



Technical Memorandum

Date: August 10, 2021 **Project No.:** 300041559.0001

Project Name: Elements Condominium - Hydrogeology Brief

Client Name: Bistro 6 - Subdivision

Submitted To: Mike Flis - Jones Consulting

Submitted By: Dwight Smikle, M.Sc., P.Geo.

Reviewed By: Stephanie Charity, B.Sc., P.Geo

1.0 Background

R.J. Burnside & Associates Limited (Burnside) has been requested to prepare the following hydrogeological brief to respond to comments from the Lake Simcoe Region Conservation Authority (LSRCA) regarding site-specific conditions within Block 598 of the Bistro 6 West subdivision in Barrie. Block 598 forms part of the larger Bistro 6 West subdivision that was studied by Burnside and for which a report entitled "Hydrogeological Study in Support of Draft Plan- Bistro 6 West Subdivision" was completed in October 2019. The current hydrogeology brief draws extensively from the work previously completed.

2.0 Hydrogeological Setting

The local soils were investigated by various studies including the Burnside hydrogeological study and geotechnical studies completed by Peto McCallum. Details of local soils and soil stratigraphy are outlined in the Burnside 2019 report. The report indicates that the local soils consist of sandy silt to silty sand with localized units of silty clay. Geological cross-sections were produced as part of the Burnside study and indicated that the Bistro 6 West lands are underlain by a layer of sand and silt that overlies a sand and silt till. Cross-section B-B' from the Burnside report is attached as it represents the hydrogeological setting interpreted to occur beneath Block 598.

3.0 Significant Groundwater Recharge Areas

The available LSRCA mapping indicates that a Significant Groundwater Recharge Area (SGRA) extends unto the northwestern corner of Block 598. The Burnside 2019 report indicates that the borehole log for monitoring well CD-1 was used to interpret that the area of coarse-grained sediments mapped in this area and assumed to be associated with the SGRA was not proven by the borehole. It was interpreted that the SGRA did not extend into Block 598. More recent boreholes completed by Peto McCallum and included in their “Geotechnical Investigation Proposed Bistro 6 West Development Kneeshaw Drive Barrie, Ontario” Peto McCallum (May 2021) indicate that the sediments in the area of Block 598 are mainly sandy silt to sandy silt till that are compacted and very dense. These sediments are not likely to form high capacity recharge areas due to both compaction and the fine-grained sediments that are also present. The additional data is interpreted as confirming the previous submission that the SGRA does not extend unto Block 598.

4.0 Seasonal Groundwater High

Seasonal groundwater high was mapped by Burnside in 2019 and was noted to vary between approximately 252 meters above sea level (masl) and 254 masl near the east end of Block 598. It is our understanding that the east end of Block 598 is the area where Low Impact Development (LID) measures to promote infiltration are proposed. More recent work completed by Peto McCallum (May 2021), indicates that groundwater in the vicinity of the proposed LIDs varies between 252 masl and 254 masl. Specifically, the report references groundwater measurements conducted in May 2021 that confirm that the depth to water in the area is within this range. The report goes on to recommend elevations for the base of the proposed LID measures that are at least 1 m above the measured seasonal high. Based on the consistency between the Burnside measurements and those completed by Peto McCallum, it is our opinion that the measurements are representative of the seasonal groundwater high in the vicinity of the proposed LID measures.

5.0 Groundwater Balance

A groundwater balance was completed for Block 598 in keeping with LSRCA requirements and based on the Thornthwaite and Mather approach. The assumptions of the calculation were kept the same as those used for the entire subdivision in the Burnside 2019 report in order to remain consistent with those calculations. The methodology for the calculations is outlined in the Burnside 2019 report. The infiltration factors used for the calculation are summarized in the Table 1 below:

Table 1: Infiltration Factors

| | Pre-Development | | Post-Development | |
|------------|-----------------|-------------------------------|------------------|------------------------------|
| | Agricultural | | Urban Lawn | |
| | Factor | Rationale | Factor | Rationale |
| Topography | 0.1 | Slope of 4% | 0.1 | Similar to pre-conditions |
| Soils | 0.40 | Sandy loam soils | 0.40 | Same soils as pre-conditions |
| Cover | 0.1 | Predominantly cultivated land | 0.15 | Urban lawns |
| Total | 0.60 | | 0.65 | |

Using data from the Barrie WPCC climate station the calculations were completed and a summary of the water balance component values is provided in Table 2.

Table 2: Water Balance Component Values

| Water Balance Component | Agricultural Lands | Urban Lawn |
|---------------------------|--------------------|-------------|
| Average Precipitation | 933 mm/year | 933 mm/year |
| Actual Evapotranspiration | 593 mm/year | 555 mm/year |
| Water Surplus | 340 mm/year | 378 mm/year |
| Infiltration | 204 mm/year | 246 mm/year |
| Runoff | 136 mm/year | 132 mm/year |

The water balance component values from Table WB-1 and Table WB-2 (attached) were used to calculate the average annual volume of infiltration across Block 598. Based on these component values, the total pre-development infiltration volume for the block is calculated to be about 6,400 m³/year.

To assess potential development impacts on infiltration, the post-development infiltration volumes have been calculated for the block on Table WB-3 (attached). The proposed land use areas were provided by Jones Consulting Group. The calculated post-development infiltration volume (without mitigation) for the block is about 3,500 m³/year.

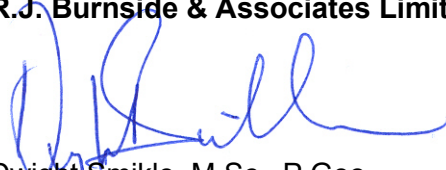
Comparing the pre- and post-development infiltration volumes, shows that development has the potential to reduce the average infiltration on the block by 45 % or 2,900 m³/year (Table WB-3, attached).

6.0 Mitigation Strategies for Infiltration

To minimize the potential impacts of development on the water balance, the use of Low Impact Development (LID) measures for stormwater management are generally recommended by the conservation authority. It is our understanding that LID measures are proposed in three locations within the block. Based on calculations completed by the design engineers at Jones Consulting, we understand that a total infiltration volume of approximately 11,400 m³/year would

be generated at the three infiltration facilities. This available infiltration is significantly above the calculated deficit and indicates that the proposed LID measures would mitigate for the loss in natural infiltration caused by the development process.

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Enclosure(s) Water Balance Tables WB-1, WB-2 and WB-3
Figure 5 – Borehole, Well and Cross-Section Locations
Figure 7 – Interpreted Geological Cross-Section B-B'

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WATER BALANCE CALCULATIONS

Block 598
Bistro 6 West Subdivision
Barrie, ON
PROJECT No.300041559



TABLE WB-1

| Water Balance Components | | | | | | | | | | | | | |
|--|--|--|--|--|--|--|--|--|--|--|--|--|--|
| Based on Thornthwaite's Soil Moisture Balance Approach with a Soil Moisture Retention of 150 mm (moderately-rooted vegetation in sandy loam soils) | | | | | | | | | | | | | |
| Precipitation data from Barrie WPCC Climate Station (1981 - 2010) | | | | | | | | | | | | | |

| Potential Evapotranspiration Calculation | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | YEAR |
|--|------|---------|------|-------|-------|-------|--------|-------|-------|-------|-------|------|------|
| Average Temperature (Degree C) | -7.7 | -6.6 | -2.1 | 5.6 | 12.3 | 17.9 | 20.8 | 19.7 | 15.3 | 8.7 | 2.7 | -3.5 | 6.9 |
| Heat index: $i = (t/5)^{1.514}$ | 0.00 | 0.00 | 0.00 | 1.19 | 3.91 | 6.90 | 8.66 | 7.97 | 5.44 | 2.31 | 0.39 | 0.00 | 36.8 |
| Unadjusted Daily Potential Evapotranspiration U (mm) | 0.00 | 0.00 | 0.00 | 25.18 | 58.76 | 88.02 | 103.48 | 97.59 | 74.33 | 40.47 | 11.47 | 0.00 | 499 |
| Adjusting Factor for U (Latitude 44° 20' N) | 0.81 | 0.82 | 1.02 | 1.13 | 1.27 | 1.29 | 1.3 | 1.2 | 1.04 | 0.95 | 0.8 | 0.76 | |
| Adjusted Potential Evapotranspiration PET (mm) | 0 | 0 | 0 | 28 | 75 | 114 | 135 | 117 | 77 | 38 | 9 | 0 | 593 |
| | | | | | | | | | | | | | |
| WATER BALANCE COMPONENTS | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | YEAR |
| Precipitation (P) | 83 | 62 | 58 | 62 | 82 | 85 | 77 | 90 | 94 | 78 | 89 | 74 | 933 |
| Potential Evapotranspiration (PET) | 0 | 0 | 0 | 28 | 75 | 114 | 135 | 117 | 77 | 38 | 9 | 0 | 593 |
| P - PET | 83 | 62 | 58 | 34 | 8 | -29 | -57 | -27 | 17 | 39 | 80 | 74 | 340 |
| Change in Soil Moisture Storage | 0 | 0 | 0 | 0 | 0 | -29 | -57 | -27 | 17 | 39 | 58 | 0 | 0 |
| Soil Moisture Storage max 150 mm | 150 | 150 | 150 | 150 | 150 | 121 | 64 | 37 | 53 | 92 | 150 | 150 | |
| Actual Evapotranspiration (AET) | 0 | 0 | 0 | 28 | 75 | 114 | 135 | 117 | 77 | 38 | 9 | 0 | 593 |
| Soil Moisture Deficit max 150 mm | 0 | 0 | 0 | 0 | 0 | 29 | 86 | 113 | 97 | 58 | 0 | 0 | |
| Water Surplus - available for infiltration or runoff | 83 | 62 | 58 | 34 | 8 | 0 | 0 | 0 | 0 | 0 | 22 | 74 | 340 |
| Potential Infiltration (based on MOE methodology*; independent of temperature) | 50 | 37 | 35 | 20 | 5 | 0 | 0 | 0 | 0 | 0 | 13 | 44 | 204 |
| Potential Direct Surface Water Runoff (independent of temperature) | 33 | 25 | 23 | 13 | 3 | 0 | 0 | 0 | 0 | 0 | 9 | 29 | 136 |
| | | | | | | | | | | | | | |
| IMPERVIOUS AREA WATER SURPLUS | | | | | | | | | | | | | |
| Precipitation (P) | 933 | mm/year | | | | | | | | | | | |
| Potential Evaporation (PE) from impervious areas (assume 15%) | 140 | mm/year | | | | | | | | | | | |
| P-PE (surplus available for runoff from impervious areas) | 793 | mm/year | | | | | | | | | | | |

Assume January storage is 100% of Soil Moisture Storage
Soil Moisture Storage

150 mm

<-- See "Water Holding Capacity" values in Table 3.1, MOE SWMPDM, 2003

*MOE SWM infiltration calculations

topography - hilly land (avg slope ~ 4%)

0.1

soils - sandy loam

0.4

cover - predominantly cultivated land

0.1

Infiltration factor

0.6

<-- Infiltration Factors from the bottom section of Table 3.1, MOE SWMPDM, 2003

<-- Infiltration Factors from the bottom section of Table 3.1, MOE SWMPDM, 2003

<-- Infiltration Factors from the bottom section of Table 3.1, MOE SWMPDM, 2003

Latitude of site (or climate station)

44 ° N.

WATER BALANCE CALCULATIONS

Block 598
Bistro 6 West Subdivision
Barrie, ON
PROJECT No.300041559



TABLE WB-2

| Post-Development Water Balance Components | | | | | | | | | | | | | |
|---|--|--|--|--|--|--|--|--|--|--|--|--|--|
| Based on Thornthwaite's Soil Moisture Balance Approach with a Soil Moisture Retention of 75 mm (urban lawn in sandy loam soils) | | | | | | | | | | | | | |
| Precipitation data from Barrie WPCC Climate Station (1981 - 2010) | | | | | | | | | | | | | |

| Potential Evapotranspiration Calculation | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | YEAR |
|--|------|---------|------|-------|-------|-------|--------|-------|-------|-------|-------|------|------|
| Average Temperature (Degree C) | -7.7 | -6.6 | -2.1 | 5.6 | 12.3 | 17.9 | 20.8 | 19.7 | 15.3 | 8.7 | 2.7 | -3.5 | 6.9 |
| Heat index: $i = (t/5)^{1.514}$ | 0.00 | 0.00 | 0.00 | 1.19 | 3.91 | 6.90 | 8.66 | 7.97 | 5.44 | 2.31 | 0.39 | 0.00 | 36.8 |
| Unadjusted Daily Potential Evapotranspiration U (mm) | 0.00 | 0.00 | 0.00 | 25.18 | 58.76 | 88.02 | 103.48 | 97.59 | 74.33 | 40.47 | 11.47 | 0.00 | 499 |
| Adjusting Factor for U (Latitude 44° 20' N) | 0.81 | 0.82 | 1.02 | 1.13 | 1.27 | 1.29 | 1.3 | 1.2 | 1.04 | 0.95 | 0.8 | 0.76 | |
| Adjusted Potential Evapotranspiration PET (mm) | 0 | 0 | 0 | 28 | 75 | 114 | 135 | 117 | 77 | 38 | 9 | 0 | 593 |
| | | | | | | | | | | | | | |
| WATER BALANCE COMPONENTS | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC | YEAR |
| Precipitation (P) | 83 | 62 | 58 | 62 | 82 | 85 | 77 | 90 | 94 | 78 | 89 | 74 | 933 |
| Potential Evapotranspiration (PET) | 0 | 0 | 0 | 28 | 75 | 114 | 135 | 117 | 77 | 38 | 9 | 0 | 593 |
| P - PET | 83 | 62 | 58 | 34 | 8 | -29 | -57 | -27 | 17 | 39 | 80 | 74 | 340 |
| Change in Soil Moisture Storage | 0 | 0 | 0 | 0 | 0 | -29 | -46 | 0 | 17 | 39 | 19 | 0 | 0 |
| Soil Moisture Storage max 75 mm | 75 | 75 | 75 | 75 | 75 | 46 | 0 | 0 | 17 | 56 | 75 | 75 | |
| Actual Evapotranspiration (AET) | 0 | 0 | 0 | 28 | 75 | 114 | 123 | 90 | 77 | 38 | 9 | 0 | 555 |
| Soil Moisture Deficit max 75 mm | 0 | 0 | 0 | 0 | 0 | 29 | 75 | 75 | 58 | 19 | 0 | 0 | |
| Water Surplus - available for infiltration or runoff | 83 | 62 | 58 | 34 | 8 | 0 | 0 | 0 | 0 | 0 | 60 | 74 | 378 |
| Potential Infiltration (based on MOE methodology*; independent of temperature) | 54 | 40 | 38 | 22 | 5 | 0 | 0 | 0 | 0 | 0 | 39 | 48 | 246 |
| Potential Direct Surface Water Runoff (independent of temperature) | 29 | 22 | 20 | 12 | 3 | 0 | 0 | 0 | 0 | 0 | 21 | 26 | 132 |
| | | | | | | | | | | | | | |
| IMPERVIOUS AREA WATER SURPLUS | | | | | | | | | | | | | |
| Precipitation (P) | 933 | mm/year | | | | | | | | | | | |
| Potential Evaporation (PE) from impervious areas (assume 15%) | 140 | mm/year | | | | | | | | | | | |
| P-PE (surplus available for runoff from impervious areas) | 793 | mm/year | | | | | | | | | | | |

Assume January storage is 100% of Soil Moisture Storage
Soil Moisture Storage

75 mm

<-- See "Water Holding Capacity" values in Table 3.1, MOE SWMPDM, 2003

*MOE SWM infiltration calculations

topography - hilly land

0.1

soils - sandy loam

0.4

cover - urban lawn

0.15

Infiltration factor

0.65

<-- Infiltration Factors from the bottom section of Table 3.1, MOE SWMPDM, 2003

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Latitude of site (or climate station)

44 ° N.

WATER BALANCE CALCULATIONS

Block 598
Bistro 6 West Subdivision
Barrie, ON
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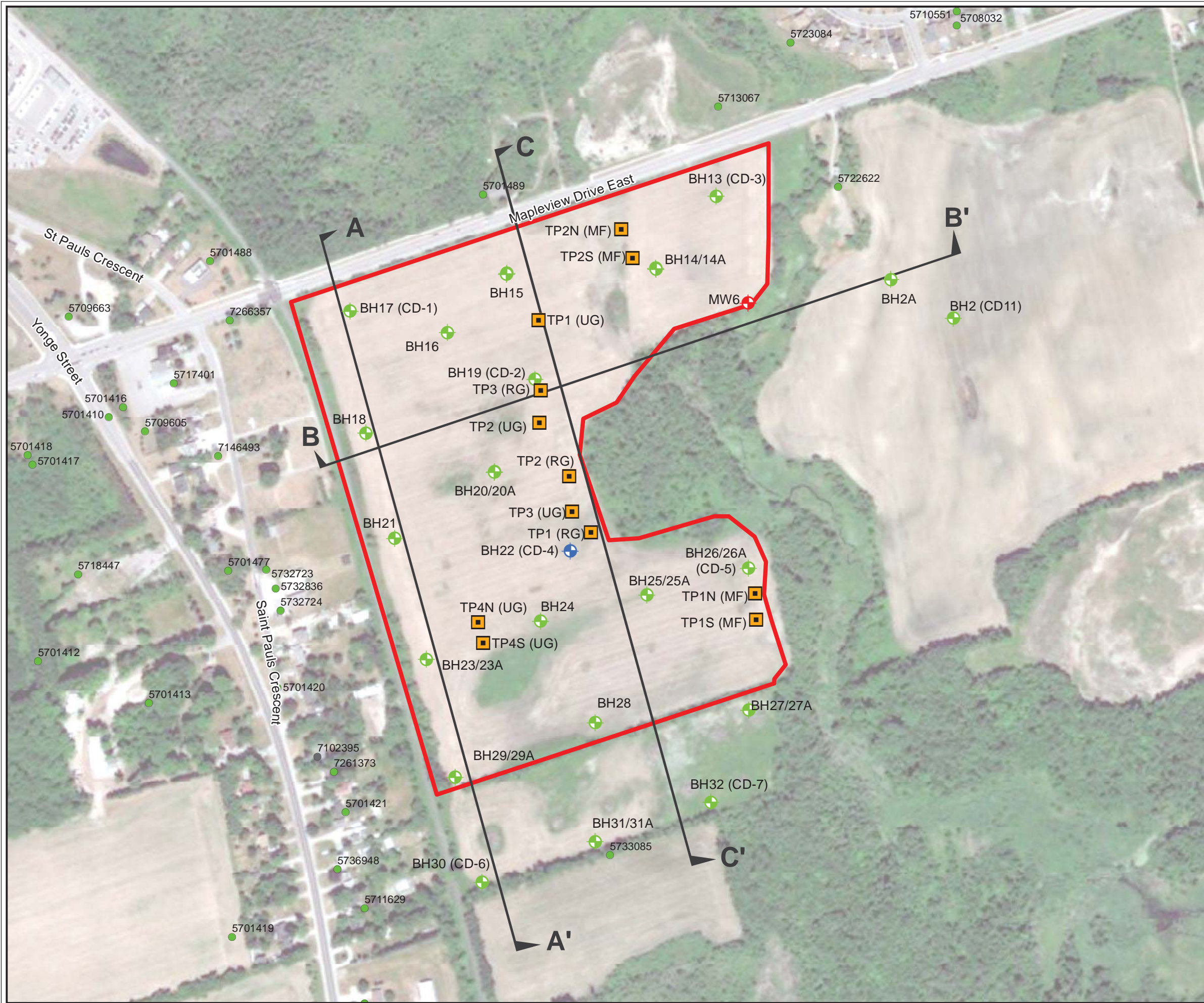
TABLE WB-3

| Water Balance for Pre- and Post-Development Land Use Conditions (with no SWM/LID measures in place) | | | | | | | | | | | | |
|---|--------------------------------------|---|---|-------------------------------------|--|---|-----------------------------------|--|---|--|---|---|
| Land Use Description | Approx. Land Area* (m ²) | Estimated Impervious Fraction for Land Use* | Estimated Impervious Area (m ²) | Runoff from Impervious Area** (m/a) | Runoff Volume from Impervious Area (m ³ /a) | Estimated Pervious Area (m ²) | Runoff from Pervious Area** (m/a) | Runoff Volume from Pervious Area (m ³ /a) | Infiltration from Pervious Area** (m/a) | Infiltration Volume from Pervious Area (m ³ /a) | Total Runoff Volume (m ³ /a) | Total Infiltration Volume (m ³ /a) |
| Pre-Development Land Use | | | | | | | | | | | | |
| Open Space /Agricultural | 31,500 | 0.00 | 0 | 0.793 | 0 | 31,500 | 0.136 | 4,280 | 0.204 | 6,421 | 4,280 | 6,421 |
| TOTAL PRE-DEVELOPMENT | 31,500 | | 0 | | 0 | 31,500 | | 4,280 | | 6,421 | 4,280 | 6,421 |
| Post-Development Land Use (with no LID measures in place) | | | | | | | | | | | | |
| Landscape/ Open Space | 16,800 | 0.15 | 2,520 | 0.793 | 1,998 | 14,280 | 0.132 | 1,889 | 0.246 | 3,509 | 3,887 | 3,509 |
| Residential Building | 6,400 | 1.00 | 6,400 | 0.793 | 5,075 | 0 | 0.132 | 0 | 0.246 | 0 | 5,075 | 0 |
| Parking | 8,300 | 1.00 | 8,300 | 0.793 | 6,582 | 0 | 0.132 | 0 | 0.246 | 0 | 6,582 | 0 |
| TOTAL POST-DEVELOPMENT | 31,500 | | 17,220 | | 13,655 | 14,280 | | 1,889 | | 3,509 | 15,544 | 3,509 |
| % Change from Pre to Post | | | | | | | | | | | 363 | 45 |
| Effect of development (with no mitigation) | | | | | | | | | | | 3.6 times increase in runoff | 45% reduction of infiltration |

* data provided by Jones Consulting Group Ltd.

** figures from Tables WB-1 and WB-2

To balance pre- to post-,
the infiltration target (m³/a)= **2,912**



LEGEND

- SUBJECT LANDS
- MONITORING WELL (PML, JULY 2017)
- MONITORING WELL (PML, JUNE 2017)
- MONITORING WELL (RJB, 2014)
- TEST PIT (PETO MacCALLUM, 2019)

MECP WELL RECORD

- OVERBURDEN
- UNKNOWN

CROSS SECTION LOCATION KEY

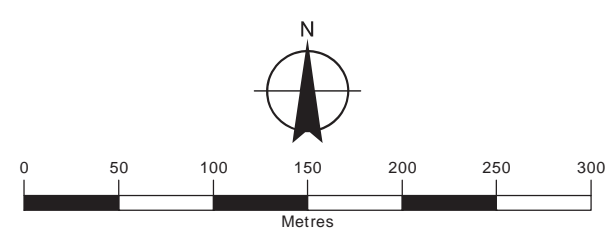
A — A'

B — B'

C — C'

Sources:

1. Ministry of Natural Resources and Forestry, © Queen's Printer for Ontario
2. Natural Resources Canada © Her Majesty the Queen in Right of Canada.



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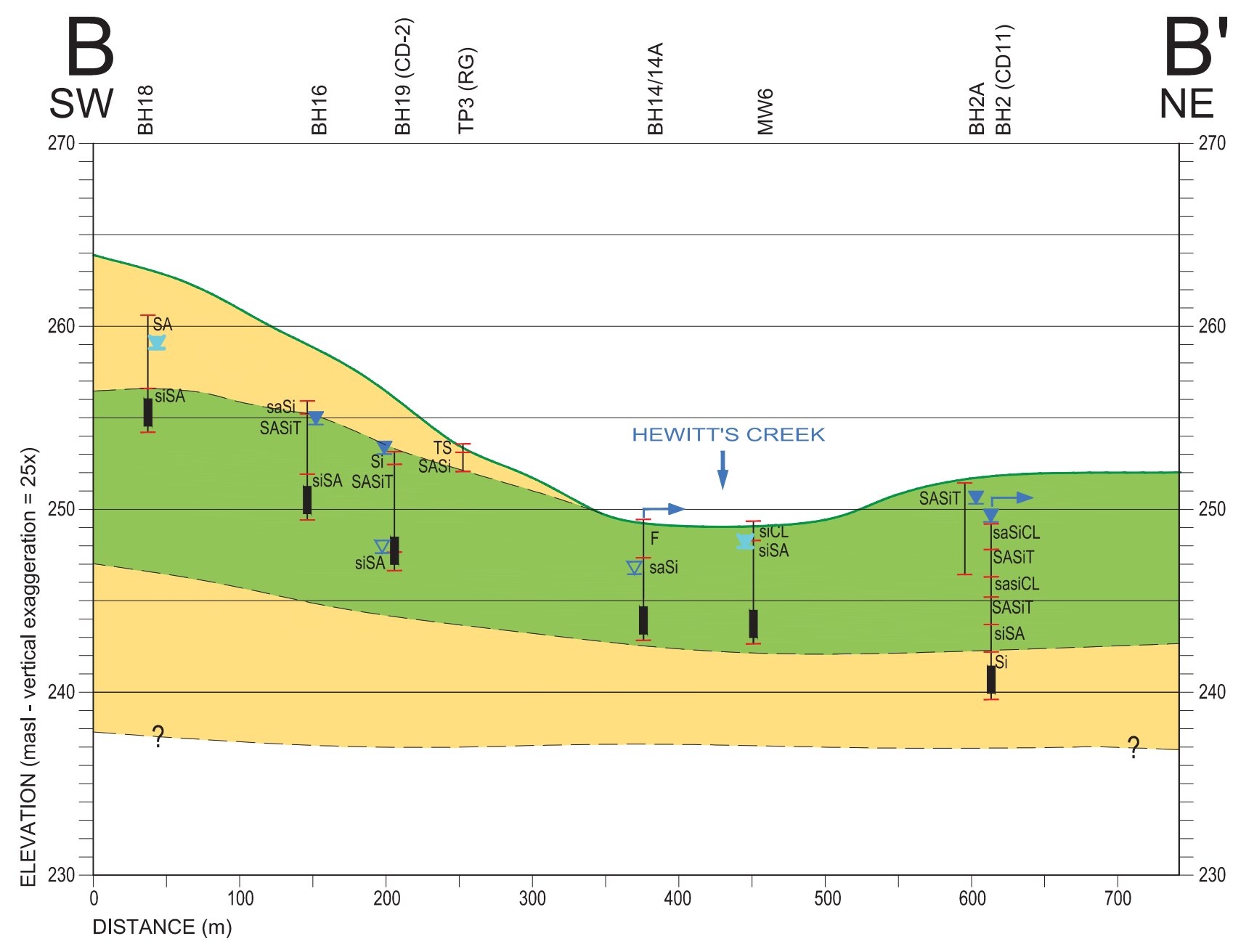
CRISDAWN CONSTRUCTION LIMITED
BARRIE, ONTARIO

HYDROGEOLOGICAL STUDY
BISTRO 6 SUBDIVISION

Figure Title

**BOREHOLE, WELL AND
CROSS-SECTION LOCATIONS**

| | | | |
|---------|---------|-------------|------------------------|
| Drawn | Checked | Date | Figure No. 5 |
| SK | SC | August 2019 | |
| Scale | | Project No. | |
| 1:4,000 | | 300041559 | |



LEGEND

- 4901807 MW10
- CLGR
- WELL / BOREHOLE ID
- MOE WELL RECORD NUMBER
- WELL
- GEOLOGICAL STRATIGRAPHY
- WATER LEVEL AT FIRST STRIKE (REPORTED ON BOREHOLE AND TEST PIT LOGS (PETO))
- MEASURED WATER LEVEL (SEASONAL HIGH) FROM ARTESIAN SYSTEM
- MEASURED WATER LEVEL (SEASONAL HIGH) FROM SHALLOW SYSTEM
- WELL SCREEN

- SAND / SILT / TILL
- SAND / SILT
- INTERPRETED GEOLOGICAL CONTACT
- WATERCOURSE CROSSING
- INDICATES FLOWING

- si: SILTY
- cl: CLAYEY
- sa: SANDY
- F: FILL
- T: TILL
- SA: SAND
- Si: SILT
- GR: GRAVEL
- CL: CLAY
- PRDG: PREDUG



Client

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HYDROGEOLOGICAL STUDY
BISTRO 6 SUBDIVISION

Figure Title

INTERPRETED GEOLOGICAL
CROSS-SECTION B-B'

| | | | |
|---------|-------------|-------------|------------|
| Drawn | Checked | Date | Figure No. |
| SK | SC | August 2019 | |
| Scale | Project No. | | |
| 1:7,500 | 300041559 | | |