

GRADIENTWIND

ENGINEERS & SCIENTISTS

PEDESTRIAN LEVEL WIND STUDY

642 Dunlop Street West
Barrie, Ontario

Report: 22-041-PLW



April 21, 2022

PREPARED FOR
2507517 Ontario Inc.
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EXECUTIVE SUMMARY

This report describes a pedestrian level wind (PLW) study to satisfy Site Plan Control application requirements for the proposed mixed-use residential development located at 642 Dunlop Street West in Barrie, Ontario (hereinafter referred to as the “subject site” or “propose development”). Our mandate within this study is to investigate pedestrian wind comfort and safety within and surrounding the subject site, and to identify areas where wind conditions may interfere with certain pedestrian activities so that mitigation measures may be considered, where required.

The study involves simulation of wind speeds for selected wind directions in a three-dimensional (3D) computer model using the computational fluid dynamics (CFD) technique, combined with meteorological data integration, to assess pedestrian wind comfort and safety within and surrounding the subject site. A complete summary of the predicted wind conditions is provided in Section 5 and illustrated in Figures 3A-8B, and is summarized as follows:

- 1) All grade-level areas within and surrounding the subject site are predicted to receive conditions that are considered acceptable for the intended pedestrian uses throughout the year. Specifically, wind conditions over the surrounding sidewalks, surface parking lots, and building access points, are considered acceptable.
- 2) Calm and acceptable wind conditions are predicted over the east common amenity terrace serving the proposed development at Level 5.
- 3) Regarding the west common amenity terrace at Level 5, conditions are predicted to be mostly suitable for sitting with standing conditions central and to the north of the terrace during the typical use period. Within the areas that are predicted to be suitable for standing, conditions are also predicted to be suitable for sitting for at least 76% of the time during the same period. Depending on the programming of the space, the noted conditions may be considered acceptable. If necessary, sitting conditions may be extended over the full terrace by introducing a perimeter wind screen, typically glazed, and rising 1.8 m above the local walking surface.



- 4) The foregoing statements and conclusions apply to common weather systems, during which no dangerous wind conditions, as defined in Section 4.4, are expected anywhere over the subject site. During extreme weather events, (e.g., thunderstorms, tornadoes, and downbursts), pedestrian safety is the main concern. However, these events are generally short-lived and infrequent and there is often sufficient warning for pedestrians to take appropriate cover.

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1. INTRODUCTION

Gradient Wind Engineering Inc. (Gradient Wind) was retained by 2507517 Ontario Inc. to undertake a pedestrian level wind (PLW) study to satisfy Site Plan Control application requirements for the proposed mixed-use residential development located at 642 Dunlop Street West in Barrie, Ontario (hereinafter referred to as the “subject site” or “propose development”). Our mandate within this study is to investigate pedestrian wind comfort and safety within and surrounding the subject site, and to identify areas where wind conditions may interfere with certain pedestrian activities so that mitigation measures may be considered, where required.

Our work is based on industry standard computer simulations using the computational fluid dynamics (CFD) technique and data analysis procedures, industry standard wind comfort and safety guidelines, architectural drawings prepared by n Architecture Inc., in February 2022, surrounding street layouts and existing and approved future building massing information obtained from the City of Barrie, recent satellite imagery, and experience with numerous similar developments.

2. TERMS OF REFERENCE

The subject site is located at 642 Dunlop Street West; situated at the northeast intersection of Dunlop Street West and Miller Drive. Throughout this report, the Dunlop Street West elevation is referred to as project south.

The proposed development comprises a five-storey mixed-use building plus mechanical penthouse level, with an “L”-shaped planform with its long axis-oriented along Dunlop Street West. The ground floor comprises a bicycle storage area at the southeast corner, a residential main entrance to the south, retail spaces to the south and west, loading space at the northwest corner, a central elevator core and loading space, and shared building support spaces throughout the remainder of the level. Indoor parking spaces are situated to the north and can be accessed by an entrance to the east and exit at the northwest corner of the proposed development. Levels 2 to 4 are reserved for residential use. Level 5 includes a central gym, party room, and mechanical penthouse. This level is also served by a common amenity terrace situated to the east which includes an open amenity space at the northeast corner and an open play area at the southeast corner and an open roof deck to the west.

Regarding wind exposures, the near-field surroundings of the development (defined as an area falling within 200 metres (m) of the site) are characterized by dense forestry to the north, an equipment rental agency to the northeast, dense forestry to the east, Simcoe Hose & Hydraulic to the southeast, and a gas station and FedEx Onsite to the west. The far-field surroundings (defined as the area beyond the near field and within a 2-kilometre (km) radius) comprise low-rise residential buildings to the north, low-rise commercial buildings to the east, low-rise residential buildings to the southeast and south, and isolated low-rise commercial buildings to the south and west. Green spaces are situated in all compass directions with the largest spaces from the southeast clockwise northwest.

Site plans for the proposed and existing massing scenarios are illustrated in Figures 1A and 1B, while Figures 2A-2H illustrate the computational models used to conduct the study. The existing massing scenario includes the existing massing and any changes which have been approved by the City of Barrie.

3. OBJECTIVES

The principal objectives of this study are to: (i) determine comparative pedestrian level wind comfort and safety conditions at key outdoor areas; (ii) identify areas where future wind conditions may interfere with the intended uses of outdoor spaces; and (iii) recommend suitable mitigation measures, where required.

4. METHODOLOGY

The approach followed to quantify pedestrian wind conditions over the site is based on CFD simulations of wind speeds across the subject site within a virtual environment, meteorological analysis of the Barrie wind climate, and synthesis of computational data with industry-accepted guidelines. The following sections describe the analysis procedures, including a discussion of the comfort guidelines.

4.1 Computer-Based Context Modelling

A computer based PLW wind study was performed to determine the influence of the wind environment on pedestrian comfort over the proposed development. Pedestrian comfort predictions, based on the mechanical effects of wind, were determined by combining measured wind speed data from CFD simulations with statistical weather data obtained from Lake Simcoe Regional Airport.

The general concept and approach to CFD modelling is to represent building and topographic details in the immediate vicinity of the subject site on the surrounding model, and to create suitable atmospheric wind profiles at the model boundary. The wind profiles are designed to have similar mean and turbulent wind properties consistent with actual site exposures.

An industry standard practice is to omit trees, vegetation, and other existing and planned landscape elements from the model due to the difficulty of providing accurate seasonal representation of vegetation. The omission of trees and other landscaping elements produces slightly more conservative (i.e., windier) wind speed values.

4.2 Wind Speed Measurements

The PLW analysis was performed by simulating wind flows and gathering velocity data over a CFD model of the site for 12 wind directions. The CFD simulation model was centered on the study building, complete with surrounding massing within a diameter of approximately 1.1 km.

Mean and peak wind speed data obtained over the study site for each wind direction were interpolated to 36 wind directions at 10° intervals, representing the full compass azimuth. Measured wind speeds on a continuous measurement plane 1.5 m above local grade and the common amenity terraces at Level 5 were referenced to the wind speed at gradient height to generate mean and peak velocity ratios, which were used to calculate full-scale values. The gradient height represents the theoretical depth of the boundary layer of the earth's atmosphere, above which the mean wind speed remains constant. Further details of the CFD wind flow simulation technique are presented in Appendix A.

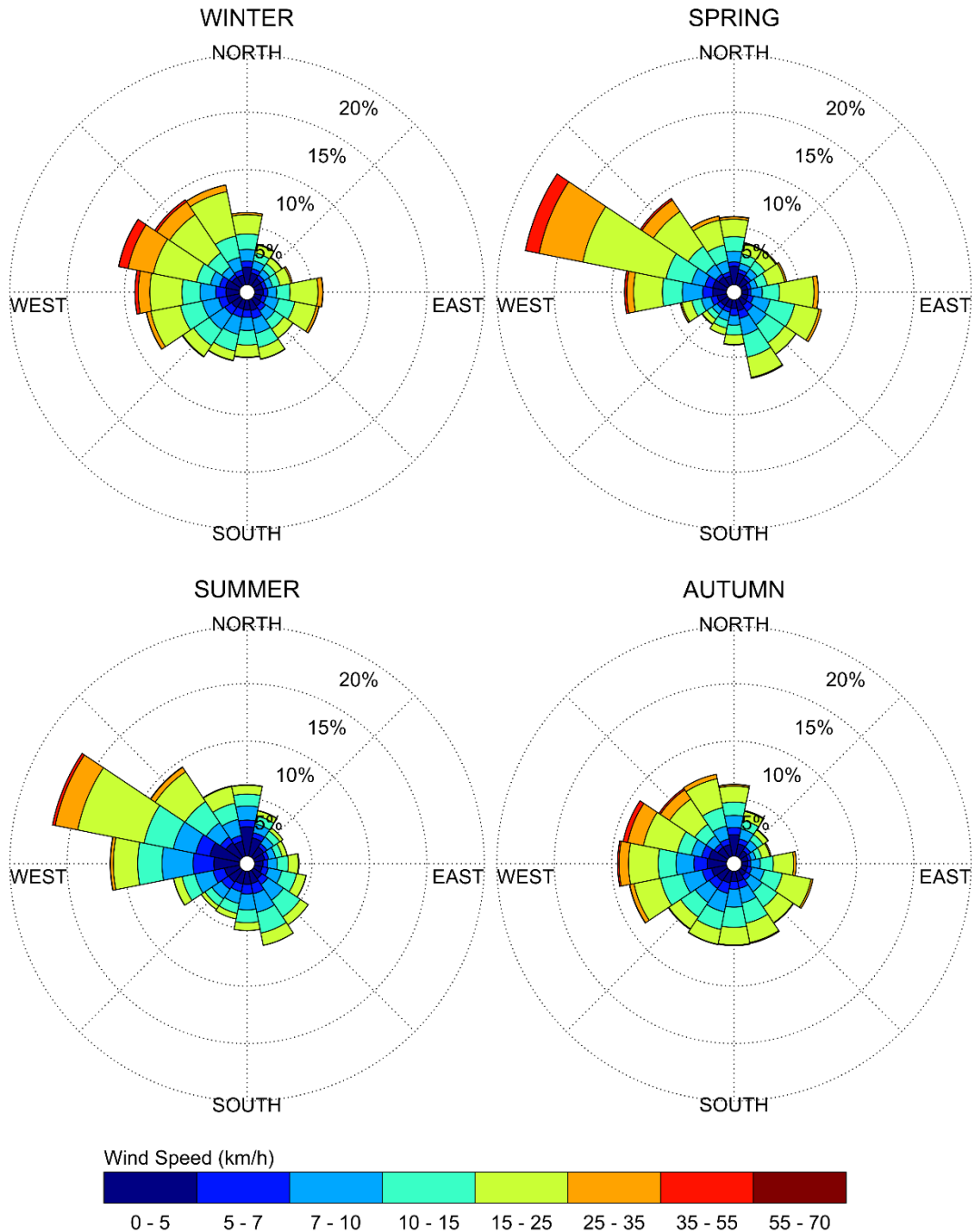
4.3 Meteorological Data Analysis

A statistical model for winds in Barrie was developed from approximately 18 years of hourly meteorological wind data recorded at Lake Simcoe Regional Airport and obtained from Environment and Climate Change Canada. Wind speed and direction data were analyzed for each month of the year to determine the statistically prominent wind directions and corresponding speeds, and to characterize similarities between monthly weather patterns. Based on this portion of analysis, the four seasons are represented by grouping data from consecutive months based on similarity of weather patterns, and not according to the traditional calendar method; spring is defined as April-May, summer as June-September, autumn as October-November, and winter as December-March.

The statistical model of the Barrie area wind climate, which indicates the directional character of local winds on a seasonal basis, is illustrated on the following page. The plots illustrate seasonal distribution of measured wind speeds and directions in km/h. Probabilities of occurrence of different wind speeds are represented as stacked polar bars in sixteen azimuth divisions. The radial direction represents the percentage of time for various wind speed ranges per wind direction during the measurement period. The preferred wind speeds and directions can be identified by the longer length of the bars. For Barrie, the most common winds concerning pedestrian comfort occur from the west clockwise to the north. The directional preference and relative magnitude of the wind speed varies somewhat from season to season, with the summer months displaying the calmest winds relative to the remaining seasonal periods.

Additionally, a second model was developed from approximately twenty years of similar data recorded at the Centre for Atmospheric Research Experiments in Egbert, which lies to the southwest of Barrie, whereas the Lake Simcoe Airport lies to the northeast of Barrie. The results of the second model exhibited generally lower wind speeds since the Lake Simcoe Airport is more exposed to prominent winds from Georgian Bay. Since the Lake Simcoe Airport data produce more conservative results, the results of the second model are not presented in this report.

SEASONAL DISTRIBUTION OF WIND LAKE SIMCOE REGIONAL AIRPORT, ORO-MEDONTE, ONTARIO



Notes:

1. Radial distances indicate percentage of time of wind events.
2. Wind speeds are mean hourly in km/h, measured at 10 m above the ground.



4.4 Pedestrian Comfort and Safety Guidelines

Pedestrian comfort and safety guidelines are based on the mechanical effects of wind without consideration of other meteorological conditions (i.e., temperature, relative humidity). The comfort guidelines assume that pedestrians are appropriately dressed for a specified outdoor activity during any given season. Five pedestrian comfort classes are based on 80% non-exceedance gust wind speed ranges, which include (1) Sitting; (2) Standing; (3) Strolling; (4) Walking; and (5) Uncomfortable. More specifically, the comfort classes and associated gust wind speed ranges are summarized as follows:

- (i) **Sitting** – Mean wind speeds no greater than 10 km/h occurring at least 80% of the time. The equivalent gust wind speed is approximately 16 km/h.
- (ii) **Standing** – Mean wind speeds no greater than 14 km/h occurring at least 80% of the time. The equivalent gust wind speed is approximately 22 km/h.
- (iii) **Strolling** – Mean wind speeds no greater than 17 km/h occurring at least 80% of the time. The equivalent gust wind speed is approximately 27 km/h.
- (iv) **Walking** – Mean wind speeds no greater than 20 km/h occurring at least 80% of the time. The equivalent gust wind speed is approximately 30 km/h.
- (v) **Uncomfortable** – Uncomfortable conditions are characterized by predicted values that fall below the 80% target for walking. Brisk walking and exercise, such as jogging, would be acceptable for moderate excesses of this comfort class.

The pedestrian safety wind speed guideline is based on the approximate threshold that would cause a vulnerable member of the population to fall. A 0.1% exceedance gust wind speed of greater than 90 km/h is classified as dangerous. The wind speeds associated with the above categories are gust wind speeds. The gust speeds, and equivalent mean speeds, are selected based on 'The Beaufort Scale', presented on the following page, which describes the effects of forces produced by varying wind speed levels on objects. Gust speeds are included because pedestrians tend to be more sensitive to wind gusts than to steady winds for lower wind speed ranges. For strong winds approaching dangerous levels, this effect is less important because the mean wind can also create problems for pedestrians.



THE BEAUFORT SCALE

Number	Description	Wind Speed (km/h) Gust	Description
2	Light Breeze	9-17	Wind felt on faces
3	Gentle Breeze	18-29	Leaves and small twigs in constant motion; wind extends light flags
4	Moderate Breeze	30-42	Wind raises dust and loose paper; small branches are moved
5	Fresh Breeze	43-57	Small trees in leaf begin to sway
6	Strong Breeze	58-74	Large branches in motion; Whistling heard in electrical wires; umbrellas used with difficulty
7	Moderate Gale	75-92	Whole trees in motion; inconvenient walking against wind
8	Gale	93-111	Breaks twigs off trees; generally impedes progress

Experience and research on people's perception of mechanical wind effects has shown that if the wind speed levels are exceeded for more than 80% of the time, the activity level would be judged to be uncomfortable by most people. For instance, if wind speeds of 16 km/h were exceeded for more than 20% of the time, most pedestrians would judge that location to be too windy for sitting or more sedentary activities. Similarly, if 32 km/h at a location were exceeded for more than 20% of the time, walking or less vigorous activities would be considered uncomfortable. As these guidelines are based on subjective reactions of a population to wind forces, their application is partly based on experience and judgment.

Once the pedestrian wind speed predictions have been established throughout the site, the assessment of pedestrian comfort involves determining the suitability of the predicted wind conditions for discrete regions within and surrounding the subject site. This step involves comparing the predicted comfort classes to the desired comfort classes, which are dictated by the location type for each region (i.e., a sidewalk, building entrance, amenity space, or other). An overview of common pedestrian location types and their typical windiest desired comfort classes are summarized on the following page. Depending on the programming of a space, the desired comfort class may differ from this table.

DESIRED PEDESTRIAN COMFORT CLASSES FOR VARIOUS LOCATION TYPES

Location Types	Desired Comfort Classes
Primary Building Entrance	Standing
Secondary Building Access Point	Walking
Public Sidewalk / Bicycle Path	Walking
Outdoor Amenity Space	Sitting (During Typical Use Period)
Café / Patio / Bench / Garden	Sitting (Typical Use Period)
Transit Stop (Without Shelter)	Standing
Transit Stop (With Shelter)	Walking
Public Park / Plaza	Sitting (Typical Use Period)
Garage / Service Entrance	Walking
Parking Lot	Walking
Vehicular Drop-Off Zone	Walking

5. RESULTS AND DISCUSSION

The following discussion of the predicted pedestrian wind conditions for the subject site is accompanied by Figures 3A-6B, illustrating wind conditions at grade level for the proposed and existing massing scenarios, and Figures 7A-7D, illustrating wind conditions over the Level 5 common amenity terraces. Conditions are presented as continuous contours of wind comfort within and surrounding the subject site and correspond to the various comfort classes noted in Section 4.4. Wind conditions suitable for sitting are represented by the colour blue, standing by green, strolling by yellow, and walking by orange; uncomfortable conditions are represented by the colour magenta.

Wind conditions within the common amenity terraces at Level 5 are also reported for the typical use period, defined as May to October, inclusive. Figure 8A illustrates wind comfort conditions consistent with the comfort classes in Section 4.4, while Figure 8B illustrates contours indicating the percentage of time conditions within the terrace are predicted to be suitable for sitting during the same period. The details of these conditions are summarized in the following pages for each area of interest.



5.1 Wind Comfort Conditions – Grade Level

Sidewalks and Building Access along Dunlop Street West: Following the introduction of the proposed development, conditions over the sidewalks along Dunlop Street West are predicted to be mostly suitable for sitting during the summer, becoming suitable for a mix of sitting and standing during the remaining three seasons. Conditions in the vicinity of building access points are predicted to be suitable for sitting throughout the year. The noted conditions are considered acceptable according to the comfort guidelines.

Wind conditions over the sidewalks along Dunlop Street West with the existing massing are predicted to be suitable for standing during the summer, autumn, and winter, becoming suitable for a mix of standing and strolling during the spring. While the noted wind conditions are considered acceptable according to the comfort guideline, the introduction of the proposed development is also predicted to increase comfort levels in some areas, in comparison to existing conditions.

Sidewalks and Building Access along Miller Drive: Following the introduction of the proposed development, conditions over the sidewalks along Miller Drive are predicted to be mostly suitable for sitting during the summer, becoming suitable for a mix of sitting and standing during the autumn and winter, and suitable for standing during the spring. Conditions in the vicinity of building access points are predicted to be suitable for sitting throughout the year. The noted conditions are considered acceptable according to the comfort guidelines.

Wind conditions over the sidewalks along Miller Drive with the existing massing are predicted to be suitable for a mix of sitting and standing during the summer, becoming suitable for standing during the autumn and winter, and suitable for a mix of standing and strolling during the spring. While the noted wind conditions are considered acceptable according to the comfort guideline, the introduction of the proposed development is also predicted to increase comfort levels in some areas, in comparison to existing conditions.



Building Access and Surface Parking North of Subject Site: Following the introduction of the proposed development, wind conditions over the surface parking area north of the subject site are predicted to be mostly suitable for sitting during the summer, becoming suitable for a mix of sitting and standing during the remaining three seasons. Conditions in the vicinity of building access points are predicted to be suitable for sitting throughout the year. The noted conditions are considered acceptable according to the comfort guidelines.

Building Access and Surface Parking East of Subject Site: Following the introduction of the proposed development, wind conditions over the surface parking area east of the subject site are predicted to be suitable for a mix of sitting and standing during the summer, autumn, and winter, becoming suitable for a mix of sitting, standing, and strolling during the spring. Conditions in the vicinity of building access points are predicted to be suitable for sitting throughout the year. The noted conditions are considered acceptable according to the comfort guidelines.

5.2 Wind Comfort Conditions – Common Amenity Terraces

Level 5, East Amenity Terrace: Conditions over the east amenity terrace at Level 5, which includes an open amenity space at the northeast corner and an open play area at the southeast corner of the terrace, are predicted to be suitable for sitting during the typical use period. The noted conditions are considered acceptable according to the comfort guidelines.

Level 5, West Amenity Terrace: Conditions over the west amenity terrace (open roof deck) at Level 5 are predicted to be mostly suitable for sitting with standing conditions central and to the north of the terrace during the typical use period, as illustrated in Figure 8A. Within the areas that are predicted to be suitable for standing, conditions are also predicted to be suitable for sitting for at least 76% of the time during the same period, as illustrated in Figure 8B, where the target is 80%.

Depending on the programming of the space, the noted conditions may be considered acceptable. If necessary, sitting conditions may be extended over the full terrace by introducing a perimeter wind screen, typically glazed, and rising 1.8 m above the local walking surface.



5.3 Wind Safety

Within the context of typical weather patterns, which exclude anomalous localized storm events such as tornadoes and downbursts, no pedestrian areas within or surrounding the subject site were found to experience conditions that could be considered dangerous, as defined in Section 4.4.

5.4 Applicability of Results

Pedestrian wind comfort and safety have been quantified for the specific configuration of existing and foreseeable construction around the subject site. Future changes (i.e., construction or demolition) of these surroundings may cause changes to the wind effects in two ways, namely: (i) changes beyond the immediate vicinity of the subject site would alter the wind profile approaching the subject site; and (ii) development in proximity to the subject site would cause changes to local flow patterns.

Regarding primary and secondary building access points, wind conditions predicted in this study are only applicable to pedestrian comfort and safety. As such, the results should not be construed to indicate wind loading on doors and associated hardware.

6. SUMMARY AND RECOMMENDATIONS

A complete summary of the predicted wind conditions is provided in Section 5 of this report and illustrated in Figures 3A-8B. Based on computer simulations using the CFD technique, meteorological data analysis of the Barrie wind climate, industry standard wind comfort and safety guidelines, and experience with numerous similar developments, the study concludes the following:

- 1) All grade-level areas within and surrounding the subject site are predicted to receive conditions that are considered acceptable for the intended pedestrian uses throughout the year. Specifically, wind conditions over the surrounding sidewalks, surface parking lots, and building access points, are considered acceptable.
- 2) Calm and acceptable wind conditions are predicted over the east common amenity terrace serving the proposed development at Level 5.



- 3) Regarding the west common amenity terrace at Level 5, conditions are predicted to be mostly suitable for sitting with standing conditions central and to the north of the terrace during the typical use period. Within the areas that are predicted to be suitable for standing, conditions are also predicted to be suitable for sitting for at least 76% of the time during the same period. Depending on the programming of the space, the noted conditions may be considered acceptable. If necessary, sitting conditions may be extended over the full terrace by introducing a perimeter wind screen, typically glazed, and rising 1.8 m above the local walking surface.
- 4) The foregoing statements and conclusions apply to common weather systems, during which no dangerous wind conditions, as defined in Section 4.4, are expected anywhere over the subject site. During extreme weather events, (e.g., thunderstorms, tornadoes, and downbursts), pedestrian safety is the main concern. However, these events are generally short-lived and infrequent and there is often sufficient warning for pedestrians to take appropriate cover.

Sincerely,

Gradient Wind Engineering Inc.

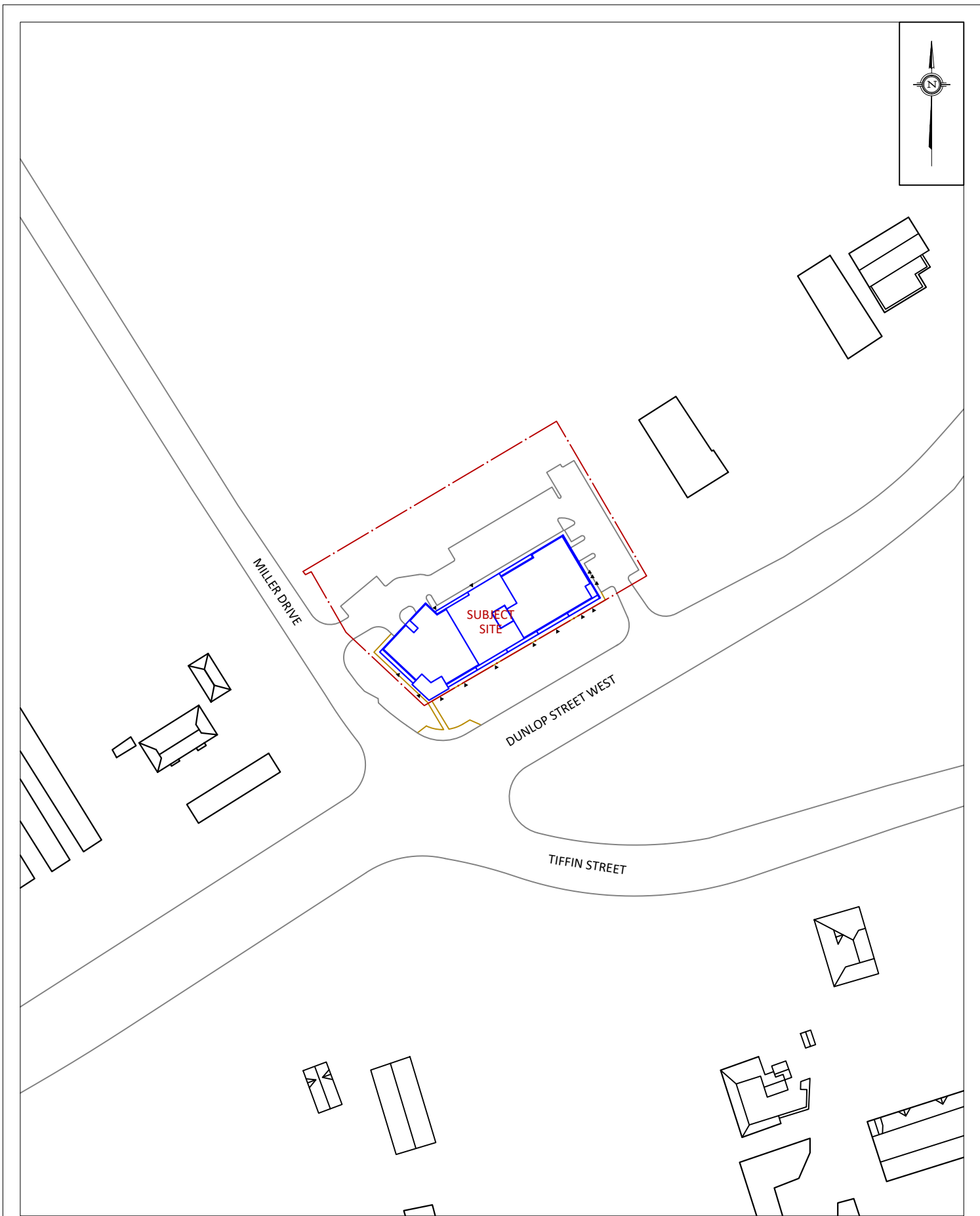
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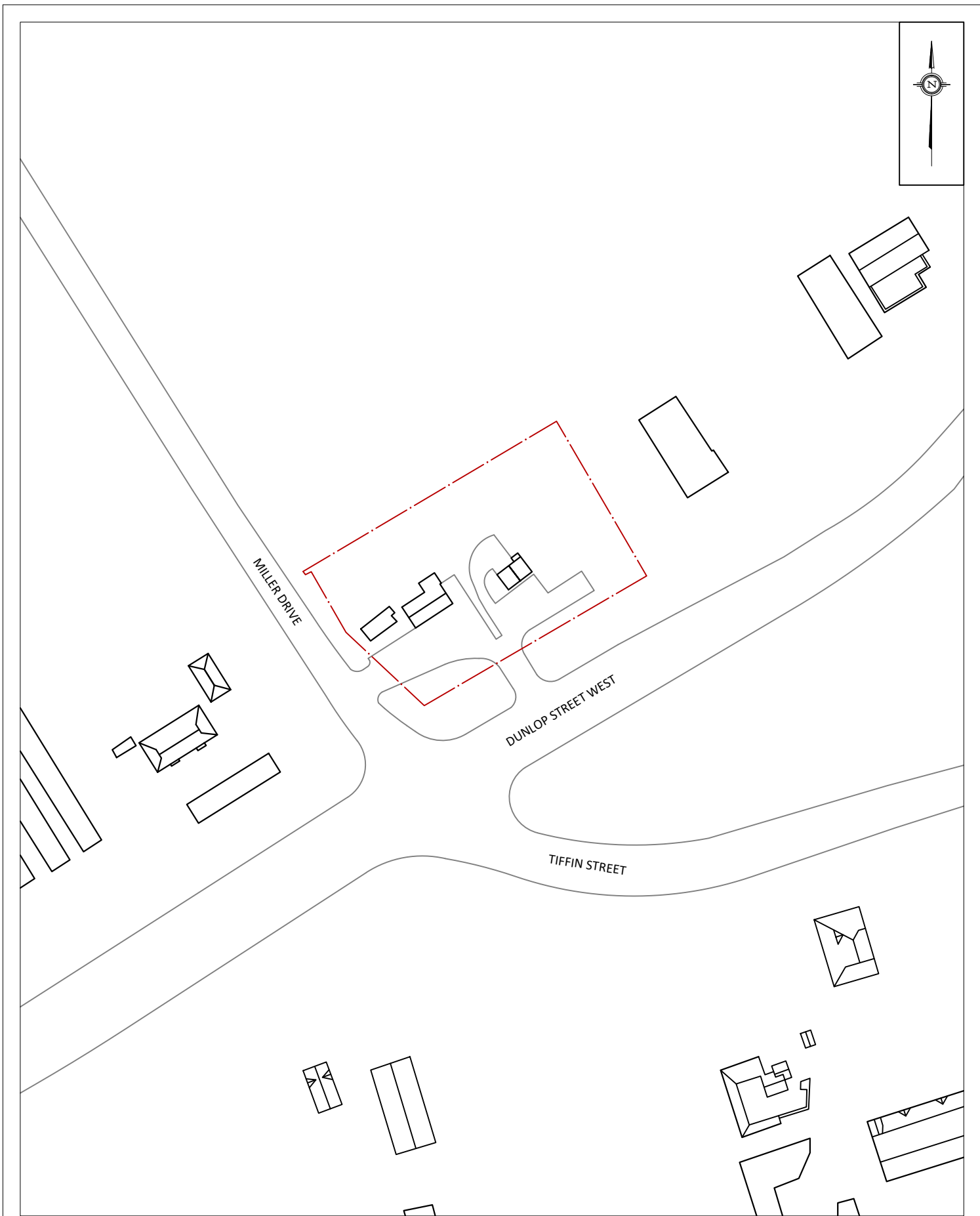


Justin Ferraro, P.Eng.
Principal





GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT 642 DUNLOP STREET WEST, BARRIE PEDESTRIAN LEVEL WIND STUDY		DESCRIPTION FIGURE 1A: PROPOSED SITE PLAN AND SURROUNDING CONTEXT
	SCALE 1:2000	DRAWING NO. 22-041-PLW-1A	
	DATE MARCH 8, 2022	DRAWN BY S.K.	



GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT 642 DUNLOP STREET WEST, BARRIE PEDESTRIAN LEVEL WIND STUDY		DESCRIPTION FIGURE 1B: EXISTING SITE PLAN AND SURROUNDING CONTEXT
	SCALE 1:2000	DRAWING NO. 22-041-PLW-1B	
	DATE MARCH 8, 2022	DRAWN BY S.K.	

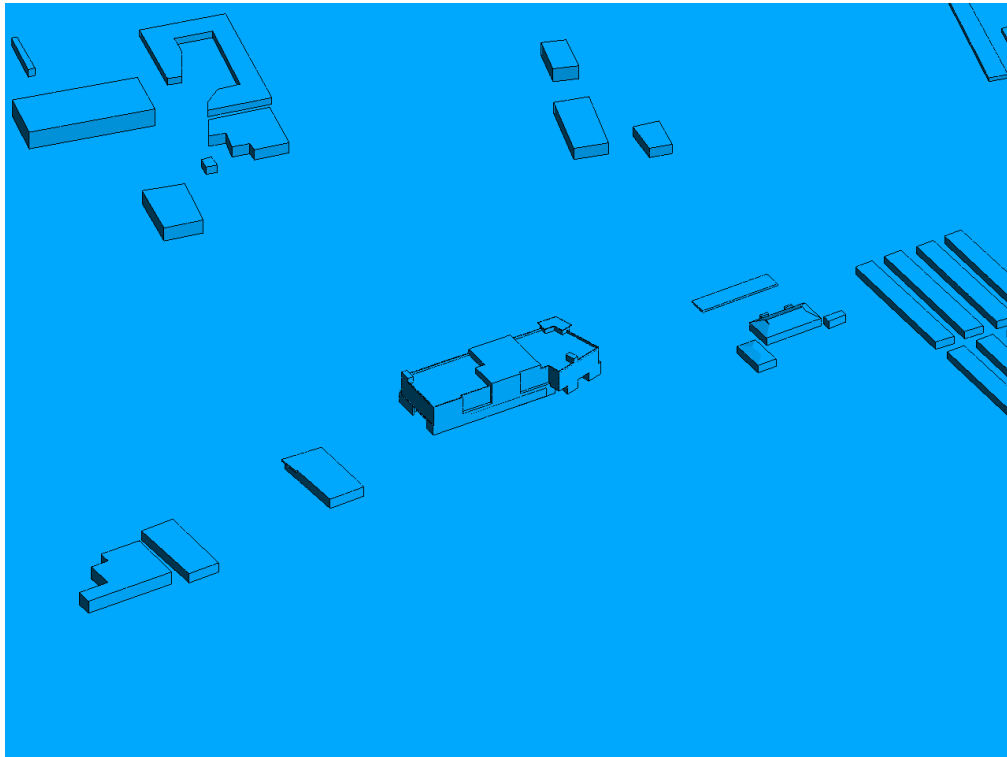


FIGURE 2A: COMPUTATIONAL MODEL, PROPOSED MASSING, NORTH PERSPECTIVE

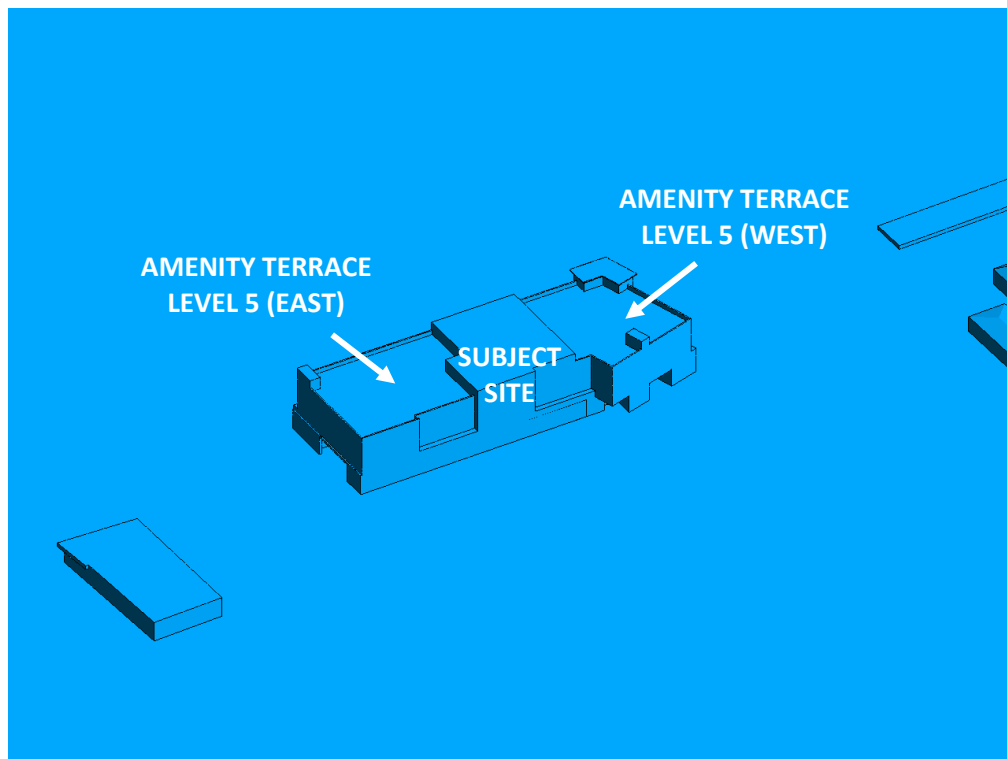


FIGURE 2B: CLOSE UP OF FIGURE 2A



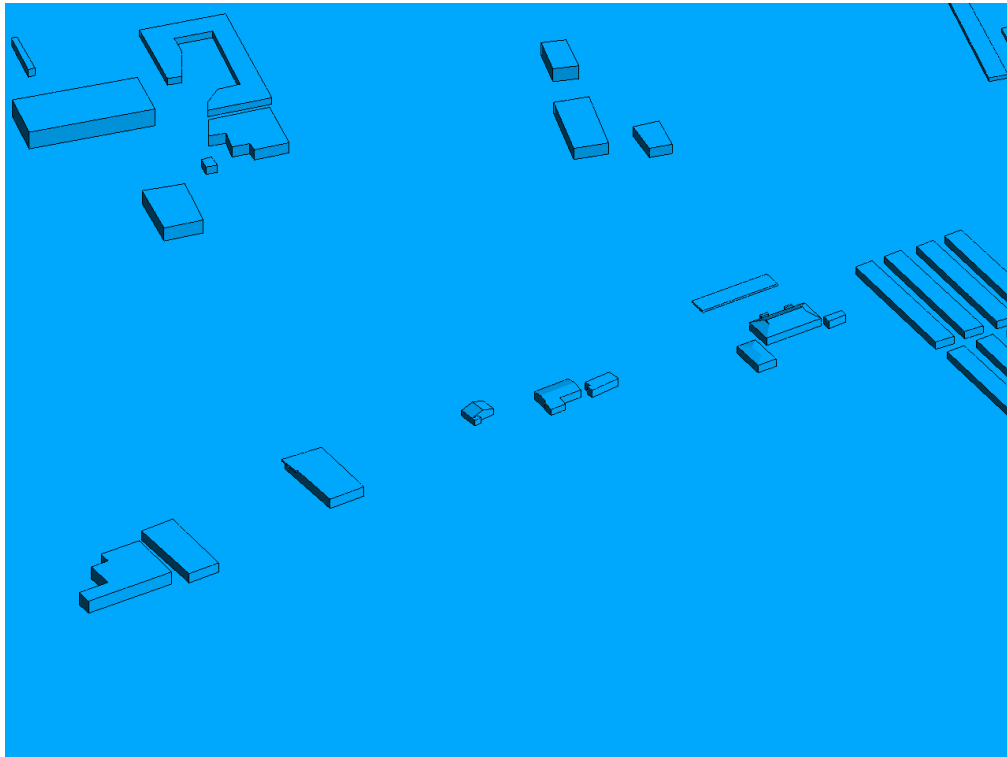


FIGURE 2C: COMPUTATIONAL MODEL, EXISTING MASSING, NORTH PERSPECTIVE

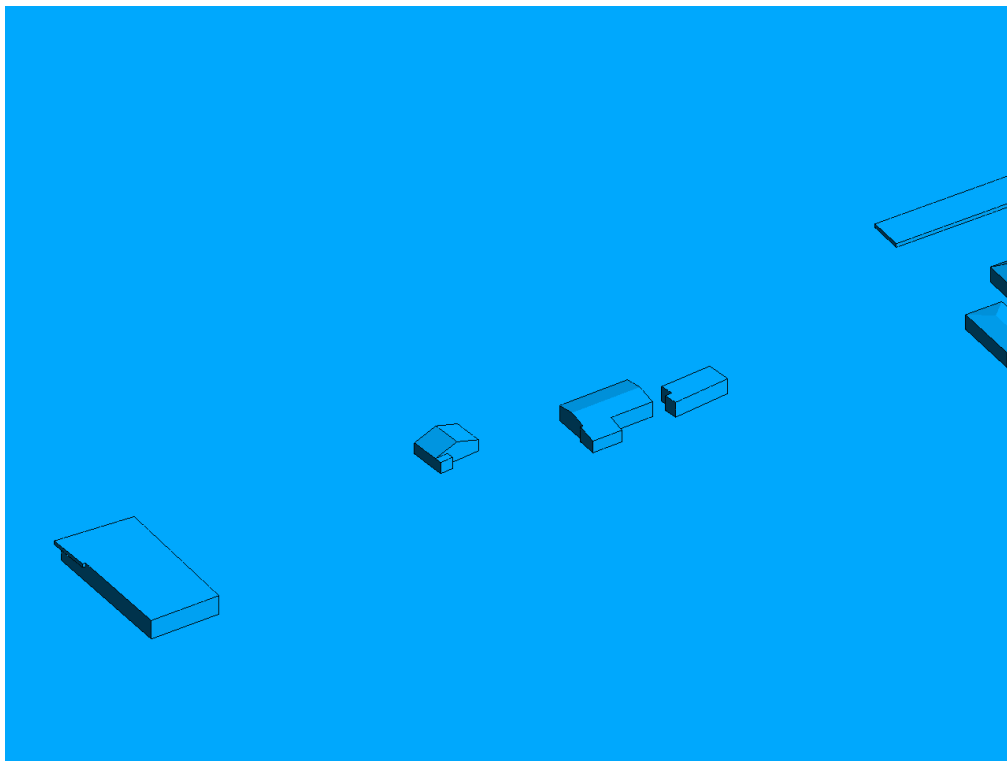


FIGURE 2D: CLOSE UP OF FIGURE 2C



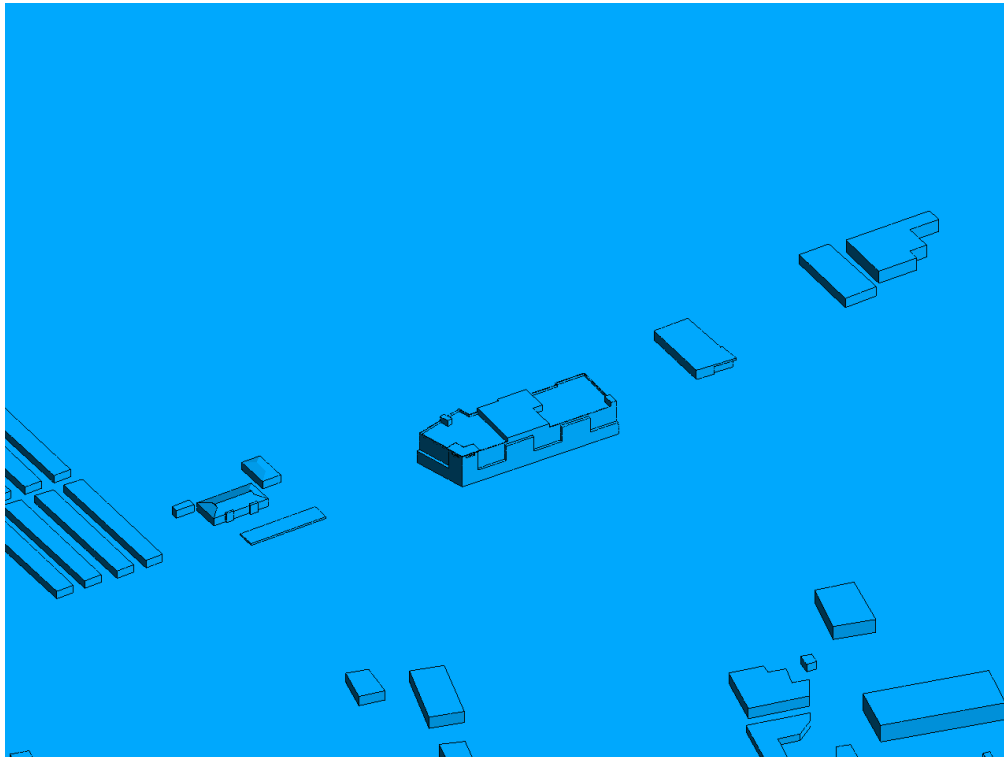


FIGURE 2E: COMPUTATIONAL MODEL, PROPOSED MASSING, SOUTH PERSPECTIVE

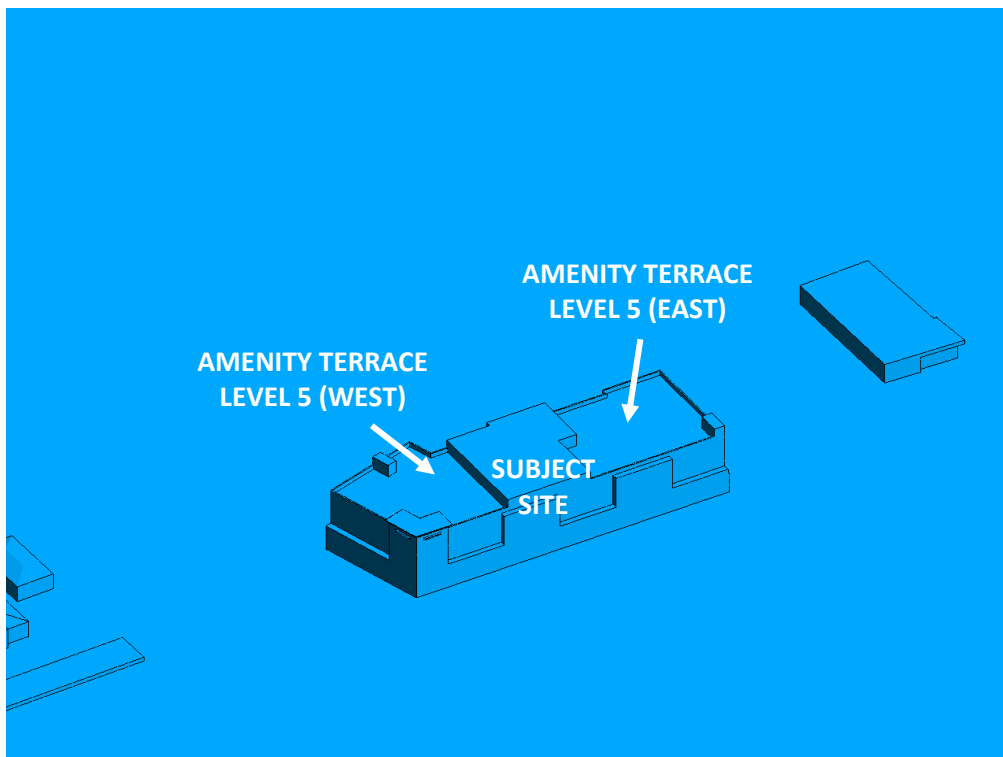


FIGURE 2F: CLOSE UP OF FIGURE 2E



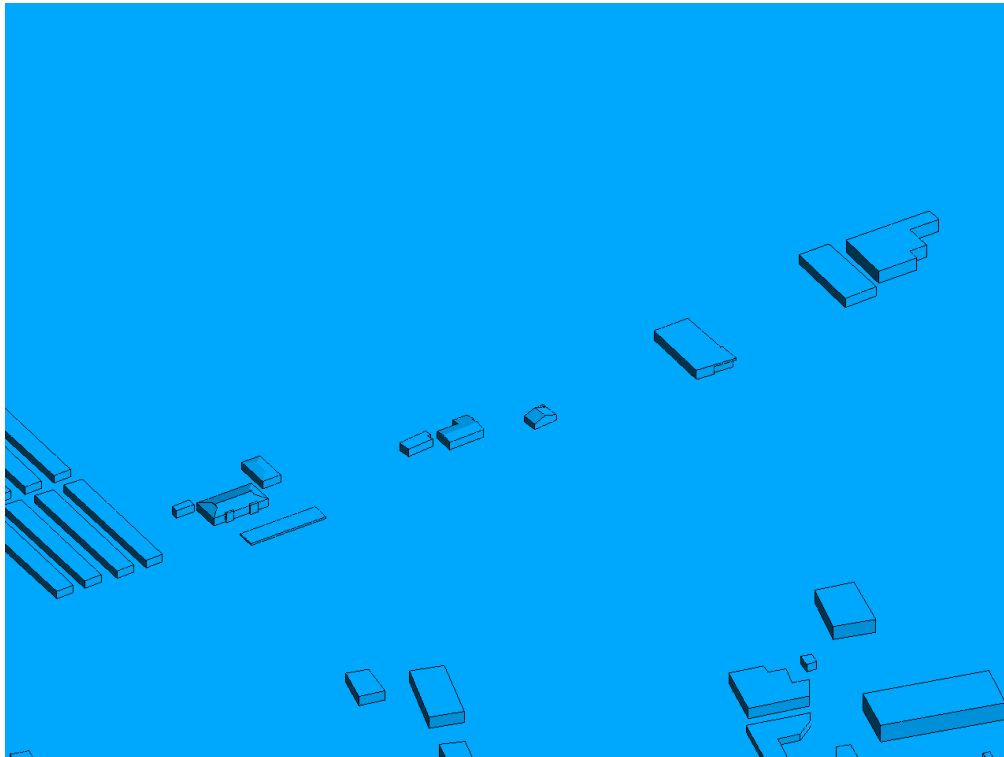


FIGURE 2G: COMPUTATIONAL MODEL, EXISTING MASSING, SOUTH PERSPECTIVE

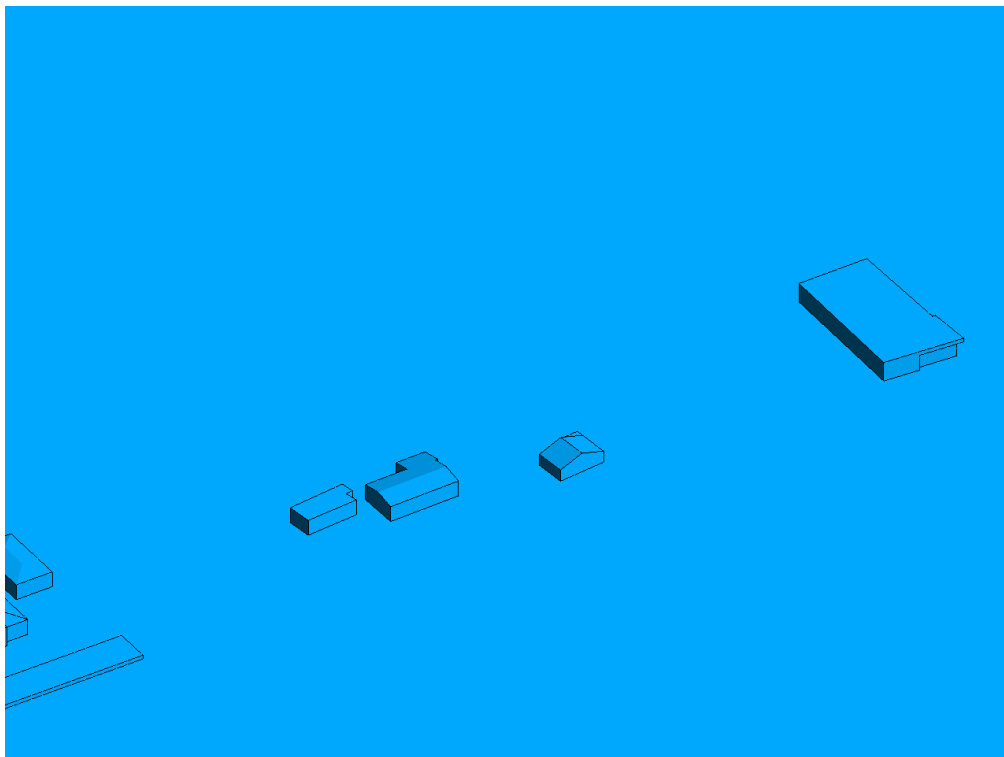


FIGURE 2H: CLOSE UP OF FIGURE 2G



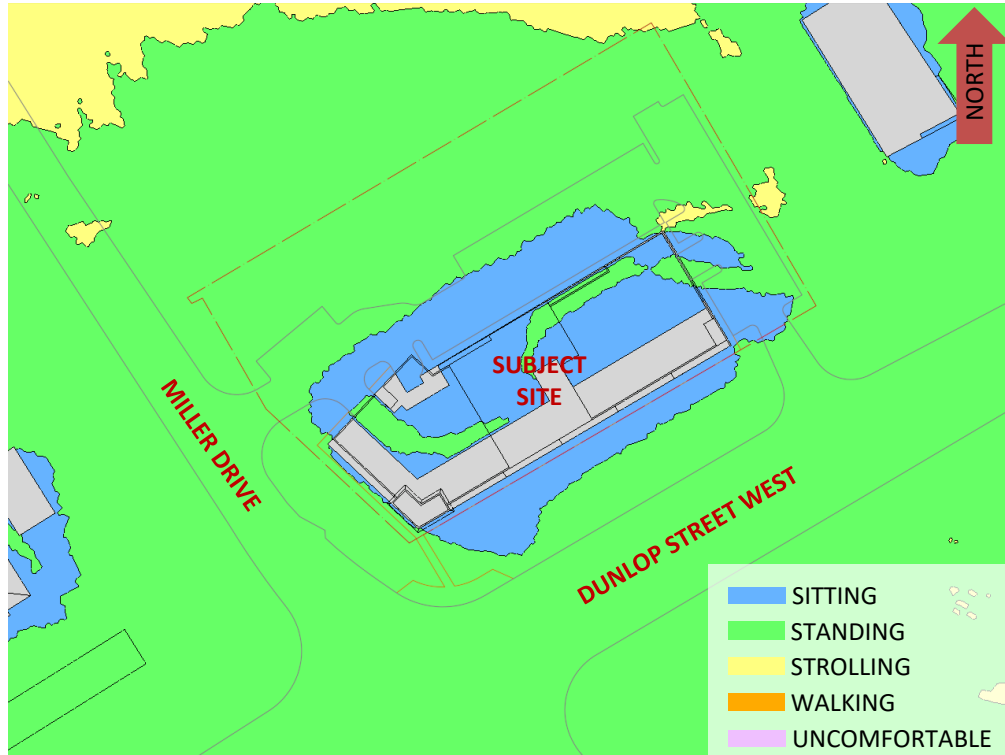


FIGURE 3A: SPRING – WIND COMFORT, GRADE LEVEL – PROPOSED MASSING

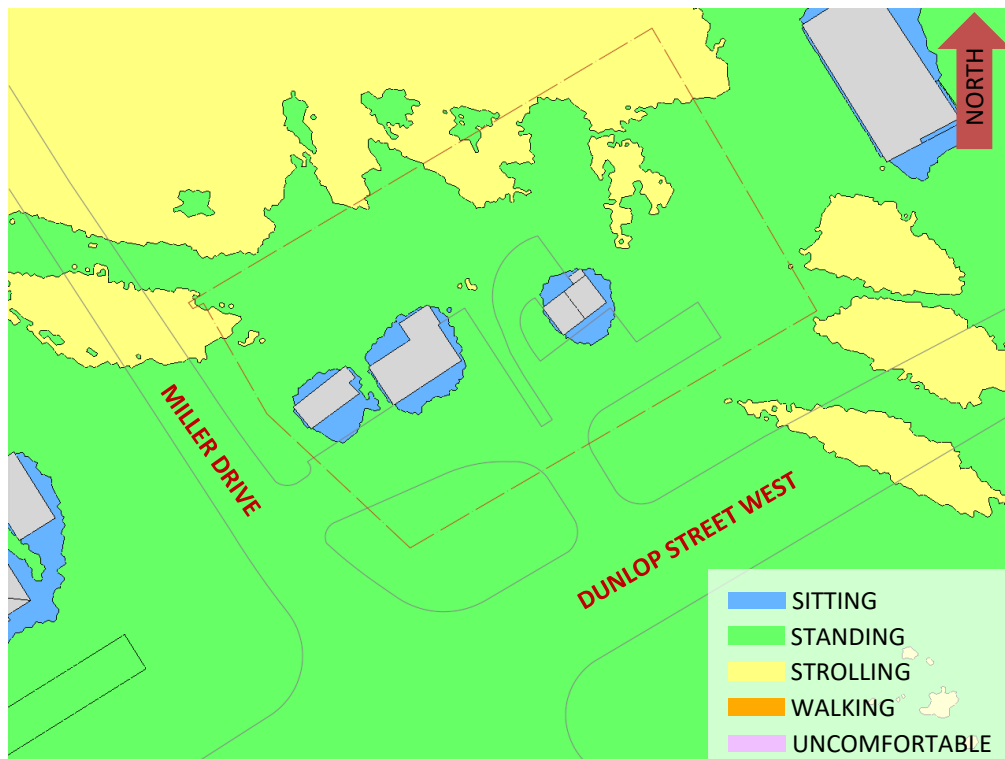


FIGURE 3B: SPRING – WIND COMFORT, GRADE LEVEL– EXISTING MASSING



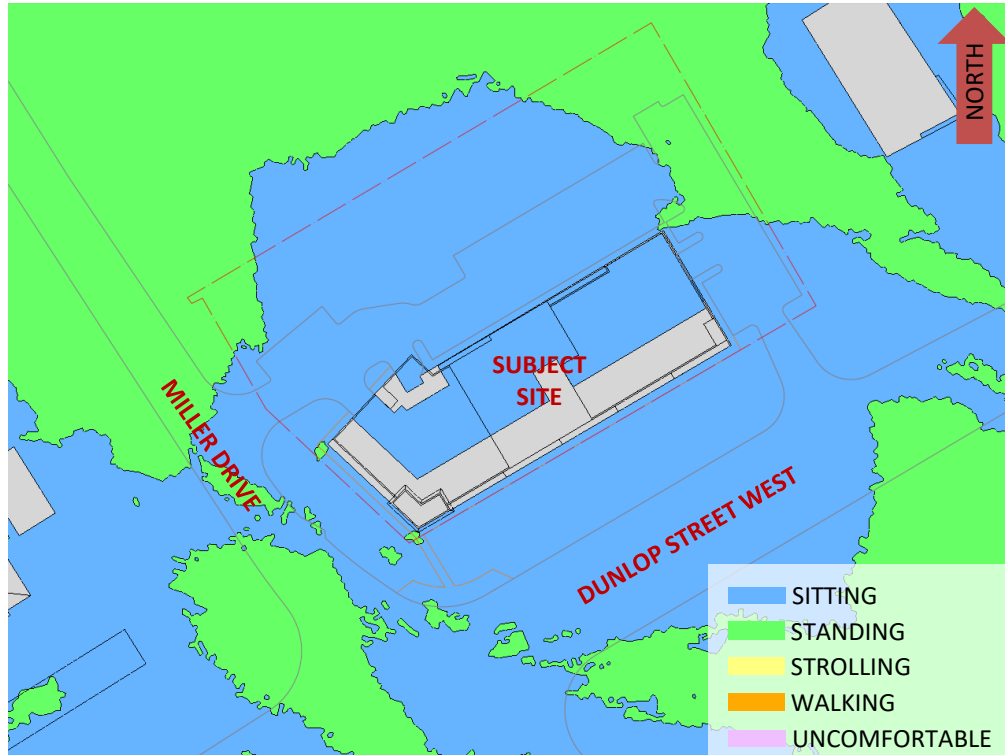


FIGURE 4A: SUMMER – WIND COMFORT, GRADE LEVEL – PROPOSED MASSING

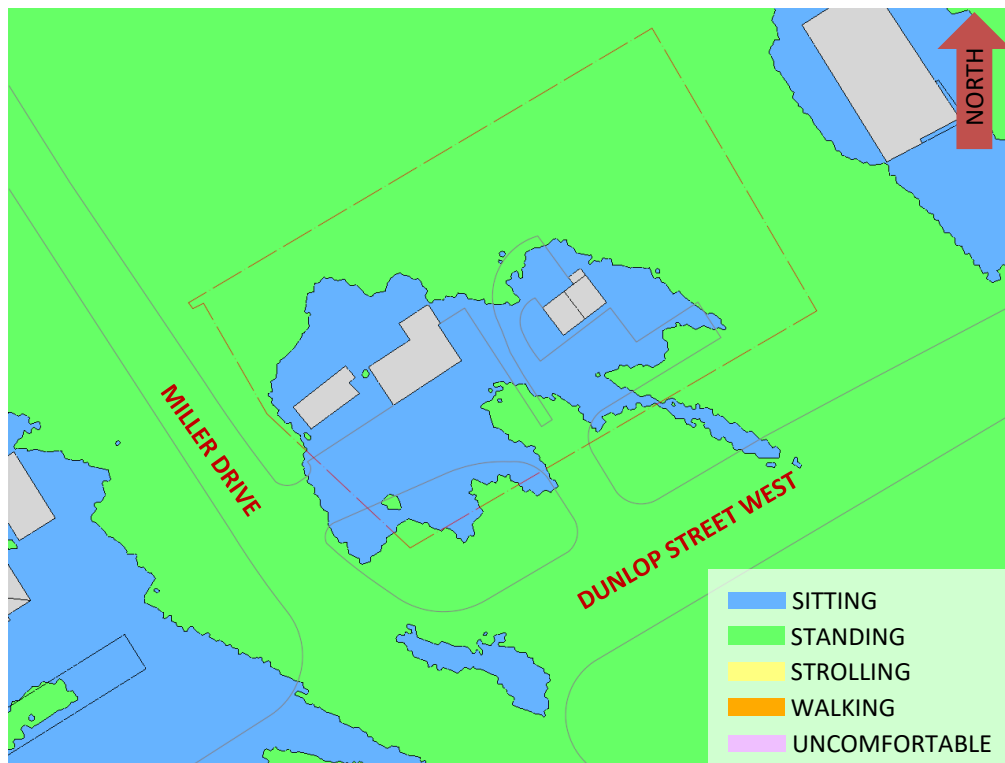


FIGURE 4B: SUMMER – WIND COMFORT, GRADE LEVEL– EXISTING MASSING



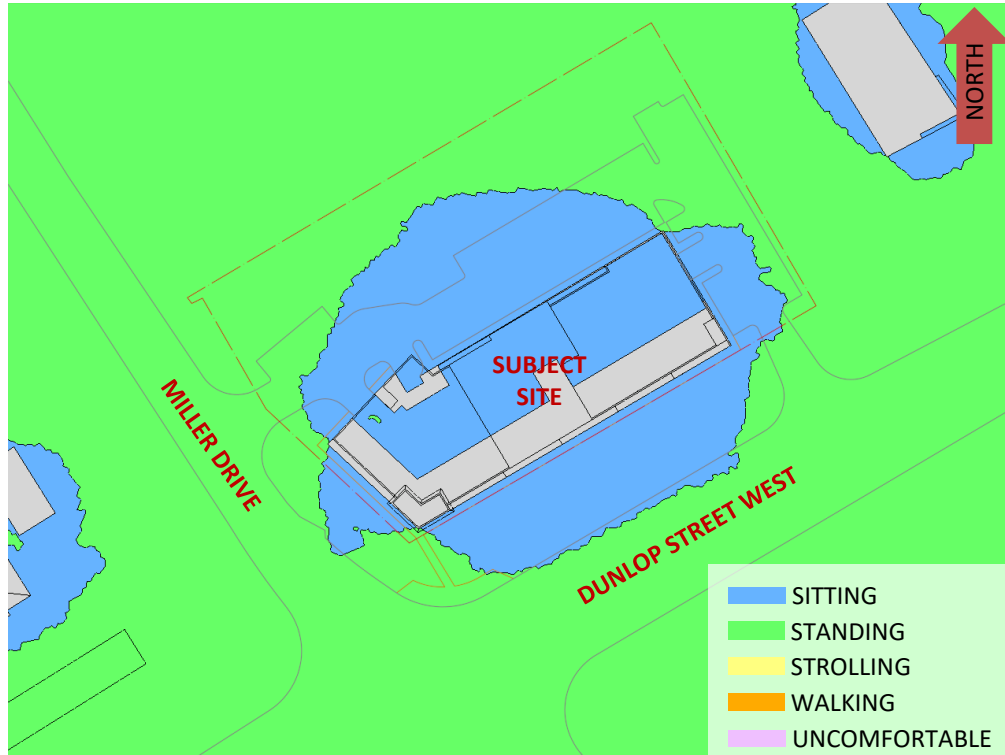


FIGURE 5A: AUTUMN – WIND COMFORT, GRADE LEVEL – PROPOSED MASSING



FIGURE 5B: AUTUMN – WIND COMFORT, GRADE LEVEL– EXISTING MASSING



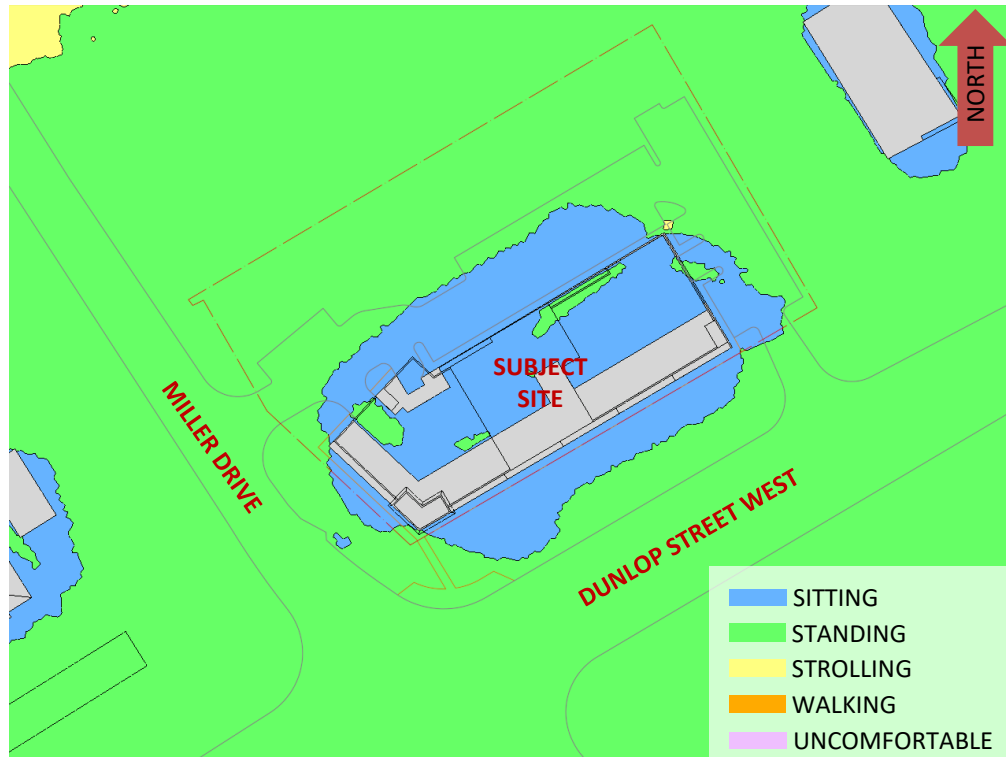


FIGURE 6A: WINTER – WIND COMFORT, GRADE LEVEL – PROPOSED MASSING

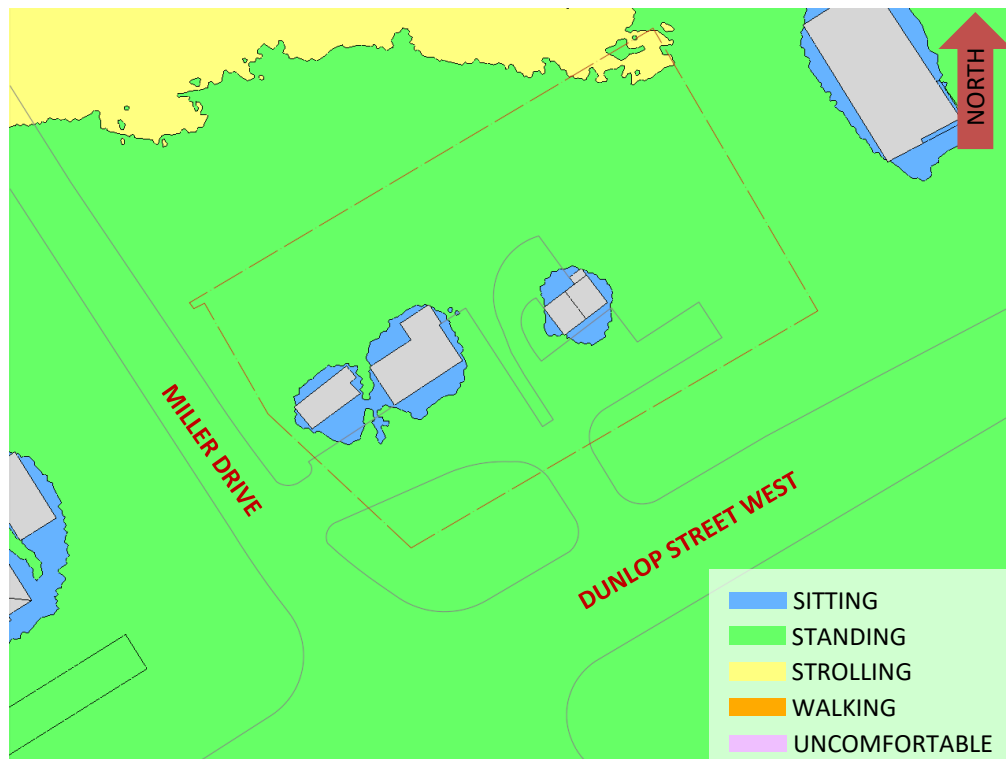


FIGURE 6B: WINTER – WIND COMFORT, GRADE LEVEL – EXISTING MASSING





FIGURE 7A: SPRING – WIND COMFORT, LEVEL 5 AMENITY TERRACES



FIGURE 7B: SUMMER – WIND COMFORT, LEVEL 5 AMENITY TERRACES





FIGURE 7C: AUTUMN – WIND COMFORT, LEVEL 5 AMENITY TERRACES



FIGURE 7D: WINTER – WIND COMFORT, LEVEL 5 AMENITY TERRACES





FIGURE 8A: TYPICAL USE PERIOD – WIND COMFORT, LEVEL 5 AMENITY TERRACES

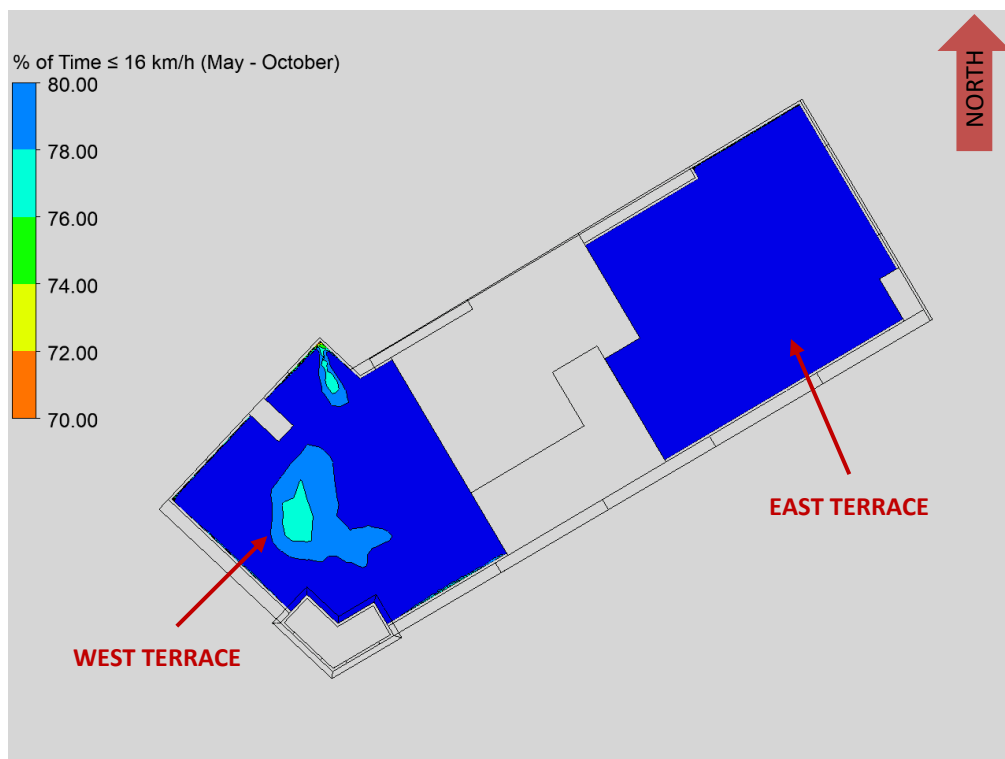


FIGURE 8B: TYPICAL USE PERIOD – % OF TIME SUITABLE FOR SITTING, LEVEL 5 AMENITY TERRACES



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APPENDIX A

SIMULATION OF THE ATMOSPHERIC BOUNDARY LAYER

SIMULATION OF THE ATMOSPHERIC BOUNDARY LAYER

The atmospheric boundary layer (ABL) is defined by the velocity and turbulence profiles according to industry standard practices. The mean wind profile can be represented, to a good approximation, by a power law relation, Equation (1), giving height above ground versus wind speed [1], [2].

$$U = U_g \left(\frac{Z}{Z_g} \right)^\alpha \quad \text{Equation (1)}$$

where, U = mean wind speed, U_g = gradient wind speed, Z = height above ground, Z_g = depth of the boundary layer (gradient height), and α is the power law exponent.

For the model, U_g is set to 6.5 metres per second (m/s), which approximately corresponds to the 50% mean wind speed for Barrie based on historical climate data and statistical analyses. When the results are normalized by this velocity, they are relatively insensitive to the selection of gradient wind speed.

Z_g is set to 540 m. The selection of gradient height is relatively unimportant, so long as it exceeds the building heights surrounding the subject site. The value has been selected to correspond to our physical wind tunnel reference value.

α is determined based on the upstream exposure of the far-field surroundings (i.e., the area that it not captured within the simulation model).

Table 1 presents the values of α used in this study, while Table 2 presents several reference values of α . When the upstream exposure of the far-field surroundings is a mixture of multiple types of terrain, the α values are a weighted average with terrain that is closer to the subject site given greater weight.

TABLE 1: UPSTREAM EXPOSURE (ALPHA VALUE) VS TRUE WIND DIRECTION

Wind Direction (Degrees True)	Alpha Value (α)
0	0.22
40	0.21
98	0.20
132	0.21
164	0.21
200	0.18
237	0.18
263	0.18
280	0.18
295	0.18
310	0.18
331	0.20

TABLE 2: DEFINITION OF UPSTREAM EXPOSURE (ALPHA VALUE)

Upstream Exposure Type	Alpha Value (α)
Open Water	0.14-0.15
Open Field	0.16-0.19
Light Suburban	0.21-0.24
Heavy Suburban	0.24-0.27
Light Urban	0.28-0.30
Heavy Urban	0.31-0.33

The turbulence model in the computational fluid dynamics (CFD) simulations is a two-equation shear-stress transport (SST) model, and thus the ABL turbulence profile requires that two parameters be defined at the inlet of the domain. The turbulence profile is defined following the recommendations of the Architectural Institute of Japan for flat terrain [3].

$$I(Z) = \begin{cases} 0.1 \left(\frac{Z}{Z_g} \right)^{-\alpha-0.05}, & Z > 10 \text{ m} \\ 0.1 \left(\frac{10}{Z_g} \right)^{-\alpha-0.05}, & Z \leq 10 \text{ m} \end{cases} \quad \text{Equation (2)}$$

$$L_t(Z) = \begin{cases} 100 \text{ m} \sqrt{\frac{Z}{30}}, & Z > 30 \text{ m} \\ 100 \text{ m}, & Z \leq 30 \text{ m} \end{cases} \quad \text{Equation (3)}$$

where, I = turbulence intensity, L_t = turbulence length scale, Z = height above ground, and α is the power law exponent used for the velocity profile in Equation (1).

Boundary conditions on all other domain boundaries are defined as follows: the ground is a no-slip surface; the side walls of the domain have a symmetry boundary condition; the top of the domain has a specified shear, which maintains a constant wind speed at gradient height; and the outlet has a static pressure boundary condition.

REFERENCES

- [1] P. Arya, "Chapter 10: Near-neutral Boundary Layers," in *Introduction to Micrometeorology*, San Diego, California, Academic Press, 2001.
- [2] S. A. Hsu, E. A. Meindl and D. B. Gilhousen, "Determining the Power-Law Wind Profile Exponent under Near-neutral Stability Conditions at Sea," vol. 33, no. 6, 1994.
- [3] Y. Tamura, H. Kawai, Y. Uematsu, K. Kondo and T. Okhuma, "Revision of AIJ Recommendations for Wind Loads on Buildings," in *The International Wind Engineering Symposium, IWES 2003*, Taiwan, 2003.