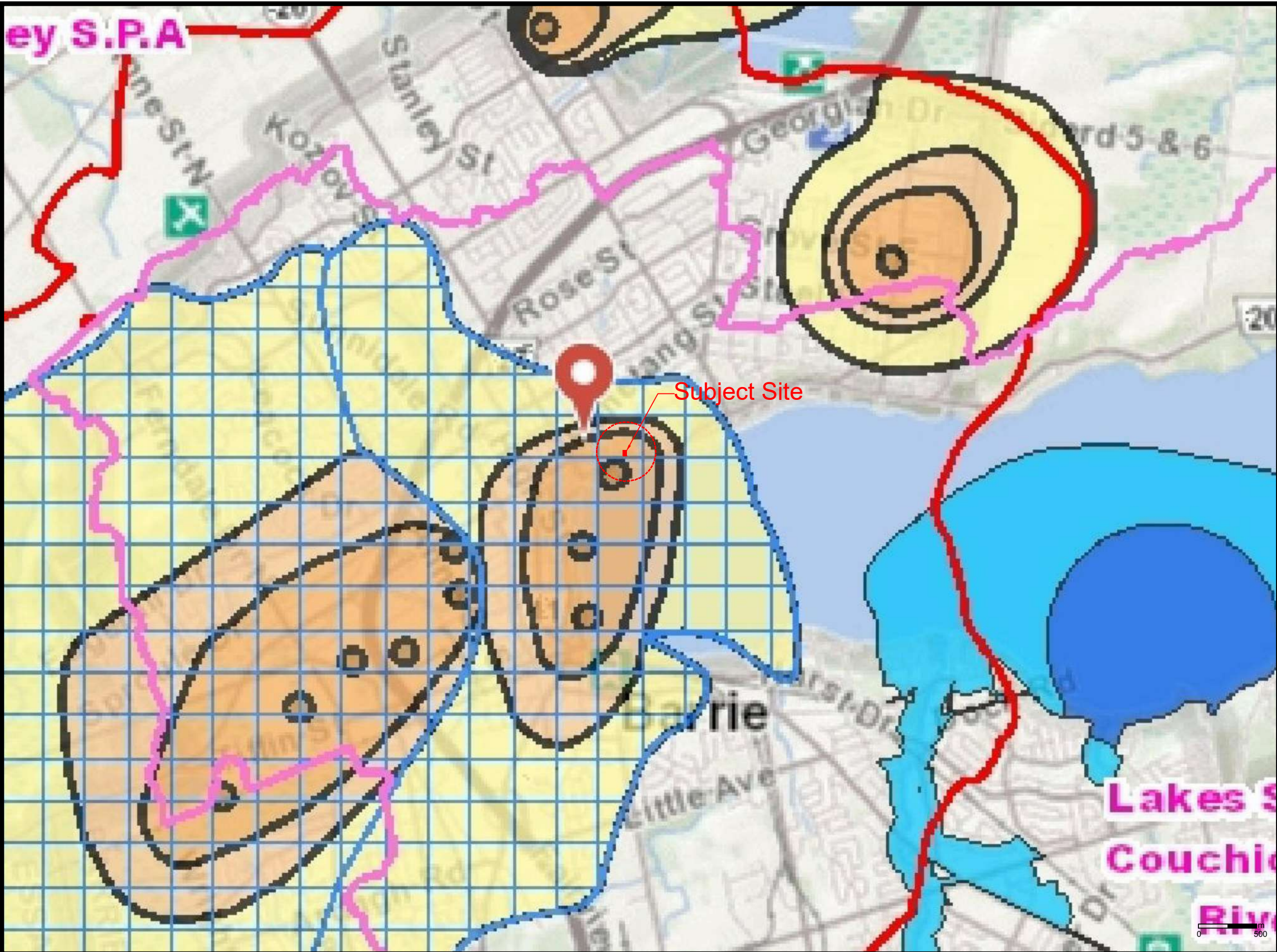
SP20-666-30

Date:

September 2020

Figure Number:

6-2



- Legend:**
- Subject Site
 - Approximately 500 m from the Site

- Legend**
- Source Protection Areas
 - Intake Protection Zone Q
 - Wellhead Protection Area Q1
 - Wellhead Protection Area Q2
 - Issue Contributing Areas
 - WHPA Groundwater Under Direct Influence (WHPA-E)
 - Wellhead Protection Area**
 - A
 - B
 - C
 - C1
 - D
 - F
 - Intake Protection Zone 1
 - Event Based Areas
 - Intake Protection Zone 2

Project Title:
Hydrogeological Investigation

Site Location:
79 Collier Street, Barrie, ON

Figure Title:
Source Protection Areas Map

Scale: As Shown
Project Number: SP20-666-30

Date: September 2020
Figure Number: 6-3



North:



Legend:

Property Boundary

Features

- LSRCA Watershed Boundary
- Lake Simcoe
- Watercourse
- Regulated Area Boundary
- Regulated Area
- Road Labels
- Assessment Parcel
- Lot and Concession
- Roads
 - Hwy 400 Series
 - Highway, Arterials
 - Local Road
- Railway

Project Title:

Hydrogeological Investigation

Site Location:

79 Collier Street, Barrie, ON

Figure Title:

LSRCA Regulated Area Map

Scale:

As Shown

Project Number:

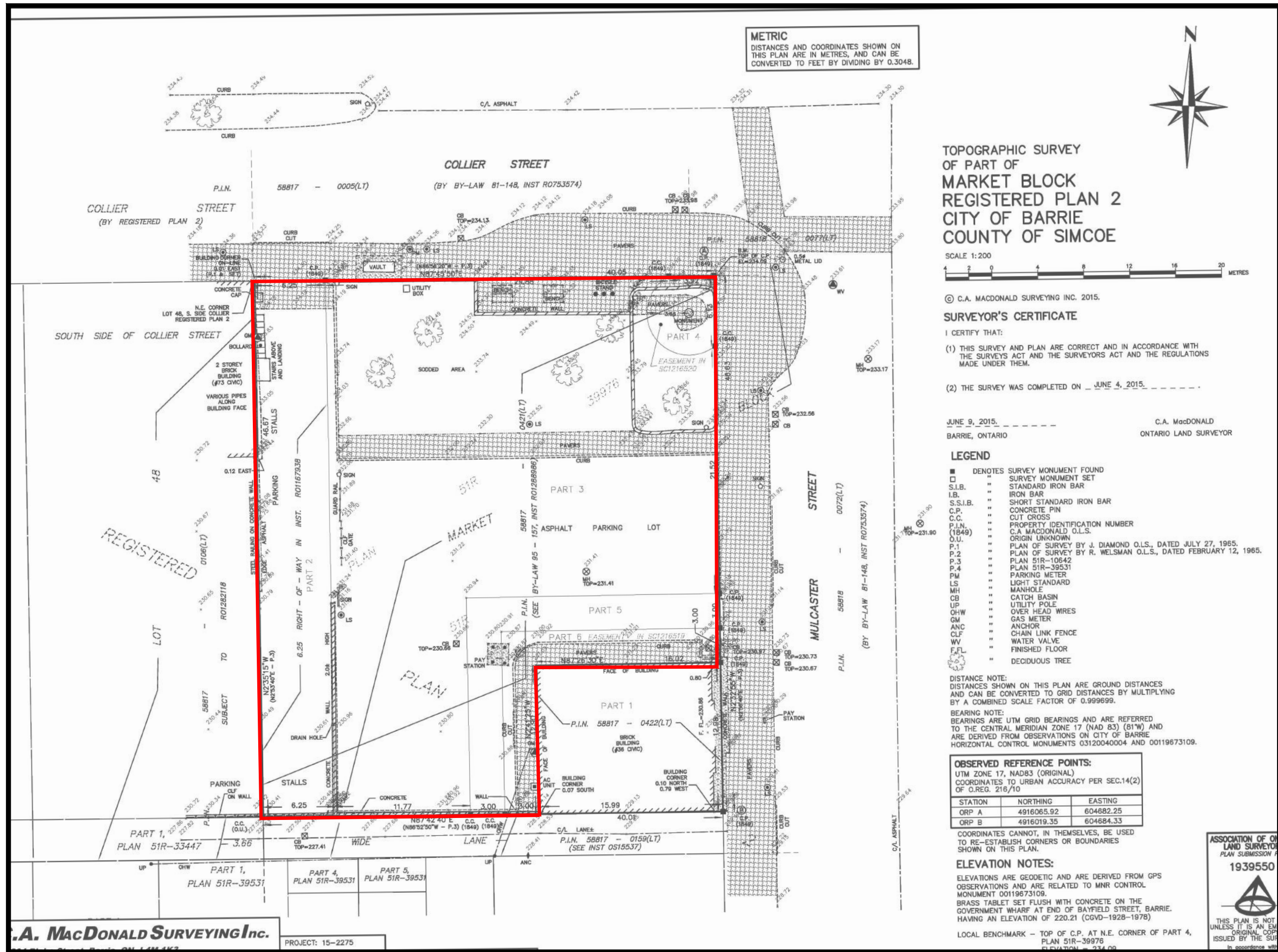
SP20-666-30

Date:

September 2020

Figure Number:

6-4



SIRATI & PARTNERS
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12700- Keele Street
King City, ON. L7B 1H5
Phone# 905 833 1582, Fax# 905 833 5360

North:

Legend:

Property Boundary

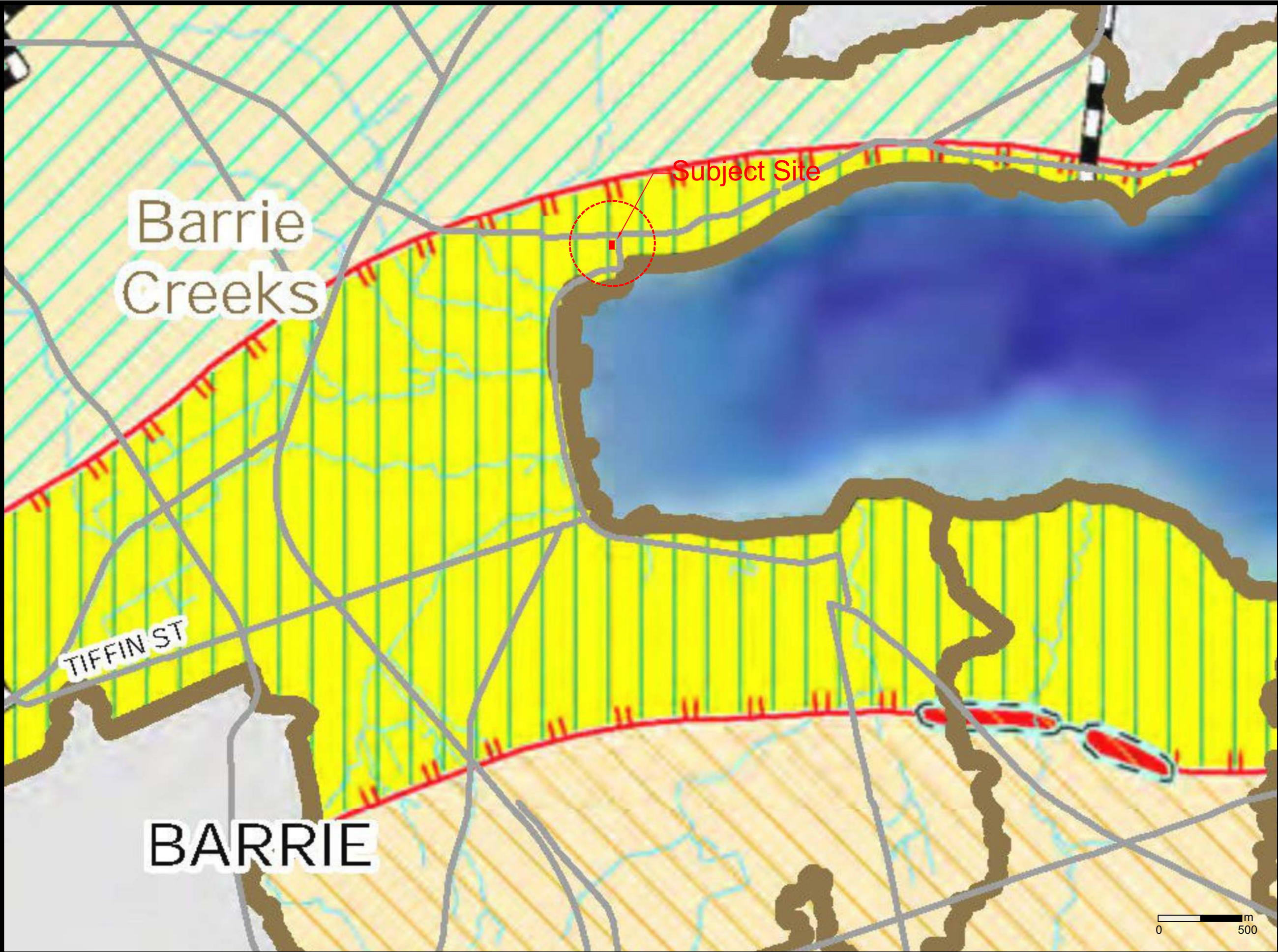
Project Title:
Hydrogeological Investigation

Site Location:
79 Collier Street, Barrie, ON

Figure Title:
Site Survey Map

Scale:	Project Number:
As Shown	SP20-666-30

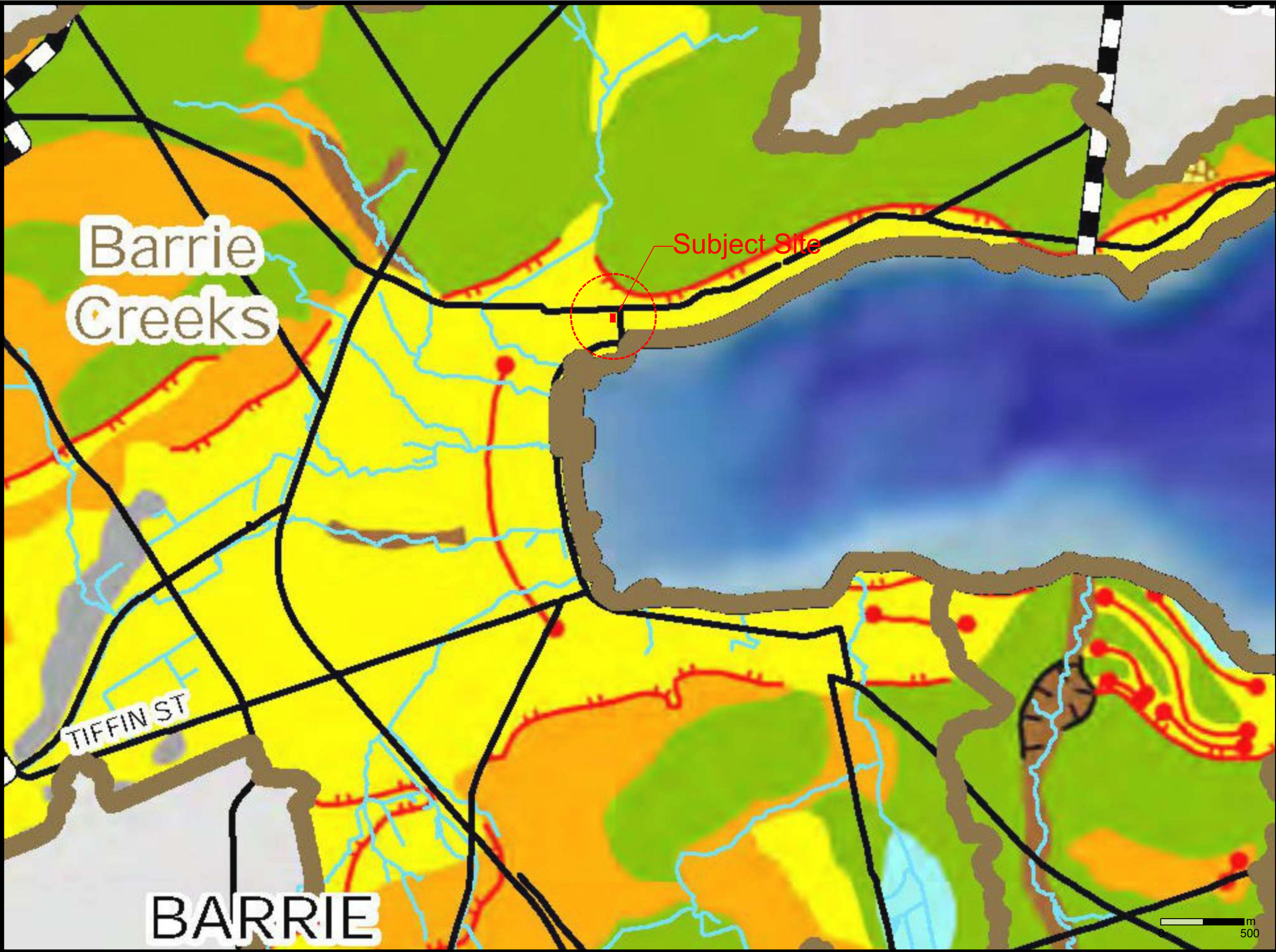
Date:	Figure Number:
September 2020	7-1



- Legend:**
- Subject Site
 - Approximately 500 m from the Site

- Legend**
- Road
 - Municipal Boundary
 - Watercourse
 - Physiography Features**
 - Dissected terrain
 - Mud flow scars
 - Contact
 - Shorecliff
 - Simcoe Uplands
 - Simcoe Lowlands
 - Peterborough Drumlin Field
 - Beach
 - Drumlin
 - Sand Plain
 - Till Plain (Drumlinized)

Project Title: Hydrogeological Investigation	
Site Location: 79 Collier Street, Barrie, ON	
Figure Title: Physiography Map	
Scale: As Shown	Project Number: SP20-666-30
Date: September 2020	Figure Number: 7-2



North:

Legend:

- Subject Site
- Approximately 500 m from the Site

Legend

- Road
- Municipal Boundary
- Watercourse
- Surficial Geology Features
 - drumlin
 - beach
 - bluff
 - eskers
 - icslope
 - ribl
 - terrace
- 5b: Stone-poor, carbonate-derived silty to sandy till
- 6: Ice-contact stratified deposits
- 8a: Massive-well laminated
- 9b: Littoral-foreshore deposits
- 9c: Foreshore-basinal deposits
- 12: Older alluvial deposits
- 19: Modern alluvial deposits
- 20: Organic deposits

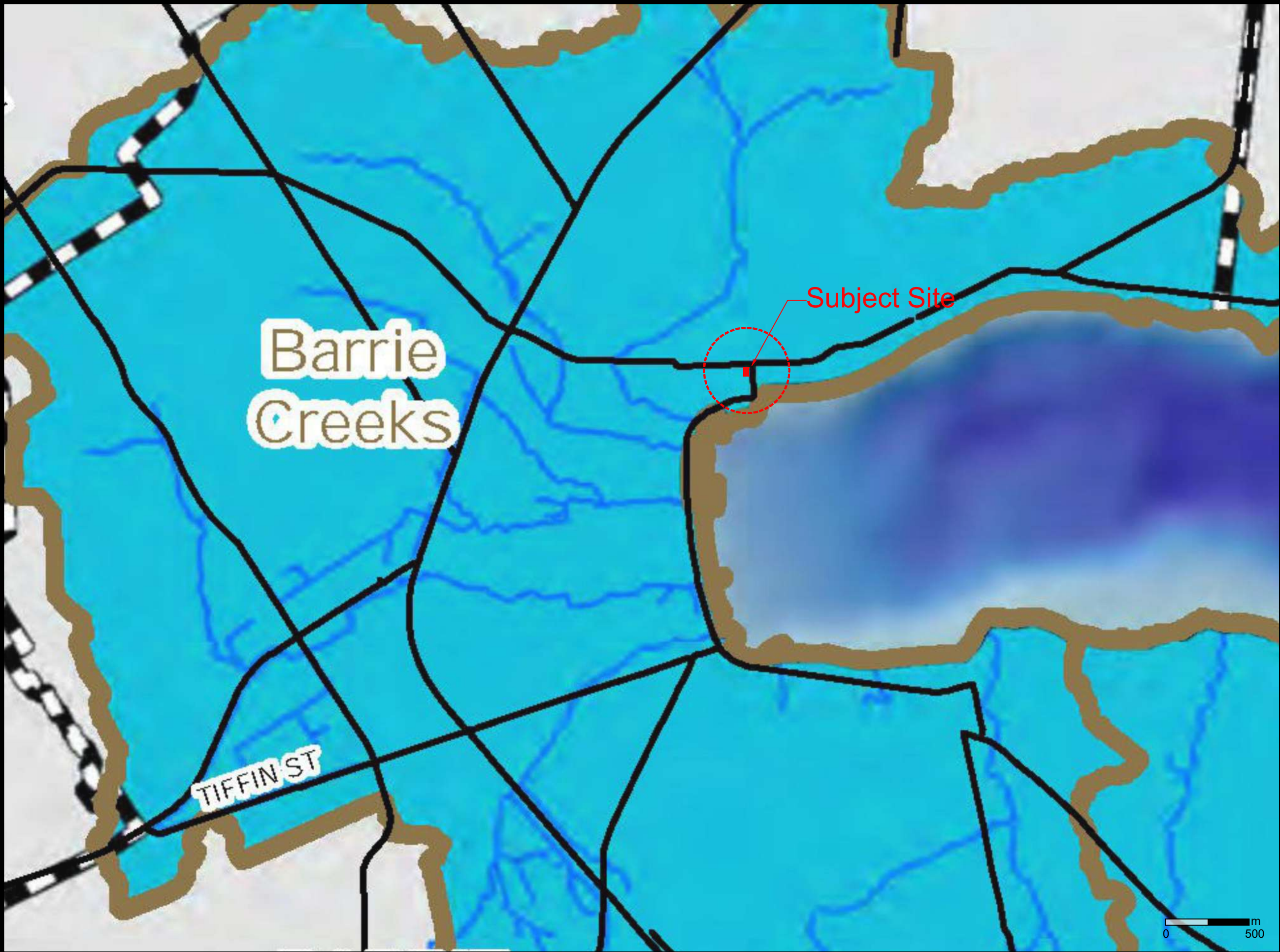
Project Title:
Hydrogeological Investigation

Site Location:
79 Collier Street, Barrie, ON

Figure Title:
Surficial Geology Map

Scale: As Shown	Project Number: SP20-666-30
---------------------------	---------------------------------------

Date: Septemebr 2020	Figure Number: 7-3
--------------------------------	------------------------------



North:

- Legend:**
- Subject Site
 - Approximately 500 m from the Site

Legend

- Road
- Municipal Boundary
- Watercourse
- 51a Ottawa Group;
Simcoe Group;
Shadow Lake Fm.

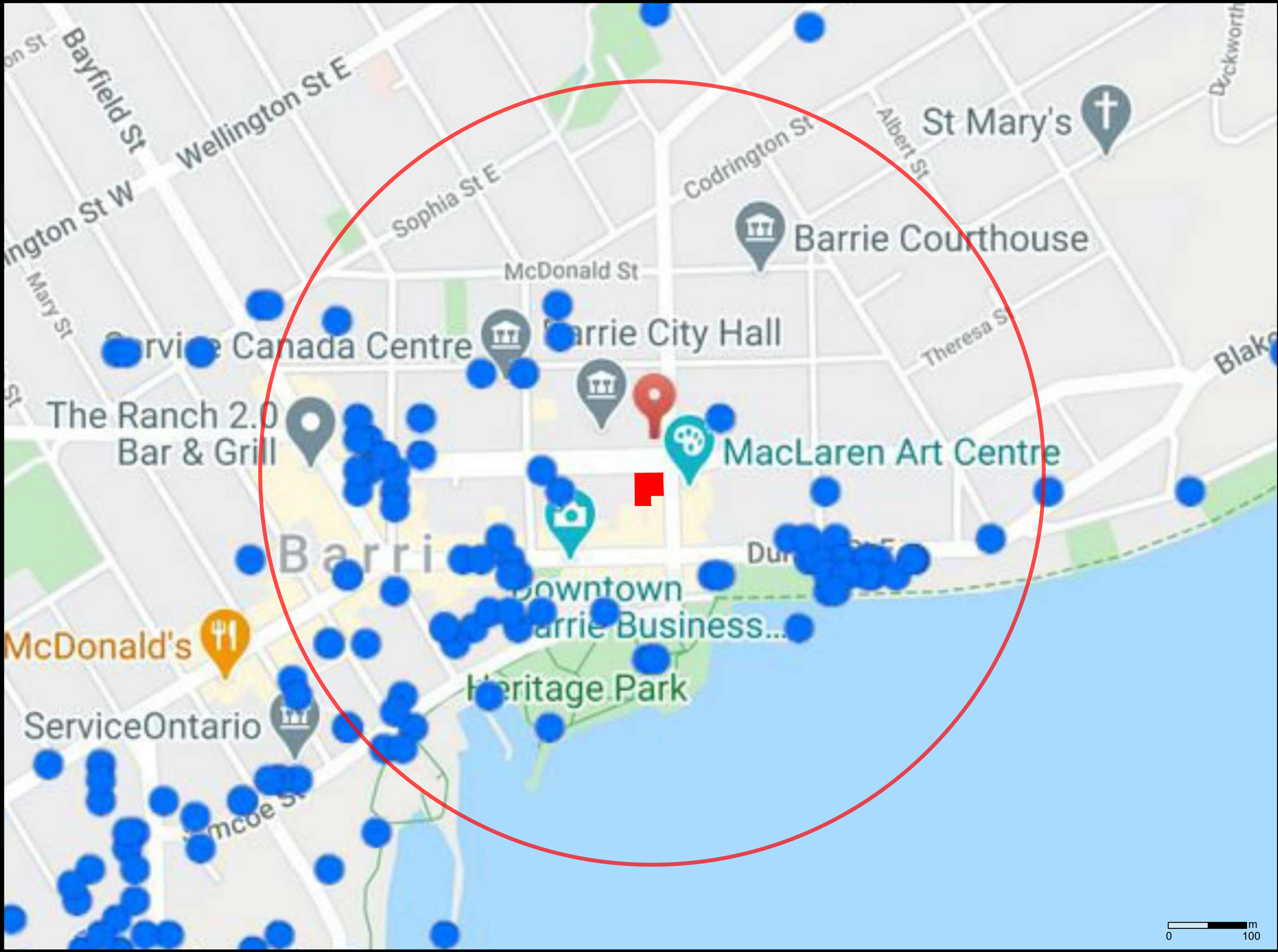
Project Title:
Hydrogeological Investigation

Site Location:
79 Collier Street, Barrie, ON

Figure Title:
Bedrock Geology Map

Scale: As Shown	Project Number: SP20-666-30
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Date: September 2020	Figure Number: 7-4
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- Legend:**
- Subject Site
 - 500m Study Area
 - MECP Well

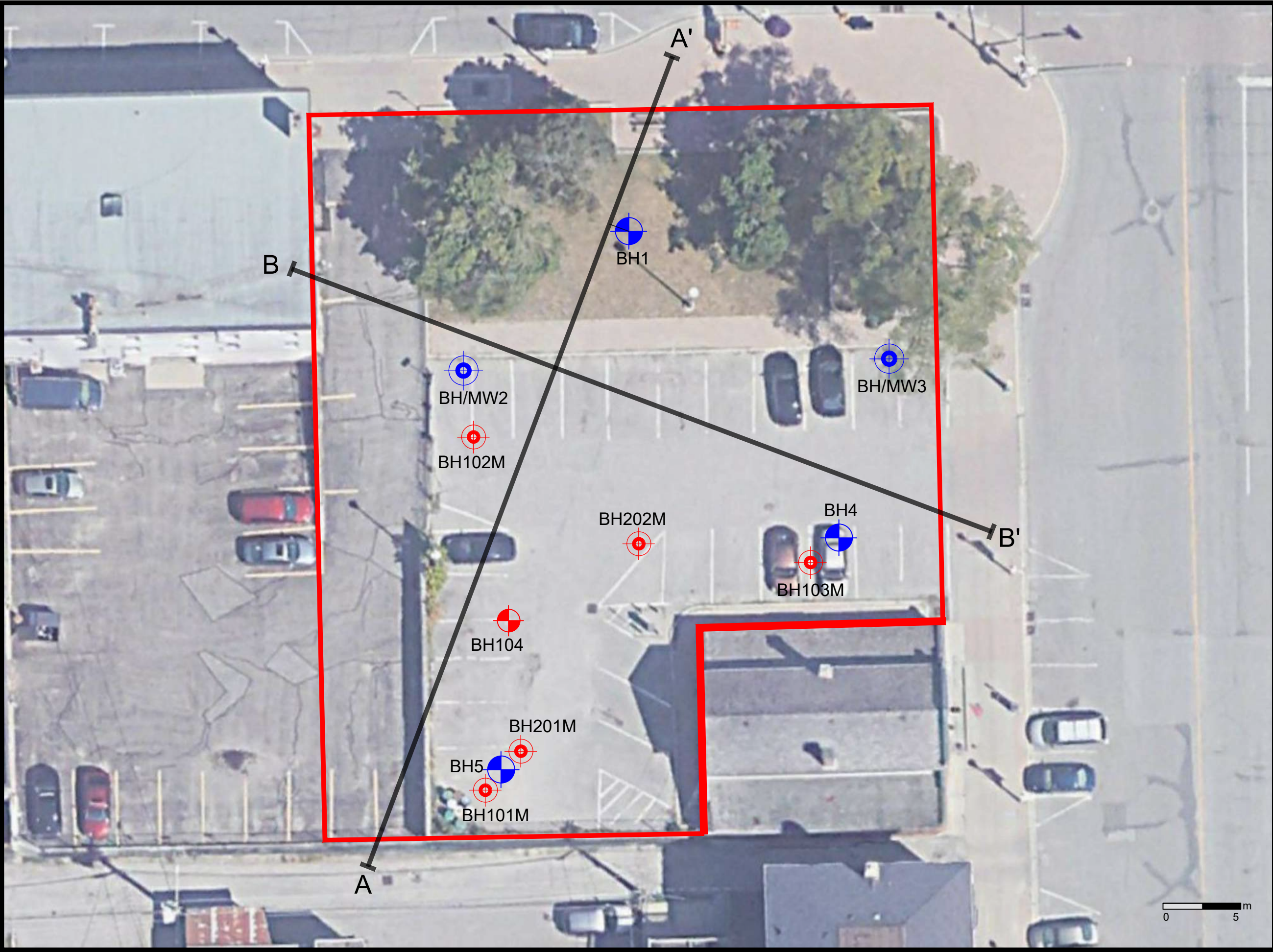
Project Title:
Hydrogeological Investigation

Site Location:
79 Collier Street, Barrie, ON

Figure Title:
MECP Water Well Records Map

Scale: As Shown	Project Number: SP20-666-30
---------------------------	---------------------------------------

Date: September 2020	Figure Number: 8-1
--------------------------------	------------------------------



North:

Legend:

- Property Boundary
- Monitoring Wells (2020 by Sirati)
- Boreholes (2020 by Sirati)
- Boreholes (2019 by PGL)
- Monitoring Wells (2019 by PGL)

Project Title:
Hydrogeological Investigation

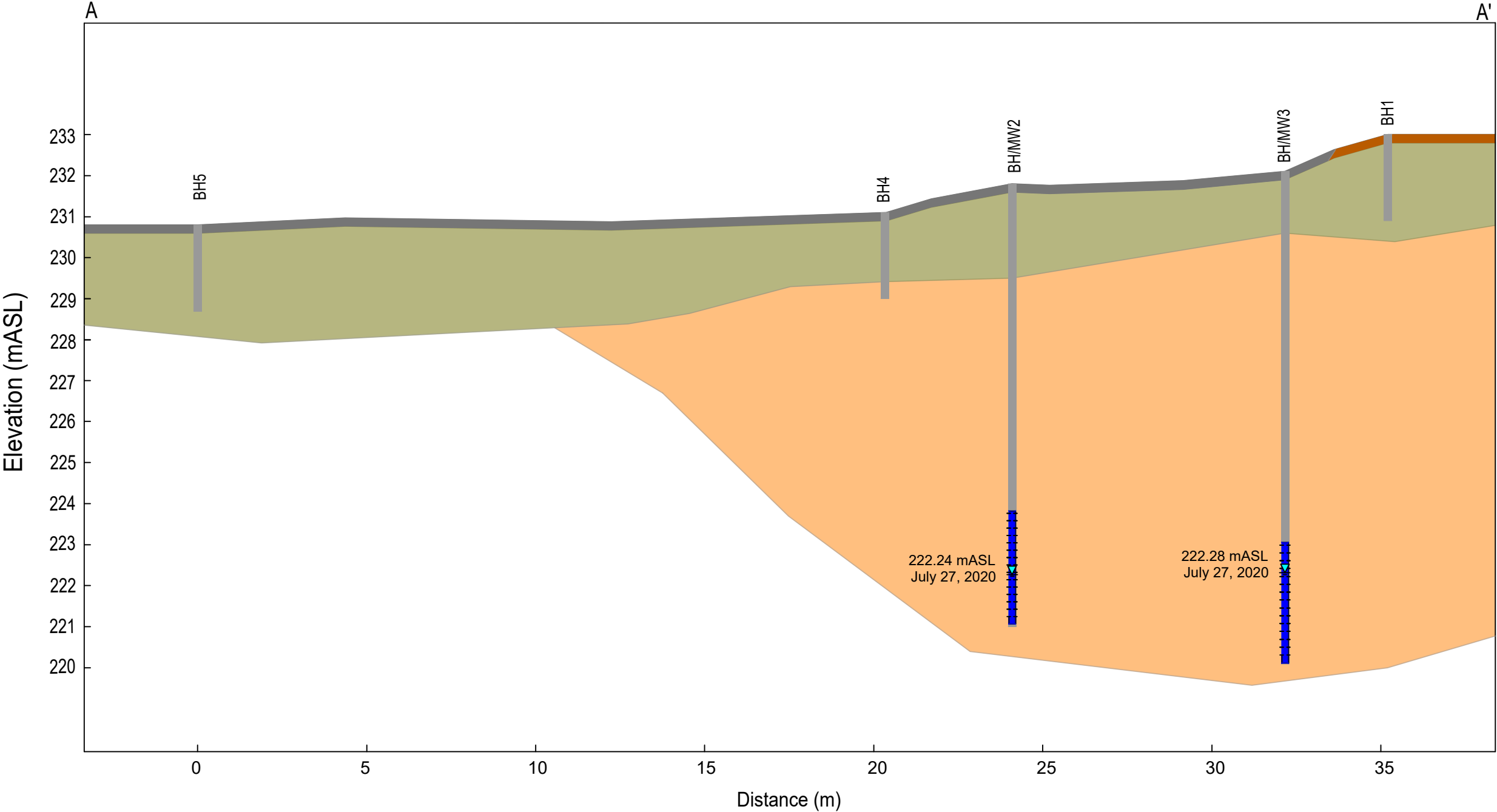
Site Location:
79 Collier Street, Barrie, ON

Figure Title:
Borehole Location plan

Scale: As Shown	Project Number: SP20-666-30
---------------------------	---------------------------------------

Date: September 2020	Figure Number: 9-1
--------------------------------	------------------------------

North:



Legend:

Asphalt

Topsoil

Fill

Sand

MW1

← Borehole / Well ID

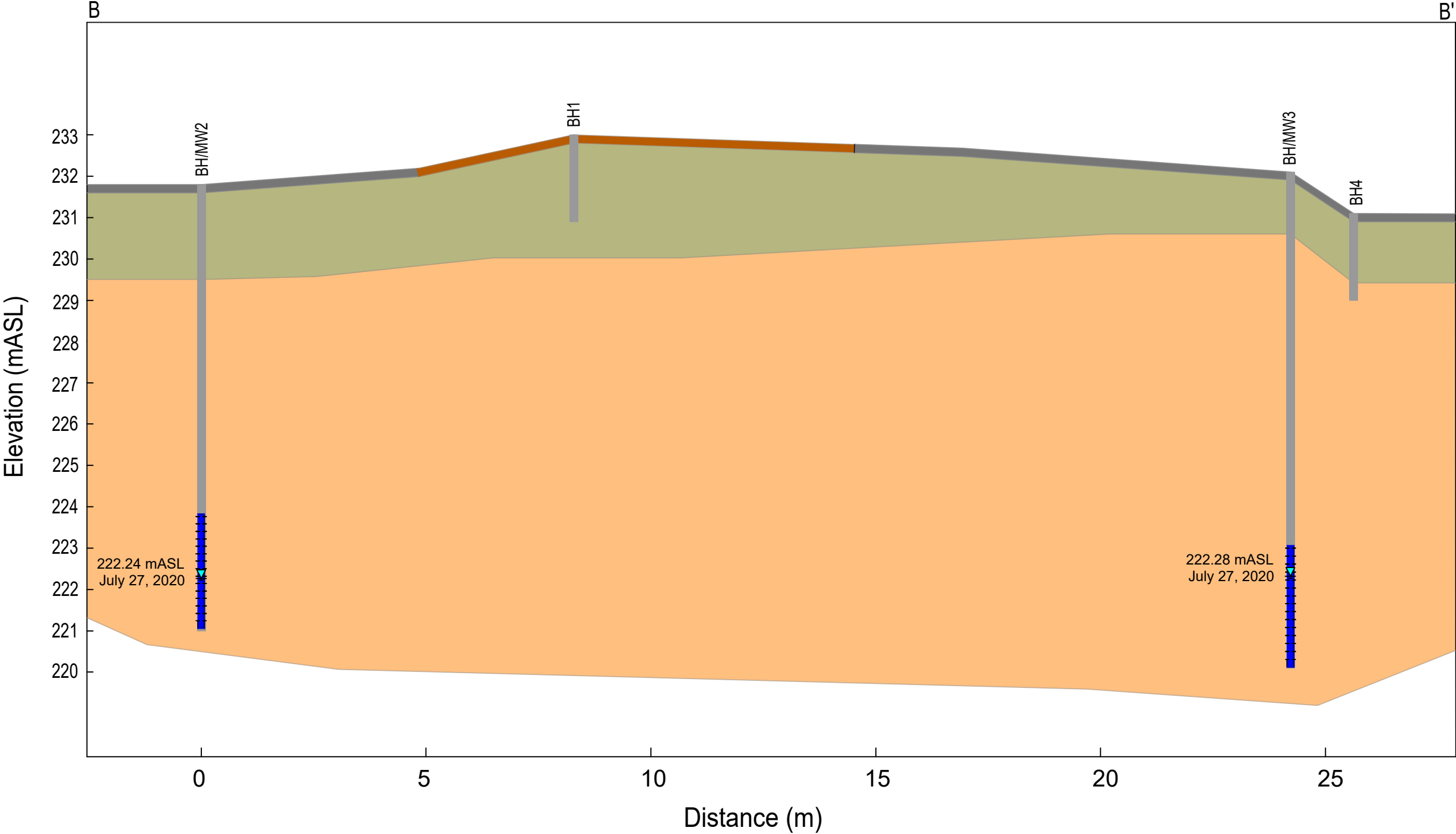
← Water Level

← Well Screen

Note: Groundwater Elevation were obtained on July 27, 2020

Project Title: Hydrogeological Investigation	
Site Location: 79 Collier Street, Barrie, ON	
Figure Title: Cross Section Profile A-A'	
Scale: N.T.S	Project Number: SP20-666-30
Date: September 2020	Figure Number: 9-2

North:



Legend:

Asphalt

Topsoil

Fill

Sand

MW1

← Borehole / Well ID

← Water Level

← Well Screen

Note: Groundwater Elevation were obtained on July 27, 2020

Project Title: Hydrogeological Investigation	
Site Location: 79 Collier Street, Barrie, ON	
Figure Title: Cross Section Profile B-B'	
Scale: N.T.S.	Project Number: SP20-666-30
Date: September 2020	Figure Number: 9-3



North:



Legend:

- Property Boundary
- Monitoring Wells (2020 by Sirati)
- Boreholes (2020 by Sirati)
- Boreholes (2019 by PGL)
- Monitoring Wells (2019 by PGL)
- Contour Line
- Inferred Shallow Groundwater Flow Direction

Note: Groundwater Elevation were obtained on July 27, 2020

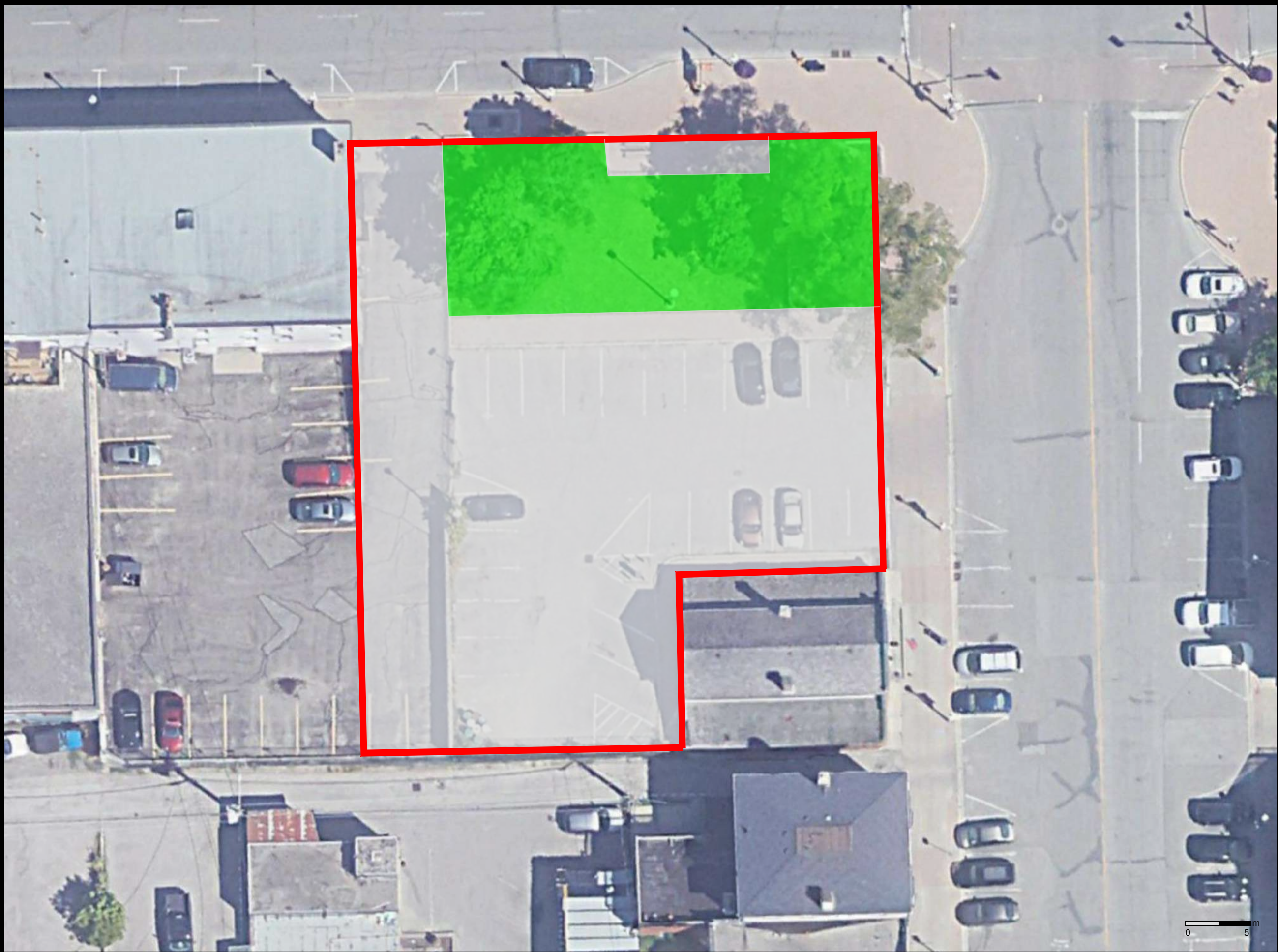
Project Title:
Hydrogeological Investigation

Site Location:
79 Collier Street, Barrie, ON

Figure Title:
Inferred Shallow Groundwater Flow Direction Map

Scale: As Shown	Project Number: SP20-666-30
---------------------------	---------------------------------------

Date: September 2020	Figure Number: 9-4
--------------------------------	------------------------------



North:



Legend:

- Property Boundary
- Paved Area
- Roof
- Landscape

Site Statistics:

Paved Area:	1260 sq.m
Roof:	0 sq.m
Landscape:	400 sq.m
Total	1660 sq.m

Project Title:

Hydrogeological Investigation

Site Location:

79 Collier Street, Barrie, ON

Figure Title:

Pre-Development Plan - Site Statistics

Scale:

As Shown

Project Number:

SP20-666-30

Date:

September 2020

Figure Number:

12-1

North:



Legend:

- Property Boundary
- Paved Area
- Roof
- Landscape

Site Statistics:

Paved Area:	558 sq.m
Roof:	1102 sq.m
Landscape:	0 sq.m
Total	1660 sq.m

Project Title:

Hydrogeological Investigation

Site Location:

79 Collier Street, Barrie, ON

Figure Title:

Post-Development Plan - Site Statistics

Scale:

As Shown

Project Number:

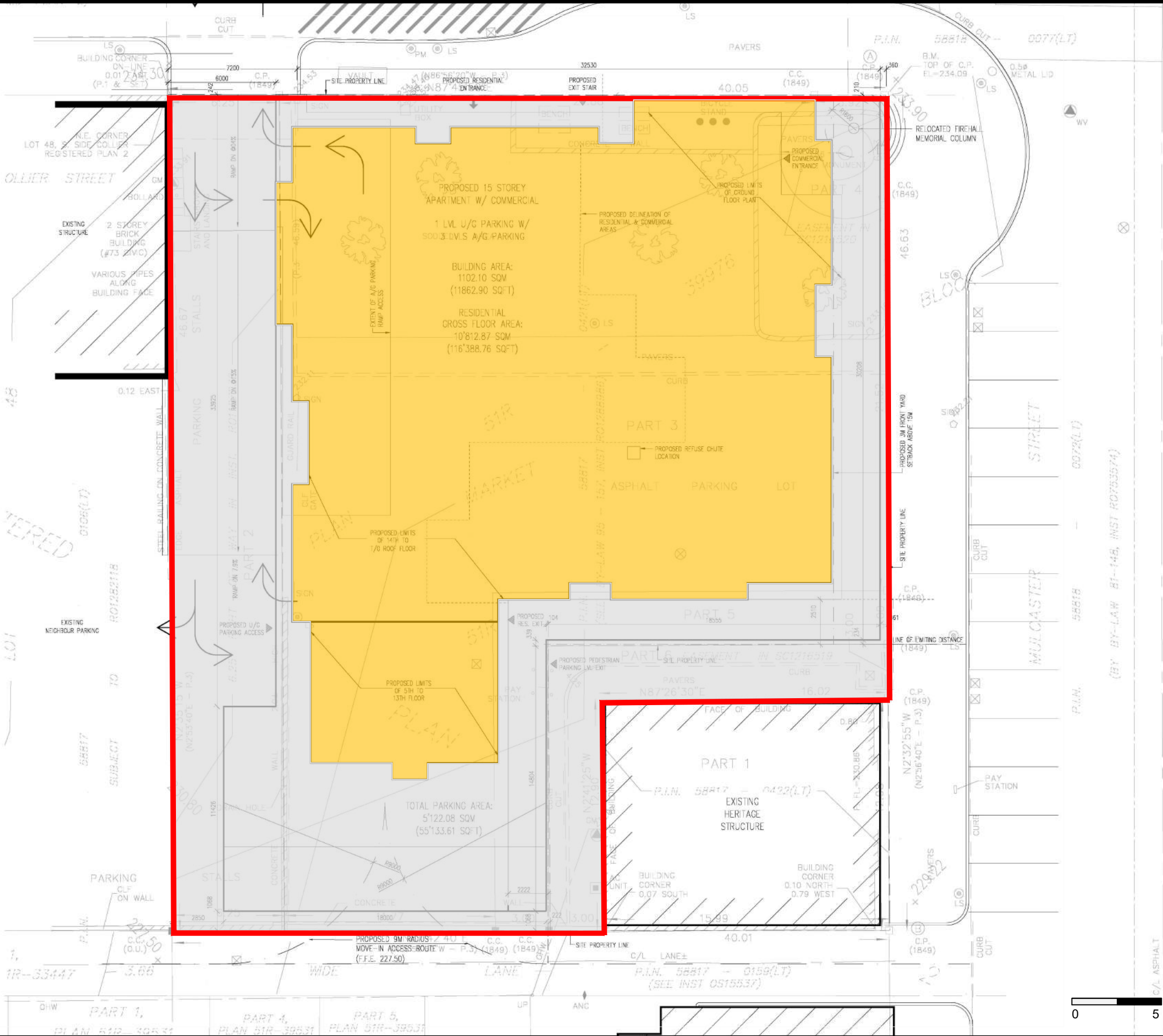
SP20-666-30

Date:

September 2020

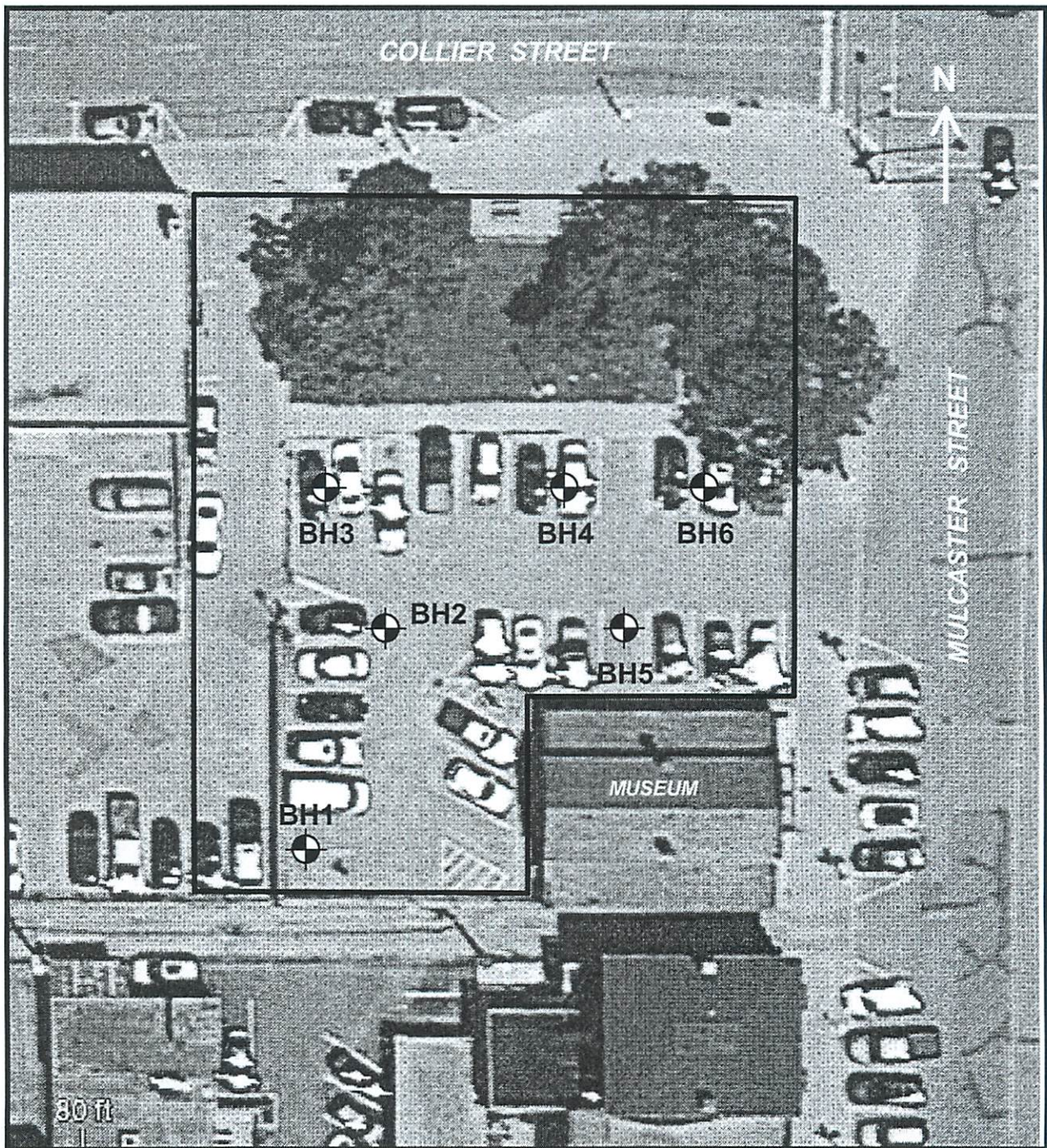
Figure Number:

12-2



APPENDICES

APPENDIX A1



BOREHOLE LOCATION PLAN

Reference No : 6862-16-02

Borehole No : 1

Enclosure No : 2

Client : Edgecon Inc.

Project : Proposed Condominium

Method : Auger

Location : 36 Mulcaster Street, Barrie, ON

Diameter : 110 mm

Datum Elevation : Local

Date : March 29, 2016

SUBSURFACE PROFILE					SAMPLE			Standard Penetration Test blows/300mm				Moisture Content, %				Remarks
Elevation m	Depth m	Description	Symbol	Water	Number	Type	N-value									
99.88	0	Ground Surface														
	1	Asphalt 75 mm Granular Base 250 mm			1	SS	17									
				2	SS	8										
	2	FILL Gravelly well graded sand, cinders, brick fragments and organics in places, dark grey to dark brown, moist, very loose to compact		3	SS	3										
				4	AS	14										
	3			5	SS	8										
95.88	4	FINE SAND Loose, fine sand, trace to some silt, brown, moist to wet														
	5			6	SS	4										
	6			7	SS	4										
92.88	7															
	8	GRAVELLY SAND Very dense, well graded sand with fine to medium gravel, brown, wet		8	SS	100+										
	9	SANDY SILT TILL Dense, trace fine gravel, some seams of fine sand, brownish grey, moist	9	SS	38								cave in at 9 m			
89.88	10															
	11	FINE SAND Very dense, fine sand, some silt, some gravel at the bottom, grey, wet			10	SS	96									
	12															
	87.23			11	AS	100+										
	13	End of Borehole														

V.A. WOOD ASSOCIATES LIMITED

Disk :

Sheet : 1 of 1

Reference No : 6862-16-02

Borehole No : 2

Enclosure No : 3

Client : Edgecon Inc.

Project : Proposed Condominium

Method : Auger

Location : 36 Mulcaster Street, Barrie, ON

Diameter : 110 mm

Datum Elevation : Local

Date : March 28, 2016

SUBSURFACE PROFILE					SAMPLE			Standard Penetration Test blows/300mm				Moisture Content, %			Remarks
Elevation m	Depth m	Description	Symbol	Water	Number	Type	N-value	20	40	60	80	5	15	25	
99.96	0	Ground Surface													
		Asphalt 75 mm Granular Base 325 mm			1	SS	15								Borehole open and dry on completion
	1	FILL Gravelly sand, trace brick fragments, dark grey, moist, compact			2	SS	9								
98.56															
	2	FILL Fine to medium sand, trace topsoil, brown, moist, loose			3	SS	4								
97.86															
	3	SAND Compact, fine sand, trace silt, brown, damp to moist			4	SS	14								
96.46					5	SS	18								
	4	End of Borehole													
	5														
	6														
	7														

V.A. WOOD ASSOCIATES LIMITED

Disk :

Sheet : 1 of 1

Reference No : 6862-16-02

Borehole No : 3

Enclosure No : 4

Client : Edgecon Inc.

Project : Proposed Condominium

Method : Auger

Location : 36 Mulcaster Street, Barrie, ON

Diameter : 110 mm

Datum Elevation : Local

Date : March 28, 2016

SUBSURFACE PROFILE					SAMPLE			Standard Penetration Test blows/300mm				Moisture Content, %			Remarks
Elevation m	Depth m	Description	Symbol	Water	Number	Type	N-value	20	40	60	80	5	15	25	
100.74	0	Ground Surface													
		Asphalt 75 mm	X		1	SS	29	○				●			Borehole open and dry on completion
		Granular Base 275 mm FILL			2	SS	8	○							
99.34	1	Gravelly well graded sand, trace brick fragments, dark grey, moist, compact then loose													
			D		3	SS	24	○				●			
	2				4	SS	44	○							
		SAND													
		Compact to dense, fine to medium sand, trace silt and fine gravel, brown, damp to moist			5	SS	45	○				●			
96.74	4														
		FINE SAND	moist wet												
		Compact, trace silt, greyish brown, moist then wet			6	SS	30	○							
	5														
	6														
94.19					7	SS	17	○				●			
		End of Borehole													
	7														
	8														

V.A. WOOD ASSOCIATES LIMITED

Disk :

Sheet : 1 of 1

Reference No : 6862-16-02

Borehole No : 4

Enclosure No : 5

Client : Edgecon Inc.

Project : Proposed Condominium

Method : Auger

Location : 36 Mulcaster Street, Barrie, ON

Diameter : 110 mm

Datum Elevation : Local

Date : March 30, 2016

SUBSURFACE PROFILE					SAMPLE			Standard Penetration Test blows/300mm				Moisture Content, %			Remarks
Elevation m	Depth m	Description	Symbol	Water	Number	Type	N-value	20	40	60	80	5	15	25	
100.61	0	Ground Surface													
		Asphalt 75 mm Granular Base 225 mm			1	SS	8								Borehole open and dry on completion
	1	FILL Fine sand, then gravelly sand, dark brown, moist, loose then compact			2	SS	15								
99.21															
	2	SAND Dense, fine to medium sand, trace fine gravel, brown, damp			3	SS	42								
98.51															
	3	SAND Compact to dense, fine sand, trace silt, brown, damp			4	SS	38								
	4														
97.11					5	SS	25								
	4	End of Borehole													
	5														
	6														
	7														

V.A. WOOD ASSOCIATES LIMITED

Disk :

Sheet : 1 of 1

Reference No : 6862-16-02

Borehole No : 5

Enclosure No : 6

Client : Edgecon Inc.

Project : Proposed Condominium

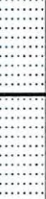
Method : Auger

Location : 36 Mulcaster Street, Barrie, ON

Diameter : 110 mm

Datum Elevation : Local

Date : March 30, 2016

SUBSURFACE PROFILE					SAMPLE											
Elevation m	Depth m	Description	Symbol	Water	Number	Type	N-value	Standard Penetration Test blows/300mm				Moisture Content, %			Remarks	
								20	40	60	80	5	15	25		
100.29	0	Ground Surface													Borehole open and dry on completion	
98.89	1	Asphalt 75 mm Granular Base 240 mm FILL Fine sand, then gravelly sand, trace brick fragments, greyish brown, moist, compact			1	SS	18									
				2	SS	15										
98.19	2	SAND Loose, fine to medium sand, brown, damp		D R Y	3	SS	7									
					4	SS	30									
93.74	5	FINE SAND Compact, trace fine gravel at the top, very dense and with some silt at the bottom, brown and damp, then brownish grey and wet <u>brown, damp</u> brownish grey, wet			5	SS	23									
	6				6	SS	18									
	7				7	SS	73									
	8	End of Borehole														

V.A. WOOD ASSOCIATES LIMITED

Disk :

Sheet : 1 of 1

Reference No : 6862-16-02

Borehole No : 6

Enclosure No : 7

Client : Edgecon Inc.

Project : Proposed Condominium

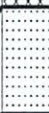
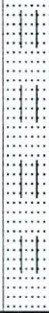
Location : 36 Mulcaster Street, Barrie, ON

Method : Auger

Diameter : 110 mm

Datum Elevation : Local

Date : March 30, 2016

SUBSURFACE PROFILE					SAMPLE			Standard Penetration Test blows/300mm				Moisture Content, %			Remarks
Elevation m	Depth m	Description	Symbol	Water	Number	Type	N-value								
100.94	0	Ground Surface													
99.54	0.5	Asphalt 75 mm			1	SS	12								
	1	Granular Base 300 mm			2	SS	43								
		FILL			3	SS	44								
98.04	1.5	Gravelly well graded sand, brownish grey, moist, compact to dense			4	SS	60								
	2	SAND			5	SS	38								
	3	Dense to very dense, fine to medium sand, some gravel, brown, damp			6	SS	21								
95.44	3.5	FINE SAND			7	SS	56								
	4	Compact to dense, fine sand, trace silt, greyish brown, moist			8	SS	95								
	5				9	SS	84								
93.94	6	SILTY SAND TILL			10	SS	88								
	7	Very dense, trace fine gravel, some seams of sand, brown, moist to wet			11	SS	44								
92.44	8	GRAVELLY SAND			12	SS	28								
	9	Very dense, well graded sand with fine to medium gravel, brown, moist			13	SS	23								
87.94	10	FINE SAND													
	11	Very dense to dense, fine sand, trace to some silt, brown then grey, wet													
	12														
85.24	13														
	14	SILT TILL													
	15	Compact, trace fine gravel, grey, moist													
	16	End of Borehole													

dry to cave in level

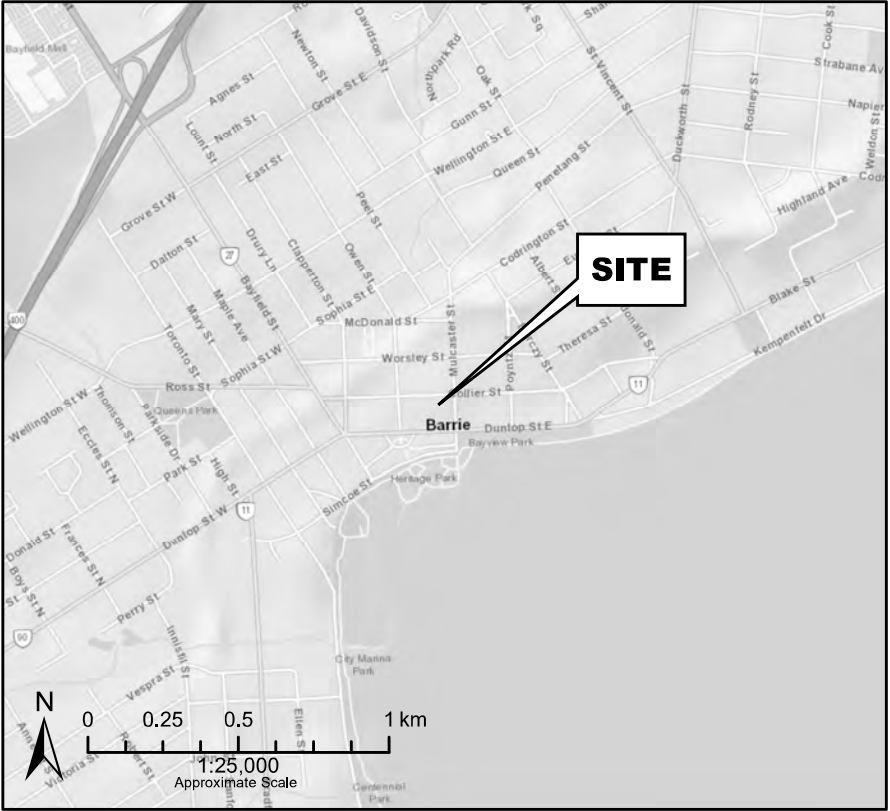
cave in at 10.4 m

V.A. WOOD ASSOCIATES LIMITED

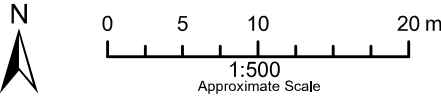
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Sheet : 1 of 1

APPENDIX A2



- Site Boundary (Approximate)
- ⊕ Borehole
- ⊕ Monitoring Well



Parcel: Approximate Image: ESRI Base Imagery

SITE LOCATION AND INVESTIGATION LOCATIONS					
36 Mulcaster Street, Barrie, ON					
GRANT THORNTON LTD.					
	File No.:	Date:	Dwg No.:	Drawn by:	FIGURE
	5717-01.01	JUN 2019	57170101-11	DPL	1

CLIENT: Grant Thornton Ltd.

PROJECT: 36 Mulcaster Street, Barrie, ON

WELL RECORD

PGL PROJECT NO: 5717-01.01

SURFACE ELEVATION: n/a

WELL NO:

BH101M

DEPTH (m)	SOIL TYPE	SOIL DESCRIPTION	SAMPLE TYPE	LABORATORY ANALYSES	● PID READING (ppmv) ● ■ VAPOUR READING (ppmv) ■	WATER LEVEL	WELL COMPLETION	COMPLETION NOTES	ELEVATION (m)
0.2		ASPHALT						Flushmount	
0.4		SAND (FILL)						J Plug	
0.6		fine to medium grained, with gravel, trace ceramics,						Cement	
0.8		trace debris, dry to moist						Silica Sand	
1.0		increased silt content for 0.15m below 0.9m							
1.2		dry, white fine sand, some black staining for 0.3m							
1.4		below 1.1m							
1.6		black, charcoal for 0.15m below 1.8m							
1.8		black staining, hydrocarbon odour for 0.6m below							
2.0		2.0m							
2.2		brick debris, trace asphalt for 0.9m below 2.7m							
2.4									
2.6									
2.8									
3.0									
3.2									
3.4									
3.6									
3.8		trace organics for 0.3m below 3.7m							
4.0		orange-brown, moist, fine sand for 1.2m below 3.7m							
4.2									
4.4									
4.6									
4.8									
5.0		black, charcoal for 0.1m below 4.9m							
5.2									
5.4		SAND							
5.6		fine grained, trace clay, brown, moist							
5.8		grey to brown below 5.5m							
6.0		wet below 6.1m							
6.2									
6.4									
6.6									
6.8									
7.0									
7.2		increased clay content below 7.2m							
7.4									
7.6		end of sampling at 7.6m; auger to depth.							
7.8									
8.0									
8.2									
8.4									

End of borehole at 8.50 m

Screened interval from 5.5 m to 8.5 m below surface.
dry on 28 May, 2019

INVESTIG. METHOD: Geoprobe 7822 DT

INVESTIG. DATE: May 23, 2019

LOGGED BY: OWM HOLE DIAM (mm): 250

Sample Notes  Macro Core Sampler

CLIENT: Grant Thornton Ltd.

PROJECT: 36 Mulcaster Street, Barrie, ON

WELL RECORD

PGL PROJECT NO: 5717-01.01

SURFACE ELEVATION: n/a

WELL NO:

BH102M

DEPTH (m)	SOIL TYPE	SOIL DESCRIPTION	SAMPLE TYPE	LABORATORY ANALYSES	PID READING (ppmv) ● VAPOUR READING (ppmv) ■	WATER LEVEL	WELL COMPLETION	COMPLETION NOTES	ELEVATION (m)
0.2		ASPHALT							
0.4		SAND (FILL)							
0.6		fine to medium grained, with gravel, trace debris,							
0.8		trace bricks, brown, dry to moist							
1.0		black staining for 0.3m below 0.9m							
1.2		rocks, asphalt pieces for 0.15m below 1.2m							
1.4		coarse-grained for 0.1m below 1.7m							
1.6									
1.8		SAND							
2.0		fine grained, trace clay, grey and brown, moist							
2.2									
2.4									
2.6									
2.8									
3.0									
3.2									
3.4									
3.6		coarse-grained, trace gravel for 0.3m below 3.4m							
3.8									
4.0									
4.2									
4.4									
4.6									
4.8									
5.0									
5.2		increased clay content for 0.15m below 5.2m							
5.4		wet below 5.6m							
5.6									
5.8									
6.0									
6.2									
6.4									
6.6									
6.8		increased coarse sand content below 6.7m							
7.0									
7.2									
7.4									
7.6									

End of borehole at 7.60 m

Screened interval from 4.6 m to 7.6 m below surface.
dry on 28 May, 2019

INVESTIG. METHOD: Geoprobe 7822 DT

INVESTIG. DATE: May 23, 2019

LOGGED BY: OWM HOLE DIAM (mm): 150

Sample Notes  Macro Core Sampler

CLIENT: Grant Thornton Ltd.

PROJECT: 36 Mulcaster Street, Barrie, ON

WELL RECORD

PGL PROJECT NO: 5717-01.01

SURFACE ELEVATION: n/a

WELL NO:

BH103M

DEPTH (m)	SOIL TYPE	SOIL DESCRIPTION	SAMPLE TYPE	LABORATORY ANALYSES	● PID READING (ppmv) ● ■ VAPOUR READING (ppmv) ■	WATER LEVEL	WELL COMPLETION	COMPLETION NOTES	ELEVATION (m)
0.2		ASPHALT						Flushmount	
0.4		SAND (FILL)						J Plug	
0.6		with gravel, trace brick debris, brown, dry to moist						Cement	
0.8		some rocks for 0.15m below 0.9m						Silica Sand	
1.0									
1.2									
1.4									
1.6									
1.8									
2.0									
2.2		some rocks for 0.15m below 2.1m							
2.4		no bricks, debris below 2.3m							
2.6		white and brown fine grained sand for 0.9m below							
2.8		2.4m							
3.0									
3.2		organics for 0.1m below 3.4m							
3.4									
3.6		SAND							
3.8		fine grained, trace clay, white and brown, moist							
4.0		coarse grained sand for 0.15m below 4.0m							
4.2									
4.4									
4.6									
4.8									
5.0		wet below 5.3m							
5.2									
5.4									
5.6									
5.8									
6.0									
6.2									
6.4		increased coarse sand for 0.3m below 6.4m							
6.6		moist below 6.4m							
6.8		increased gravel content for 0.3m below 6.7m							
7.0									
7.2									
7.4									
7.6									

End of borehole at 7.60 m

Screened interval from 4.6 m to 7.6 m below surface.
dry on 28 May, 2019

INVESTIG. METHOD: Geoprobe 7822 DT

INVESTIG. DATE: May 23, 2019

LOGGED BY: OWM HOLE DIAM (mm): 150

Sample Notes  Macro Core Sampler

CLIENT: Grant Thornton Ltd.

PROJECT: 36 Mulcaster Street, Barrie, ON

BOREHOLE RECORD

PGL PROJECT NO: 5717-01.01

SURFACE ELEVATION: n/a

BOREHOLE NO:

BH104

DEPTH (m)	SOIL TYPE	SOIL DESCRIPTION	SAMPLE TYPE	LABORATORY ANALYSES	● PID READING (ppmv) ● ■ VAPOUR READING (ppmv) ■	WELL COMPLETION	COMPLETION NOTES	ELEVATION (m)
0.2		ASPHALT		BH104-01	■<25		Bentonite	
0.4		SAND (FILL)						
0.6		with gravel, trace organics, trace debris, brown, moist						
0.8								
1.0		no organics, reduced gravel below 1.1m		BH104-02:	■<25			
1.2				Metals				
1.4								
1.6		moist to wet below 1.8m		BH104-03	■<25			
1.8								
2.0		trace black staining, some oxidation for 0.6m below 2.4m		BH104-04:	■<25			
2.2				BTEX				
2.4				PAHs				
2.6				PHCs				
2.8		some black staining for 0.3m below 3.4m		BH104-05	■<25			
3.0		some rocks for 0.1m below 3.7m		BH104-06	■<25			
3.2		SAND						
3.4		fine grained, brown, moist						
3.6								
3.8		some organics for 0.3m below 4.9m		BH104-07	■<25			
4.0								
4.2								
4.4								
4.6								
4.8								
5.0				BH104-08	■<25			
5.2								
5.4		wet below 5.5m		BH104-09	■<25			
5.6								
5.8								
6.0								

End of borehole at 6.10 m

INVESTIG. METHOD: Geoprobe 7822 DT

INVESTIG. DATE: May 23, 2019

LOGGED BY: OWM HOLE DIAM (mm): 50

Sample Notes  Macro Core Sampler

PGL PROJECT NO: 5717-01.01

SURFACE ELEVATION: n/a

WELL NO:

BH201M

PGL MULTI-TEST VAPOR LOG 2015 5717-01.GPJ PGL_DF_STD_2016.GDT 6/10/19

Screened interval from 10.7 m to 13.7 m below surface.
GW 8.70 mbgs
(6/3/2019)

LOGGED BY: OWM HOLE DIAM (mm): 250

Sample Notes  Macro Core Sampler

PGL PROJECT NO: 5717-01.01

SURFACE ELEVATION: n/a

WELL NO:

BH202M

PGL MULTI-TEST VAPOR LOG 2015 5717-01.GPJ PGL DF STD 2016.GDT 6/10/19

APPENDIX A3

LOG OF BOREHOLE BH 1

REF. NO.: SP20-666-20

PROJECT: Hydrogeological and Environmental Investigation

Method: Hollow Stem Auger

ENCL NO.: 2

CLIENT: Vitmont Holdings (Barrie) Inc.

Diameter: 200 mm

PROJECT LOCATION: 79 Collier Street, ON

Date: Jul-16-2020

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT				POCKET PEN. (C _u) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)	
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)							
233.0								20	40	60	80	100			
232.9	TOPSOIL: 150 mm thick														
0.2	FILL: sandy silt, dark brown, brick debris, some stone		1	SS											
	sand, brick debris		2	SS											
	piece of gravel and some stones, white/grey		3	SS											SS2 - PHCs/VOCs
230.9															
2.1	END OF BOREHOLE:														
	Note:														

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+³, ×³: Numbers refer to Sensitivity

○ s=3% Strain at Failure

LOG OF BOREHOLE MW 2

REF. NO.: SP20-666-20

PROJECT: Hydrogeological and Environmental Investigation

Method: Hollow Stem Auger

CLIENT: Vitmont Holdings (Barrie) Inc.

Diameter: 200 mm

ENCL NO.: 3

PROJECT LOCATION: 79 Collier Street, ON

Date: Jul-15-2020

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC NATURAL LIQUID LIMIT MOISTURE LIMIT CONTENT		POCKET PEN (Cu) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)		WATER CONTENT (%)				
231.8								20 40 60 80 100						GR SA SI CL
230.0	ASPHALT: 70 mm thick			AUGER				○ UNCONFINED	+	FIELD VANE				
	FILL: sand, some stone, trace silt, brown		1	SS				● QUICK TRIAXIAL	x	& Sensitivity (REM)				
	pieces of brick		2	SS			231			FIELD VANE				
			3	SS			230			& Sensitivity (NAT)				
229.5														
2.3	SAND: brown, moist		4	SS			229							
	coarse gravel, white/grey		5	SS										
	brown, moist		6	SS			228							
			7	SS			227							
			8	SS			226							
	very moist, coarse sand		9	SS										
	white/grey, dry		10	SS			225							
	some gravel		11	SS			224							
	brown, moist		12	SS			223							
	End of spoon sampling													
			13	AUGER			222							

W. L. 222.3 m
Jul 27, 2020

222

W. L. 222.3 m
Jul 27, 2020

Continued Next Page

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+ 3, × 3: Numbers refer to Sensitivity

○ s=3% Strain at Failure

LOG OF BOREHOLE MW 2

REF. NO.: SP20-666-20

PROJECT: Hydrogeological and Environmental Investigation

Method: Hollow Stem Auger

ENCL NO.: 3

CLIENT: Vitmont Holdings (Barrie) Inc.

Diameter: 200 mm

PROJECT LOCATION: 79 Collier Street, ON

Date: Jul-15-2020

SOIL PROFILE				SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT				PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT			POCKET PEN (Cu) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m	SHEAR STRENGTH (kPa)				WATER CONTENT (%)								
										20 40 60 80 100	20 40 60 80 100	10 20 30				GR SA SI CL		
221.1	SAND: brown, moist(Continued)																	
10.7	END OF BOREHOLE:																	
	Note: 1. Monitoring well was installed upon completion of drilling. 2. Monitoring well was covered with flush mount well cover protection. 3. Groundwater level observation(s): Date: Depth (m): July 16, 2020 9.48 July 27, 2020 9.51																	

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+³, ×³: Numbers refer to Sensitivity

○ s=3% Strain at Failure

LOG OF BOREHOLE MW 3

REF. NO.: SP20-666-20

PROJECT: Hydrogeological and Environmental Investigation

Method: Hollow Stem Auger

CLIENT: Vitmont Holdings (Barrie) Inc.

Diameter: 200 mm

ENCL NO.: 4

PROJECT LOCATION: 79 Collier Street, ON

Date: Jul-15-2020

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT		NATURAL MOISTURE CONTENT		LIQUID LIMIT		POCKET PEN (Cu) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)		FIELD VANE & Sensitivity (REM)		w _p		w				
232.1								○ UNCONFINED ● QUICK TRIAXIAL		+		×						GR SA SI CL
232.0	ASPHALT: 100 mm thick		1	SS			232											
0.1	FILL: sandy silt, some cobbles, trace stone, trace clay																	
	more stones and cobbles		2	SS			231											
230.6																		
1.5	SAND: trace stone, white/brown, moist		3	SS			230											
			4	SS														
			5	SS			229											
	fine sand, dark gery, very moist		6	SS			228											
			7	SS			227											
			8	SS			226											
			9	SS														
	trace gravel, moist		10	SS			225											
			11	SS			224											
			12	SS														
	End of spoon sampling		13	SS			223											SS13 - PHC/VOC
									</									

W. L. 222.3 m

Continued Next Page

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH
NOTES

+ 3, X 3: Numbers refer
to Sensitivity

○ s=3% Strain at Failure

LOG OF BOREHOLE MW 3

REF. NO.: SP20-666-20

PROJECT: Hydrogeological and Environmental Investigation

Method: Hollow Stem Auger

ENCL NO.: 4

CLIENT: Vitmont Holdings (Barrie) Inc.

Diameter: 200 mm

PROJECT LOCATION: 79 Collier Street, ON

Date: Jul-15-2020

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT				PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT			POCKET PEN. (Cu) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m		SHEAR STRENGTH (kPa)				W _p	W	W _L			
																GR SA SI CL
219.9	SAND: trace gravel, white/brown, moist(Continued)					Jul 27, 2020										
221																
220																
12.2	END OF BOREHOLE:															
	Note: 1. Monitoring well was installed upon completion of drilling. 2. Monitoring well was covered with flush mount well cover protection. 3. Groundwater level observation(s): Date: Depth (m): July 16, 2020 9.88 July 27, 2020 9.82															

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+ 3, × 3: Numbers refer to Sensitivity

○ s=3% Strain at Failure

LOG OF BOREHOLE BH 4

REF. NO.: SP20-666-20

PROJECT: Hydrogeological and Environmental Investigation

Method: Hollow Stem Auger

ENCL NO.: 5

CLIENT: Vitmont Holdings (Barrie) Inc.

Diameter: 200 mm

PROJECT LOCATION: 79 Collier Street, ON

Date: Jul-15-2020

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT w _p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w _L	POCKET PEN. (C _u) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)							
231.1								20 40 60 80 100	20 40 60 80 100						GR SA SI CL
230.0	ASPHALT: 100 mm thick			AUGER			231								SS1 - M&I
0.1	FILL: sand, some stone, trace gravel, brown		1	SS											
	piece of brick		2	SS			230								
229.4															
1.7	SAND:		3	SS											SS3 - PHC/VOC, PAH, PCB
229.0							229								
2.1	END OF BOREHOLE:														
	Note:														

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+³, ×³: Numbers refer to Sensitivity

○ s=3% Strain at Failure

LOG OF BOREHOLE BH 5

REF. NO.: SP20-666-20

PROJECT: Hydrogeological and Environmental Investigation

Method: Hollow Stem Auger

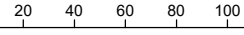
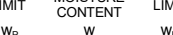
ENCL NO.: 6

CLIENT: Vitmont Holdings (Barrie) Inc.

Diameter: 200 mm

PROJECT LOCATION: 79 Collier Street, ON

Date: Jul-16-2020

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT		POCKET PEN. (C _u) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)						
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)		WATER CONTENT (%)										
230.8 230.1	ASPHALT: 80 mm thick FILL: sand, some stone, some asphalt, gravel, dark brown		1	SS		AUGER	230							GR SA SI CL						
1			2	SS																
228.7 2.1	some organics, dark brown		3	SS											229					
END OF BOREHOLE:																				
Note:																				

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+³, ×³: Numbers refer to Sensitivity

○ s=3% Strain at Failure

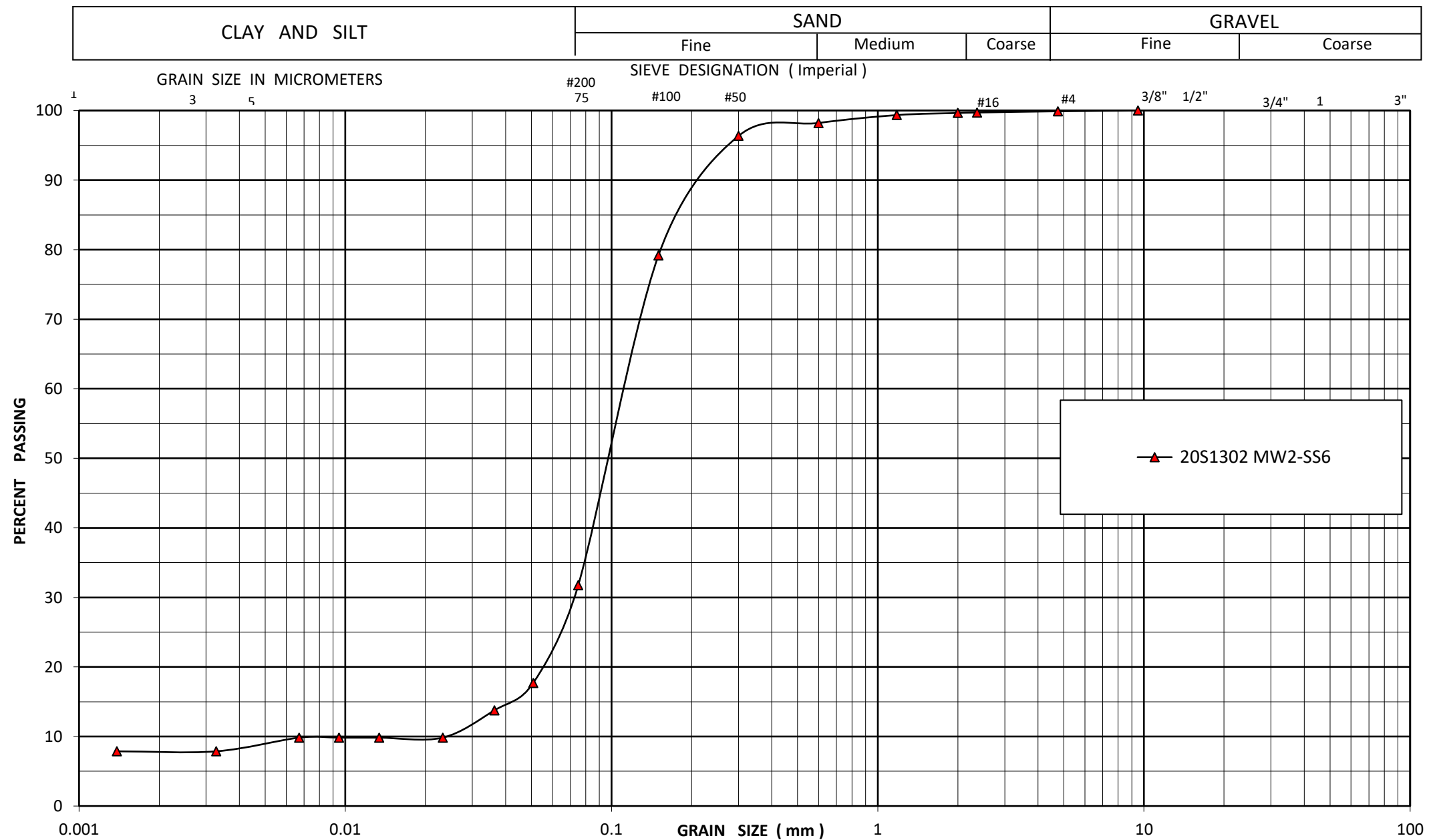
APPENDIX B



Geotechnical Hydrogeological & Environmental Solutions

GRAIN SIZE DISTRIBUTION

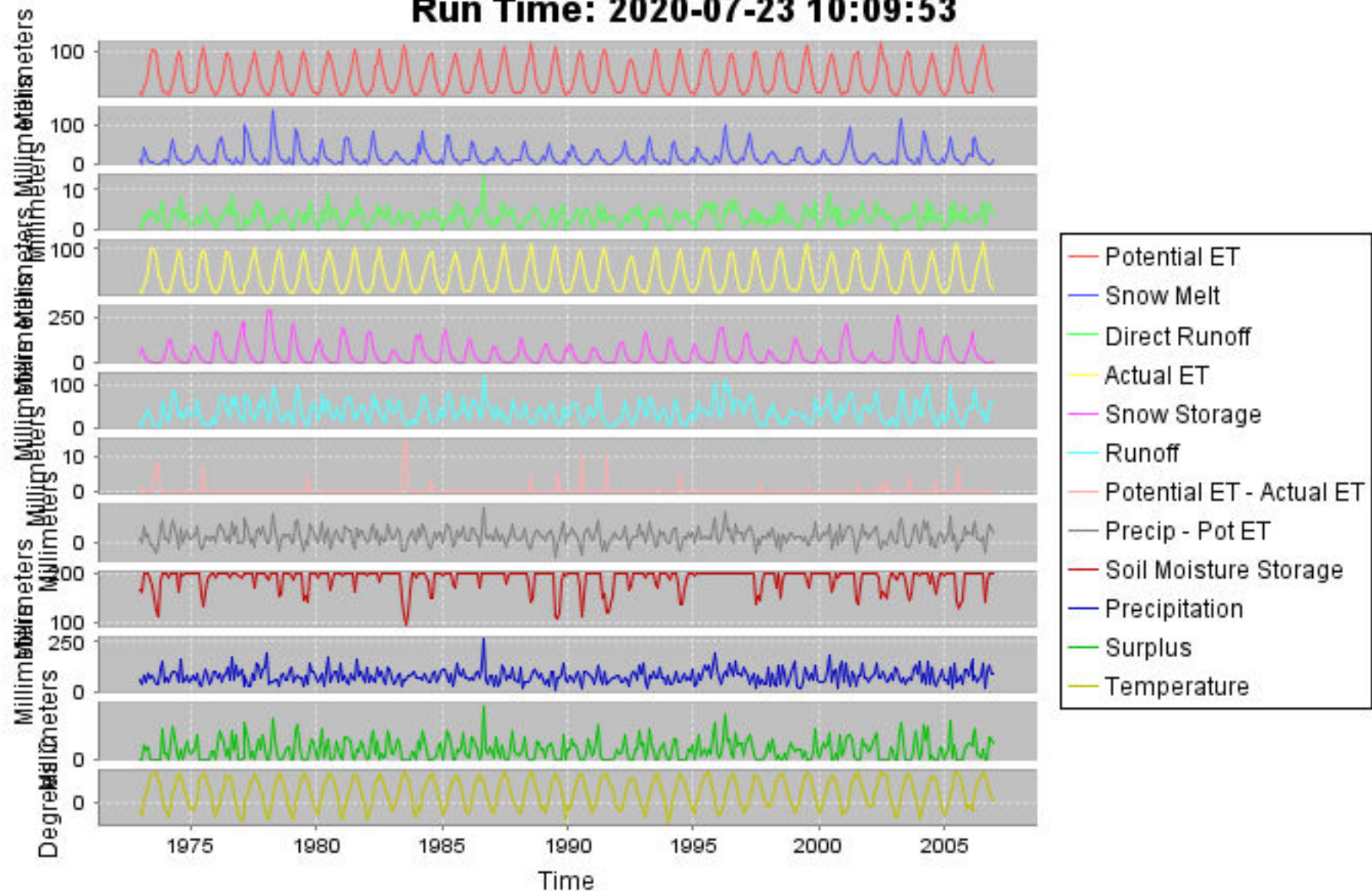
UNIFIED SOIL CLASSIFICATION SYSTEM



Project No.	:	SP20-666-00
Date	:	21 August 2020
Figure No.	:	

APPENDIX C

Run Time: 2020-07-23 10:09:53



THORNTHWAITE DATA

				Soil			Snow		
Date	PET	P	P-PET	Moisture	AET	PET-AET	Storage	Surplus	ROtotal
=====	=====	=====	=====	=====	=====	=====	=====	=====	=====
Jan-73	10.4	64.5	15.9	165.9	10.4	0	37.2	0	13.7
Feb-73	8.6	44.2	-6.2	160.8	7.6	1.1	78.8	0	6.4
Mar-73	23.7	81.5	86.6	200	23.7	0	46.3	47.4	30.6
Apr-73	34	49.8	36.4	200	34	0	23.2	36.4	34.1
May-73	54.5	91.4	43.9	200	54.5	0	11.6	43.9	42.3
Jun-73	91.3	76.2	-13.2	186.8	91.3	0	5.8	0	22.7
Jul-73	103	87.6	-14	173.8	102.1	0.9	0	0	13.8
Aug-73	97.5	39.4	-60.1	121.6	89.7	7.9	0	0	6.7
Sep-73	54.3	38.9	-17.4	111	47.5	6.8	0	0	4.3
Oct-73	36.1	113.8	72	183	36.1	0	0	0	6.9
Nov-73	17.2	156.5	125.7	200	17.2	0	6.3	108.7	62.2
Dec-73	10.3	54.1	16.1	200	10.3	0	33	16.1	36.5
Jan-74	9.9	69.1	17.7	200	9.9	0	73.7	17.7	27.5
Feb-74	8.2	52.8	-8.2	191.8	8.2	0	126.5	0	13.3
Mar-74	17	81.3	65	200	17	0	123.7	56.9	37.2
Apr-74	34.9	99.6	121.6	200	34.9	0	61.9	121.6	83.3
May-74	51.5	102.9	77.1	200	51.5	0	30.9	77.1	82.9
Jun-74	81.7	96.5	25.4	200	81.7	0	15.5	25.4	56.4
Jul-74	99.2	55.1	-39.1	160.9	99.2	0	7.7	0	28.5
Aug-74	86.2	161	74.5	200	86.2	0	0	35.4	38.6
Sep-74	48.9	47.8	-3.5	196.5	48.9	0	0	0	17.7
Oct-74	28.3	67.8	36.1	200	28.3	0	0	32.6	27.3
Nov-74	17.6	86.1	64.4	200	17.6	0	0	64.4	48.3
Dec-74	12.8	51.3	23.7	200	12.8	0	13.3	23.7	35.5
Jan-75	10.7	66	20.8	200	10.7	0	46.7	20.8	28.5
Feb-75	10.9	82.8	29.4	200	10.9	0	87.9	29.4	29.7
Mar-75	16.2	63.8	39.6	200	16.2	0	94.4	39.6	35.5
Apr-75	25.4	88.4	89.4	200	25.4	0	64.3	89.4	65.4
May-75	72.5	42.2	-0.2	199.8	72.5	0	32.2	0	33
Jun-75	90.2	31.5	-44.2	155.6	90.2	0.1	16.1	0	17
Jul-75	106.2	71.6	-30.2	132.1	99.5	6.7	8	0	11.3
Aug-75	87.2	112	27.2	159.3	87.2	0	0	0	9.5
Sep-75	48	79.8	27.8	187.1	48	0	0	0	5.9
Oct-75	34.1	43.9	7.6	194.7	34.1	0	0	0	3.2
Nov-75	21.7	58.7	34.1	200	21.7	0	0	28.8	17.8
Dec-75	9.6	103.1	28	200	9.6	0	64.1	28	22.9
Jan-76	7.2	101.6	-7.2	192.8	7.2	0	165.7	0	10.7
Feb-76	12	72.6	62	200	12	0	162.8	54.7	34.3
Mar-76	18.8	95.5	102.2	200	18.8	0	134.2	102.2	70.5
Apr-76	36.9	55.6	83	200	36.9	0	67.1	83	78
May-76	53.2	87.1	63.1	200	53.2	0	33.6	63.1	73.5
Jun-76	93.1	91.9	11	200	93.1	0	16.8	11	44.7
Jul-76	93.3	123.4	32.4	200	93.3	0	8.4	32.4	42.4
Aug-76	81	67.1	-8.8	191.2	81	0	0	0	21.5

THORNTHWAITE DATA

				Soil			Snow		
Date	PET	P	P-PET	Moisture	AET	PET-AET	Storage	Surplus	ROtotal
=====	=====	=====	=====	=====	=====	=====	=====	=====	=====
Sep-76	49.8	173.2	114.7	200	49.8	0	0	105.9	70.7
Oct-76	26.3	66.5	36.9	200	26.3	0	0	36.9	52.8
Nov-76	14.1	130.3	84.6	200	14.1	0	27.1	84.6	71.5
Dec-76	7.9	79.5	-3.1	196.9	7.9	0	101.6	0	33.7
Jan-77	6.6	111.2	-6.6	190.4	6.5	0.1	212.8	0	16.8
Feb-77	9.7	36.6	16.2	200	9.7	0	223.3	6.7	12
Mar-77	21.7	78.4	135.4	200	21.7	0	141.4	135.4	76.7
Apr-77	36.4	34.9	67.4	200	36.4	0	70.7	67.4	72.2
May-77	67.3	35.4	1.7	200	67.3	0	35.3	1.7	37.8
Jun-77	78.7	88.9	23.4	200	78.7	0	17.7	23.4	34.2
Jul-77	100.5	63.5	-31.3	168.7	100.5	0	8.8	0	18
Aug-77	78	140.2	64	200	78	0	0	32.7	30.8
Sep-77	52.7	133	73.7	200	52.7	0	0	73.7	55.4
Oct-77	29.8	70.2	36.9	200	29.8	0	0	36.9	46.3
Nov-77	18.4	113.8	89.8	200	18.4	0	0	89.8	72
Dec-77	10	125.7	43.4	200	10	0	70.2	43.4	56.9
Jan-78	7.6	193	-7.6	192.4	7.6	0	263.2	0	27.4
Feb-78	7.5	38.8	-7.5	185.2	7.2	0.3	302	0	13.7
Mar-78	14.5	55.8	57.5	200	14.5	0	284.8	42.7	29.1
Apr-78	27.9	50.8	152.7	200	27.9	0	152.6	152.7	92.9
May-78	62.5	60	70.8	200	62.5	0	76.3	70.8	83.7
Jun-78	78.7	62.6	18.9	200	78.7	0	38.2	18.9	52.9
Jul-78	99.2	32.8	-49	151	99.2	0	19.1	0	26.5
Aug-78	85.6	87	6.6	157.6	85.6	0	9.5	0	16.8
Sep-78	51.1	93.4	47.2	200	51.1	0	0	4.8	13.3
Oct-78	30.3	61.8	28.4	200	30.3	0	0	28.4	21.6
Nov-78	16.8	59	39.5	200	16.8	0	0	39.5	31.7
Dec-78	10.9	101.6	42.9	200	10.9	0	45.6	42.9	38.2
Jan-79	8.1	123.3	-5.1	194.9	8.1	0	165.8	0	18.1
Feb-79	6.9	55	-6.9	188.1	6.8	0.2	220.8	0	9
Mar-79	20.4	71	117.5	200	20.4	0	151.3	105.6	59.9
Apr-79	31.2	87.2	127.3	200	31.2	0	75.6	127.3	96.6
May-79	56.9	70.4	47.8	200	56.9	0	37.8	47.8	73.6
Jun-79	84.3	70.3	1.4	200	84.3	0	18.9	1.4	39.2
Jul-79	99.2	36	-55.6	144.4	99.2	0	9.5	0	19.7
Aug-79	80.5	83.4	8.2	152.6	80.5	0	0	0	13.1
Sep-79	54	39.8	-16.2	140.3	50.2	3.8	0	0	6.5
Oct-79	30.1	140	102.9	200	30.1	0	0	43.1	30.8
Nov-79	18.9	99.2	75.3	200	18.9	0	0	75.3	54.5
Dec-79	12.2	99.8	54.2	200	12.2	0	30.6	54.2	54.7
Jan-80	9.9	71.8	18.3	200	9.9	0	73.3	18.3	36
Feb-80	8.3	49	-8.3	191.7	8.3	0	122.3	0	17.5
Mar-80	16.6	70.2	54.6	200	16.6	0	119.5	46.3	33.6
Apr-80	34.2	93.4	114.2	200	34.2	0	59.8	114.2	77.7

THORNTHWAITE DATA

				Soil			Snow		
Date	PET	P	P-PET	Moisture	AET	PET-AET	Storage	Surplus	ROtotal
=====	=====	=====	=====	=====	=====	=====	=====	=====	=====
May-80	62.9	36.8	2	200	62.9	0	29.9	2	39.4
Jun-80	70.4	103.2	42.6	200	70.4	0	14.9	42.6	45.2
Jul-80	98.6	171.6	71.9	200	98.6	0	7.5	71.9	64.5
Aug-80	90.5	51.2	-34.4	165.6	90.5	0	0	0	30.5
Sep-80	52.4	99.2	41.9	200	52.4	0	0	7.5	22.7
Oct-80	26.9	98.6	66.7	200	26.9	0	0	66.7	47.1
Nov-80	15.8	55.6	31.6	200	15.8	0	5.9	31.6	39.2
Dec-80	8.2	144.8	10.4	200	8.2	0	131.4	10.4	24.3
Jan-81	6.7	61	-6.7	193.3	6.7	0	192.4	0	11.8
Feb-81	12.9	85.2	89.6	200	12.9	0	172.9	82.9	49.6
Mar-81	19.4	51.6	77.9	200	19.4	0	125.4	77.9	64.4
Apr-81	35.3	46.4	71.5	200	35.3	0	62.7	71.5	69.4
May-81	55.5	97.6	68.6	200	55.5	0	31.4	68.6	72.7
Jun-81	83.2	71.8	0.7	200	83.2	0	15.7	0.7	37.8
Jul-81	101.7	58.6	-38.2	161.8	101.7	0	7.8	0	20
Aug-81	84	159.8	75.6	200	84	0	0	37.4	35.2
Sep-81	50.1	80.4	26.2	200	50.1	0	0	26.2	30.8
Oct-81	27.5	101.4	68.9	200	27.5	0	0	68.9	52.9
Nov-81	17.4	70	49.4	200	17.4	0	0	49.4	51.9
Dec-81	11.2	55	20	200	11.2	0	22.5	20	35.6
Jan-82	7	120	-7	193	7	0	142.5	0	17.1
Feb-82	9.4	49	9.4	200	9.4	0	172.4	2.4	10.1
Mar-82	16.7	79	73.1	200	16.7	0	159.5	73.1	43.4
Apr-82	29.5	58.8	106.1	200	29.5	0	79.8	106.1	76.7
May-82	68.6	50.2	19	200	68.6	0	39.9	19	48.9
Jun-82	74	123.2	63	200	74	0	19.9	63	60.9
Jul-82	101.7	78	-17.6	182.4	101.7	0	10	0	31.2
Aug-82	73.3	103.4	34.9	200	73.3	0	0	17.2	27.5
Sep-82	53	62.8	6.7	200	53	0	0	6.7	17.6
Oct-82	33.5	47.2	11.4	200	33.5	0	0	11.4	15.3
Nov-82	18.7	126.8	101.8	200	18.7	0	0	101.8	63.7
Dec-82	13.8	108.4	71.4	200	13.8	0	19.3	71.4	68.3
Jan-83	10.3	72	20.8	200	10.3	0	59.1	20.8	43.6
Feb-83	11.8	43.2	22.1	200	11.8	0	67.6	22.1	33.2
Mar-83	19.8	53.4	44.9	200	19.8	0	54.4	44.9	40.5
Apr-83	31.8	83.6	74.8	200	31.8	0	27.2	74.8	60.9
May-83	50.9	93.8	51.8	200	50.9	0	13.6	51.8	59
Jun-83	85.9	28.2	-52.3	147.7	85.9	0	6.8	0	28.5
Jul-83	111.6	62.8	-45.2	114.4	99.8	11.8	0	0	16.7
Aug-83	94	63.6	-33.6	95.2	79.6	14.4	0	0	10
Sep-83	59.3	84.4	20.9	116.1	59.3	0	0	0	7.6
Oct-83	32.3	82.4	46	162.1	32.3	0	0	0	5.8
Nov-83	17.1	89	67.8	200	17.1	0	0	29.9	19.9
Dec-83	9	104.4	18.6	200	9	0	75.8	18.6	18.2

THORNTHWAITE DATA

				Soil			Snow		
Date	PET	P	P-PET	Moisture	AET	PET-AET	Storage	Surplus	ROtotal
=====	=====	=====	=====	=====	=====	=====	=====	=====	=====
Jan-84	7.6	72.6	-7.6	192.4	7.6	0	148.4	0	8.6
Feb-84	13.1	72	72	200	13.1	0	133.4	64.4	38.4
Mar-84	14.1	77.4	33.9	200	14.1	0	161.7	33.9	36.3
Apr-84	36.2	64.8	106.2	200	36.2	0	80.9	106.2	73.9
May-84	51.2	89.4	74.1	200	51.2	0	40.4	74.1	76.9
Jun-84	85.9	49.8	-18.3	181.7	85.9	0	20.2	0	38.7
Jul-84	96.2	52.2	-36.5	148.5	92.8	3.3	10.1	0	20.7
Aug-84	92.8	91	-1.3	147.5	92.5	0.3	5.1	0	13.6
Sep-84	49.2	106.8	57.3	200	49.2	0	0	4.8	12.3
Oct-84	34.7	51.8	14.5	200	34.7	0	0	14.5	13.3
Nov-84	17.5	69.2	48.5	200	17.5	0	0	48.5	32.8
Dec-84	13.2	98.6	59.8	200	13.2	0	22.3	59.8	48
Jan-85	8.1	112.6	-5.5	194.5	8.1	0	132.2	0	22.4
Feb-85	10.6	113.4	49.2	200	10.6	0	184.3	43.6	34.6
Mar-85	19	84.2	102	200	19	0	144.9	102	70.2
Apr-85	36.2	51.6	85.2	200	36.2	0	72.4	85.2	78.9
May-85	61.3	88.4	58.9	200	61.3	0	36.2	58.9	72
Jun-85	73.1	33.2	-23.4	176.6	73.1	0	18.1	0	35.5
Jul-85	93.8	83.4	-5.6	171.7	93.2	0.7	9.1	0	21.1
Aug-85	80.5	144.2	65.6	200	80.5	0	0	37.2	34.3
Sep-85	58.2	89.4	26.8	200	58.2	0	0	26.8	31.4
Oct-85	33.3	78.8	41.6	200	33.3	0	0	41.6	38.2
Nov-85	17.2	116.4	93.8	200	17.2	0	0	93.8	69.4
Dec-85	9.8	71	18.5	200	9.8	0	41.5	18.5	42.4
Jan-86	9.3	75	12	200	9.3	0	94.6	12	27.3
Feb-86	9.3	58	6.1	200	9.3	0	136.9	6.1	16.7
Mar-86	19.8	68.8	81	200	19.8	0	102.5	81	51.1
Apr-86	38.3	66.4	76	200	38.3	0	51.2	76	65.7
May-86	66.9	92.6	46.7	200	66.9	0	25.6	46.7	59.2
Jun-86	77.3	105	35.3	200	77.3	0	12.8	35.3	50.2
Jul-86	101.7	70	-28.8	171.2	101.7	0	6.4	0	26
Aug-86	78	128	50	200	78	0	0	21.2	28.2
Sep-86	51.4	263.2	198.6	200	51.4	0	0	198.6	123.4
Oct-86	31.1	66.8	32.4	200	31.1	0	0	32.4	74.6
Nov-86	15.9	38	20.5	200	15.9	0	0	20.5	47.5
Dec-86	12.3	80.6	41.8	200	12.3	0	24.1	41.8	46.2
Jan-87	10.3	80.4	24.8	200	10.3	0	68.3	24.8	35.5
Feb-87	9.7	36.4	4.8	200	9.7	0	89.9	4.8	19.9
Mar-87	20.2	83.6	78	200	20.2	0	72.3	78	51.8
Apr-87	41.3	34.4	27.6	200	41.3	0	36.1	27.6	39.9
May-87	65.2	52	2.2	200	65.2	0	18.1	2.2	22.8
Jun-87	89.7	134	46.7	200	89.7	0	9	46.7	40.1
Jul-87	108.9	111.6	6.2	200	108.9	0	0	6.2	25.4
Aug-87	84.6	66	-21.9	178.1	84.6	0	0	0	13.2

THORNTHWAITE DATA

				Soil			Snow		
Date	PET	P	P-PET	Moisture	AET	PET-AET	Storage	Surplus	ROtotal
=====	=====	=====	=====	=====	=====	=====	=====	=====	=====
Sep-87	55.7	78.2	18.6	196.7	55.7	0	0	0	8.9
Oct-87	28.3	76.8	44.6	200	28.3	0	0	41.4	27
Nov-87	17.4	123.6	100.5	200	17.4	0	0	100.5	67.6
Dec-87	12.9	59.8	30	200	12.9	0	15.1	30	47.8
Jan-88	9.8	51.4	8.9	200	9.8	0	47.1	8.9	28.1
Feb-88	9.4	119.6	16.1	200	9.4	0	140.3	16.1	22.6
Mar-88	17.2	25.2	35.5	200	17.2	0	112.2	35.5	29.3
Apr-88	32.8	57.2	77.6	200	32.8	0	56.1	77.6	56
May-88	66.1	54.4	13.7	200	66.1	0	28	13.7	36.1
Jun-88	81.7	48.8	-21.3	178.7	81.7	0	14	0	19.1
Jul-88	114.4	68.6	-42.2	140.9	109.9	4.5	7	0	11.8
Aug-88	92.2	99.8	9.6	150.5	92.2	0	0	0	9.2
Sep-88	52.7	113	54.7	200	52.7	0	0	5.2	10.3
Oct-88	27.3	95.4	63.3	200	27.3	0	0	63.3	38.8
Nov-88	19.4	77	53.7	200	19.4	0	0	53.7	47.7
Dec-88	10.6	91.8	35.2	200	10.6	0	44.2	35.2	41.3
Jan-89	11.5	64	32.5	200	11.5	0	62.8	32.5	37.4
Feb-89	9.4	47.2	3.7	200	9.4	0	96.6	3.7	20.2
Mar-89	16	62	39.2	200	16	0	102	39.2	30.9
Apr-89	30.3	29.4	48.7	200	30.3	0	51	48.7	40.6
May-89	59.8	100	60.7	200	59.8	0	25.5	60.7	54.9
Jun-89	86.9	102.6	23.3	200	86.9	0	12.8	23.3	41.7
Jul-89	106.9	12.2	-88.9	111.1	106.9	0	6.4	0	18.9
Aug-89	84.6	69.9	-11.8	104.5	79.3	5.2	0	0	12.6
Sep-89	53	72.4	15.8	120.3	53	0	0	0	8.2
Oct-89	32.7	97.6	60.1	180.4	32.7	0	0	0	7.2
Nov-89	15.7	145.8	107.9	200	15.7	0	16.3	88.2	51.2
Dec-89	6.6	58	-6.6	193.4	6.6	0	74.3	0	22.6
Jan-90	12.8	55.4	44.7	200	12.8	0	70.7	38.1	31.9
Feb-90	11.1	84	37.2	200	11.1	0	104.9	37.2	35.2
Mar-90	20.3	68.4	72.1	200	20.3	0	78.4	72.1	55.4
Apr-90	37.8	54.4	53.1	200	37.8	0	39.2	53.1	55.7
May-90	55.2	87.2	47.3	200	55.2	0	19.6	47.3	54.5
Jun-90	85.3	106	25.2	200	85.3	0	9.8	25.2	43
Jul-90	98.6	62.8	-29.1	170.9	98.6	0	0	0	22
Aug-90	88.3	20.8	-68.6	112.3	78.3	10	0	0	10.5
Sep-90	52.4	99.2	41.9	154.2	52.4	0	0	0	9.7
Oct-90	31.3	104	67.5	200	31.3	0	0	21.7	18.4
Nov-90	19	97.8	73.9	200	19	0	0	73.9	48.4
Dec-90	12.3	85	44.8	200	12.3	0	25.4	44.8	46.6
Jan-91	9.3	71.6	9.8	200	9.3	0	77.3	9.8	27.6
Feb-91	12.1	42.2	28	200	12.1	0	78.4	28	28.4
Mar-91	20.2	85	75	200	20.2	0	65.2	75	54.3
Apr-91	39.3	136.6	123.1	200	39.3	0	32.6	123.1	94

THORNTHWAITE DATA

				Soil			Snow		
Date	PET	P	P-PET	Moisture	AET	PET-AET	Storage	Surplus	ROtotal
=====	=====	=====	=====	=====	=====	=====	=====	=====	=====
May-91	72.9	72.4	12.1	200	72.9	0	16.3	12.1	53.3
Jun-91	94.8	38.6	-50	150	94.8	0	8.2	0	26.8
Jul-91	102.3	107.4	7.8	157.9	102.3	0	0	0	17.8
Aug-91	91.7	43.4	-50.4	118	81	10.6	0	0	8.4
Sep-91	51.4	56	1.8	119.9	51.4	0	0	0	5.9
Oct-91	33.5	68.6	31.7	151.5	33.5	0	0	0	5
Nov-91	16.6	68.4	48.8	200	16.6	0	0	0.3	3.9
Dec-91	11	87.2	36.5	200	11	0	37.8	36.5	20.7
Jan-92	9.7	86.2	20.6	200	9.7	0	92.7	20.6	20.6
Feb-92	10.6	50.6	20.8	200	10.6	0	111.3	20.8	20.9
Mar-92	16.2	55.6	40.4	200	16.2	0	109	40.4	31.6
Apr-92	31.2	69.8	89.6	200	31.2	0	54.5	89.6	63.4
May-92	58.4	58.2	24.2	200	58.4	0	27.2	24.2	45
Jun-92	75.4	28.8	-34.4	165.6	75.4	0	13.6	0	22.5
Jul-92	82.9	87	6.6	172.2	82.9	0	6.8	0	14.9
Aug-92	74.2	100.2	27.8	199.9	74.2	0	0	0	10.3
Sep-92	52.4	93.8	36.8	200	52.4	0	0	36.7	25.7
Oct-92	28.3	64.4	32.9	200	28.3	0	0	32.9	30.1
Nov-92	16.9	132.4	102.4	200	16.9	0	7.1	102.4	70.6
Dec-92	12	89.6	47.8	200	12	0	34.5	47.8	58.7
Jan-93	10.4	147.4	55.2	200	10.4	0	114	55.2	58
Feb-93	7.9	51	-7.9	192.1	7.9	0	165	0	27.8
Mar-93	16.7	23.2	38	200	16.7	0	132.8	30.2	29.6
Apr-93	33.4	78.2	107.3	200	33.4	0	66.4	107.3	72.1
May-93	56.9	76.4	48.9	200	56.9	0	33.2	48.9	62.3
Jun-93	79.2	99	31.4	200	79.2	0	16.6	31.4	49.9
Jul-93	102.3	75.8	-22	178	102.3	0	8.3	0	26.3
Aug-93	90.5	75.4	-10.6	168.5	89.4	1.2	0	0	15
Sep-93	47.7	121	67.2	200	47.7	0	0	35.8	29.6
Oct-93	29.6	75	41.7	200	29.6	0	0	41.7	36.3
Nov-93	17	76.4	55.9	200	17	0	0	55.9	47.7
Dec-93	11.1	40.4	11.2	200	11.1	0	17.2	11.2	28.7
Jan-94	6	81.3	-6	194	6	0	98.5	0	13.9
Feb-94	8.2	38.2	-8.2	186.1	8	0.2	136.7	0	6.9
Mar-94	17.7	44.6	50.2	200	17.7	0	112.1	36.3	22.9
Apr-94	36.2	58.8	75.7	200	36.2	0	56.1	75.7	51.6
May-94	54.2	103.2	71.9	200	54.2	0	28	71.9	65.4
Jun-94	88	53.6	-23.1	176.9	88	0	14	0	32.8
Jul-94	102.3	53.6	-44.4	137.6	97.2	5.1	7	0	17.7
Aug-94	78	70.2	-4.3	134.7	76.7	1.3	0	0	11
Sep-94	54.3	89.4	30.6	165.2	54.3	0	0	0	8.2
Oct-94	33.3	58.4	22.2	187.4	33.3	0	0	0	4.8
Nov-94	19.6	72	48.8	200	19.6	0	0	36.2	22.6
Dec-94	12.9	58	28.7	200	12.9	0	14.6	28.7	25.7

THORNTHWAITE DATA

				Soil			Snow		
Date	PET	P	P-PET	Moisture	AET	PET-AET	Storage	Surplus	ROtotal
=====	=====	=====	=====	=====	=====	=====	=====	=====	=====
Jan-95	11.1	113.8	48.5	200	11.1	0	66.5	48.5	38.4
Feb-95	8.7	33.6	-5.1	194.9	8.7	0	96.4	0	18.2
Mar-95	20.9	38	47.1	200	20.9	0	64.9	42	31.5
Apr-95	28.4	90.2	86.9	200	28.4	0	35.4	86.9	62.8
May-95	59.1	58	13.7	200	59.1	0	17.7	13.7	39
Jun-95	96.6	128.6	34.4	200	96.6	0	8.9	34.4	41.7
Jul-95	103.6	115.8	15.2	200	103.6	0	0	15.2	31
Aug-95	95.7	133.8	31.4	200	95.7	0	0	31.4	35
Sep-95	48.3	71.6	19.7	200	48.3	0	0	19.7	27.6
Oct-95	35.2	129	87.4	200	35.2	0	0	87.4	62.1
Nov-95	14.3	196	136.5	200	14.3	0	38.3	136.5	102.9
Dec-95	9	111.6	24.3	200	9	0	115.6	24.3	61.3
Jan-96	8.4	74.6	0.3	200	8.4	0	181.4	0.3	30.4
Feb-96	9.8	46.2	17.9	200	9.8	0	199.5	17.9	24.5
Mar-96	16	81.2	72.4	200	16	0	190.4	72.4	50.1
Apr-96	29.5	107	167.3	200	29.5	0	95.2	167.3	113.1
May-96	55.5	79.8	67.9	200	55.5	0	47.6	67.9	91.8
Jun-96	87.5	144.4	73.5	200	87.5	0	23.8	73.5	87.9
Jul-96	92.1	108.2	22.6	200	92.1	0	11.9	22.6	57
Aug-96	87.2	86.8	1.2	200	87.2	0	5.9	1.2	30.7
Sep-96	56.1	152.8	95.1	200	56.1	0	0	95.1	68.4
Oct-96	31.7	88.2	52.1	200	31.7	0	0	52.1	60.8
Nov-96	14.9	91.2	58.3	200	14.9	0	14.6	58.3	60.8
Dec-96	13	85.2	53.8	200	13	0	30.3	53.8	58.3
Jan-97	8.9	120.4	13.1	200	8.9	0	128	13.1	35.1
Feb-97	11.3	105.6	58.9	200	11.3	0	161.6	58.9	48.5
Mar-97	16.6	81	70.6	200	16.6	0	153.4	70.6	60.6
Apr-97	31.2	45.4	88.6	200	31.2	0	76.7	88.6	75.9
May-97	47.9	74	60.8	200	47.9	0	38.4	60.8	70.9
Jun-97	92.5	97.4	19.2	200	92.5	0	19.2	19.2	48.1
Jul-97	96.8	25	-63.5	136.5	96.8	0	9.6	0	22.9
Aug-97	77.1	87.4	15.6	152.1	77.1	0	0	0	15.2
Sep-97	53	44.6	-10.6	144	50.5	2.5	0	0	7.6
Oct-97	30.9	66.6	32.4	176.4	30.9	0	0	0	6
Nov-97	16.6	44.6	26	200	16.6	0	0	2.4	4.5
Dec-97	12.2	45	17.5	200	12.2	0	14.1	17.5	11.3
Jan-98	11.5	123.4	57.9	200	11.5	0	65.4	57.9	36.6
Feb-98	13.5	33.6	27.6	200	13.5	0	57	27.6	31.7
Mar-98	21.1	91.2	76.1	200	21.1	0	47.5	76.1	56.9
Apr-98	37.6	47	30.8	200	37.6	0	23.8	30.8	44.5
May-98	76.7	35	-31.5	168.5	76.7	0	11.9	0	22.8
Jun-98	88.6	134.8	45.4	200	88.6	0	5.9	13.9	24.2
Jul-98	100.5	45.2	-51.6	148.4	100.5	0	0	0	11
Aug-98	89.4	136.6	40.3	188.8	89.4	0	0	0	11.2

THORNTHWAITE DATA

				Soil			Snow		
Date	PET	P	P-PET	Moisture	AET	PET-AET	Storage	Surplus	ROtotal
=====	=====	=====	=====	=====	=====	=====	=====	=====	=====
Sep-98	58.5	94.4	31.1	200	58.5	0	0	19.9	16.9
Oct-98	33.7	35.2	-0.2	199.8	33.7	0	0	0	7.8
Nov-98	18.7	57.2	35.6	200	18.7	0	0	35.4	23.6
Dec-98	13.6	88.8	54.7	200	13.6	0	17.4	54.7	40.8
Jan-99	9.1	148.8	24.4	200	9.1	0	131.4	24.4	32.3
Feb-99	12.3	33	36.3	200	12.3	0	115	36.3	34.5
Mar-99	18.5	21.4	32	200	18.5	0	85.3	32	33.5
Apr-99	36.4	26	30.9	200	36.4	0	42.6	30.9	33.2
May-99	68.1	55.4	5.8	200	68.1	0	21.3	5.8	21.6
Jun-99	94.8	118.8	28.7	200	94.8	0	10.7	28.7	29.7
Jul-99	111.6	92.4	-18.5	181.5	111.6	0	5.3	0	16.5
Aug-99	81.5	65.2	-14.2	168.6	80.2	1.3	0	0	9.2
Sep-99	59.6	94.8	30.4	199	59.6	0	0	0	7.7
Oct-99	31.3	62.8	28.4	200	31.3	0	0	27.4	18.3
Nov-99	19	138.2	112.2	200	19	0	0	112.2	70.6
Dec-99	12	66	30.6	200	12	0	21.6	30.6	49
Jan-00	9.1	55	4.5	200	9.1	0	62.6	4.5	26.2
Feb-00	12	56.8	31.5	200	12	0	74.7	31.5	29.9
Mar-00	24.7	48.8	57.1	200	24.7	0	39.2	57.1	45.3
Apr-00	32.8	60.8	44.6	200	32.8	0	19.6	44.6	46.8
May-00	62.5	117.4	58.9	200	62.5	0	9.8	58.9	57.2
Jun-00	81.7	179	98.2	200	81.7	0	0	98.2	83.7
Jul-00	92.1	54.4	-40.4	159.6	92.1	0	0	0	40.1
Aug-00	82	99.4	12.4	172	82	0	0	0	23.7
Sep-00	52.4	108.4	50.6	200	52.4	0	0	22.6	26.1
Oct-00	33.5	24.8	-9.9	190.1	33.5	0	0	0	11.6
Nov-00	17	127.6	98.5	200	17	0	6.3	88.6	55.3
Dec-00	8.2	154.6	11.7	200	8.2	0	140.3	11.7	31.2
Jan-01	10.1	57.4	30.4	200	10.1	0	156.5	30.4	31.3
Feb-01	10.8	144.4	69.2	200	10.8	0	218.7	69.2	52
Mar-01	17.3	77.2	89.9	200	17.3	0	186.7	89.9	71.9
Apr-01	35.5	31.6	87.8	200	35.5	0	93.4	87.8	80.4
May-01	66.9	100.4	75.2	200	66.9	0	46.7	75.2	82
Jun-01	89.1	82.4	12.5	200	89.1	0	23.3	12.5	48.9
Jul-01	95.6	29.2	-56.2	143.8	95.6	0	11.7	0	23.8
Aug-01	97.5	87.4	-8.7	137.6	95.1	2.4	5.8	0	15.6
Sep-01	53.3	86.2	34.4	172	53.3	0	0	0	9.9
Oct-01	32.7	142.8	103	200	32.7	0	0	75	47.4
Nov-01	21.7	73.2	47.8	200	21.7	0	0	47.8	47.7
Dec-01	14.6	77.6	50	200	14.6	0	9.9	50	50.1
Jan-02	13.1	49.2	23.5	200	13.1	0	21	23.5	36.7
Feb-02	12.8	75.6	38.2	200	12.8	0	43.8	38.2	38.6
Mar-02	19	86.8	58.4	200	19	0	50.4	58.4	50.4
Apr-02	34.9	91.8	77.5	200	34.9	0	25.2	77.5	67.1

THORNTHWAITE DATA

				Soil			Snow		
Date	PET	P	P-PET	Moisture	AET	PET-AET	Storage	Surplus	ROtotal
=====	=====	=====	=====	=====	=====	=====	=====	=====	=====
May-02	52.5	139.6	92.7	200	52.5	0	12.6	92.7	84.6
Jun-02	88	77.6	-8	192	88	0	6.3	0	42.7
Jul-02	114.4	68.2	-43.3	150.4	112.7	1.7	0	0	22.8
Aug-02	90	104.2	9	159.4	90	0	0	0	14.9
Sep-02	65.9	53.6	-14.9	147.5	62.8	3	0	0	7.5
Oct-02	29	65.2	32.9	180.4	29	0	0	0	5.7
Nov-02	16.3	88	60.7	200	16.3	0	7.2	41.1	25.6
Dec-02	11.4	59.2	24.8	200	11.4	0	28.8	24.8	24.7
Jan-03	7.4	128.2	-7.4	192.6	7.4	0	157	0	11.7
Feb-03	8.2	111.6	-8.2	184.7	7.9	0.3	268.6	0	5.8
Mar-03	17.3	76.6	102.8	200	17.3	0	223.1	87.5	48.7
Apr-03	29.7	51.2	130.5	200	29.7	0	111.5	130.5	91.1
May-03	57.3	73	67.8	200	57.3	0	55.8	67.8	81.9
Jun-03	85.3	45.4	-14.3	185.7	85.3	0	27.9	0	41.4
Jul-03	99.8	61	-27.9	159.7	97.8	2	13.9	0	22.6
Aug-03	93.4	68.8	-21.1	142.9	89.2	4.2	7	0	13.2
Sep-03	56.8	65.2	12.2	155.1	56.8	0	0	0	8.1
Oct-03	29.8	111	75.7	200	29.8	0	0	30.8	23.4
Nov-03	18.5	131	106	200	18.5	0	0	106	68.5
Dec-03	12.1	97.4	51.4	200	12.1	0	31.2	51.4	59.4
Jan-04	6.7	149.6	-6.7	193.3	6.7	0	180.8	0	28.3
Feb-04	10.5	56.6	34.1	200	10.5	0	192	27.4	28.6
Mar-04	20.4	94.2	125.4	200	20.4	0	136.9	125.4	80.1
Apr-04	33.6	43	75.7	200	33.6	0	68.5	75.7	78.3
May-04	57.6	148.6	117.8	200	57.6	0	34.2	117.8	104.4
Jun-04	78.7	44	-19.8	180.2	78.7	0	17.1	0	50.7
Jul-04	95.6	124.8	31.5	200	95.6	0	8.6	11.7	36.3
Aug-04	77.5	48	-23.4	176.6	77.5	0	0	0	17.5
Sep-04	60	37.4	-24.5	155	57.1	2.9	0	0	9.4
Oct-04	32.7	61.6	25.9	180.9	32.7	0	0	0	6.8
Nov-04	18.1	81.8	59.6	200	18.1	0	0	40.5	26.2
Dec-04	10	115.6	38.2	200	10	0	65.6	38.2	32
Jan-05	8.2	59.2	-4.7	195.3	8.2	0	121.2	0	15.2
Feb-05	10.4	61.8	26	200	10.4	0	145.8	21.3	19
Mar-05	16	39.4	37.8	200	16	0	130.5	37.8	28.9
Apr-05	35.3	121	144.9	200	35.3	0	65.3	144.9	92.5
May-05	54.2	26.8	3.9	200	54.2	0	32.6	3.9	46.5
Jun-05	104	142.4	47.5	200	104	0	16.3	47.5	53.5
Jul-05	111.6	50.4	-55.6	144.4	111.6	0	8.2	0	25.7
Aug-05	94	65.2	-23.9	127.2	87.3	6.6	0	0	14.8
Sep-05	64.6	78.6	10	137.2	64.6	0	0	0	9.7
Oct-05	35.4	44	6.4	143.6	35.4	0	0	0	5.1
Nov-05	18.9	118.2	93.4	200	18.9	0	0	37	25.8
Dec-05	10.6	114.6	46.5	200	10.6	0	55.2	46.5	35.5

THORNTHWAITE DATA

				Soil			Snow		
Date	PET	P	P-PET	Moisture	AET	PET-AET	Storage	Surplus	ROtotal
=====	=====	=====	=====	=====	=====	=====	=====	=====	=====
Jan-06	12.8	78.2	54.3	200	12.8	0	64.1	54.3	46
Feb-06	10.1	166.6	47.3	200	10.1	0	171.4	47.3	47.4
Mar-06	18.8	61	80	200	18.8	0	131.6	80	64.7
Apr-06	36.9	85	109.6	200	36.9	0	65.8	109.6	90.5
May-06	64.4	52.2	18	200	64.4	0	32.9	18	54.7
Jun-06	90.8	85.8	7.2	200	90.8	0	16.4	7.2	33.9
Jul-06	113.7	143.8	31.1	200	113.7	0	8.2	31.1	37.6
Aug-06	87.8	22.2	-58.5	141.5	87.8	0	0	0	16.3
Sep-06	52.7	100.2	42.5	184	52.7	0	0	0	12.6
Oct-06	30.3	132.4	95.5	200	30.3	0	0	79.5	50.2
Nov-06	19.9	97.8	73	200	19.9	0	0	73	63.2
Dec-06	14.5	88.8	59	200	14.5	0	11.8	59	62.1
	535	999	425	2346	531	4	551	427	465

DETAILED WATER BALANCE CALCULATIONS

79 Collier Street, City of Barrie

1 Climate Information

Precipitation	999 mm/a
Actual Evapotranspiration	531 mm/a
Water Surplus	468 mm/a

2 Infiltration Rates

Table 2 Approach - Infiltration factors

Topography: Flat to rolling Land	0.25
Soil Type: predominantly open sandy loam	0.4
Cover: Open Land	0.1
Total	0.75
Infiltration (0.75 x 468)	351 mm/a
Run-off (468-351)	117 mm/a

Table 3 Approach - Typical Recharge Rates

Coarse Sand and Gravel	>250	mm/a
Fine to medium sand	200-250	mm/a
Silty sand to sandy silt	150-200	mm/a
Silt	125-150	mm/a
Clayey Silt	100- 125	mm/a
Clay	<100	mm/a

Site development area is underlain predominantly by sandy soils

Based on the above, the recharge rate is typically 200-250 mm/a

3 Pre-Development Property Statistics

	ha	m2
Paved Area	0.126	1260
Roof Area	0	0
Landscape Area	0.04	400
Total	0.166	1660

4 Post-Development Property Statistics

	ha	m2
Paved Area	0.0558	558
Total Building Roof Area	0.1102	1102
Landscape Area	0	0
Total Land Area	0.166	1660

5. Annual Pre-Development Water Balance

Land Use		Area (m ²)	Precipitation (m ³)	Evapotranspiration (m3)	Infiltration (m ³)	Run-off (m ³)
Impervious Areas	Paved Area	1260	1259	126	0	1133
	Roof Area	0	0	0	0	0
Pervious Areas	Landscape Area	400	400	212	140	47
		1,660	1,658	338	140	1,180

Assuming no infiltration occurring in paved and roof areas, and 10% of precipitation to be evaporated from paved and roof areas.

6. Annual Post-Development Water Balance

Land Use		Area (m ²)	Precipitation (m ³)	Evapotranspiration (m3)	Infiltration (m ³)	Run-off (m ³)
Impervious Areas	Paved Area	558	557	56	0	502
	Roof Area	1102	1,101	110	0	991
Pervious Areas	Landscape Area	0	0	0	0	0
		1,660	1,658	166	0	1,493

Assuming no infiltration occurring in paved and roof areas, 10% of precipitation to be evaporated from paved and general roof areas.

7. Comparison of Pre- and Post -Development

	Precipitation (m ³)	Evapotranspiration (m3)	Infiltration (m ³)	Run-off (m ³)
Pre-Development	1,658	338	140	1,180
Post-Development	1,658	166	0	1,493
Change in Volume		-172	-140	313
Change in %			-100	27

8. Requirement for Infiltration of Roof Run-off

Volume of Pre-Development Infiltration (m ³ /annum)	140
Volume of Post-Development Infiltration (m ³ /annum)	0
Deficit from Pre to Post Development Infiltration (m ³ /annum)	140
Percentage of Roof Runoff required to match the pre-development infiltration (%)	14